Naval Oceanographic Office

Stennis Space

Technical Report

Center MS 39522-5001 TR 304 October 1991



AD-A245 860

TR 304

THE JOINT US/UK 1990 EPOCH WORLD MAGNETIC MODEL

JOHN M. QUINN RACHEL J. COLEMAN MICHAEL R. PECK STEPHEN E. LAUBER

GEOPOTENTIAL DIVISION



Approved for public release; distribution is unlimited

Prepared under the authority of Commander,
Naval Oceanography Command

92-02457

FOREWORD

As it has in centuries past, the Earth's magnetic field still plays a vital role in global navigation. All navigational aids or attitude/heading reference systems (AHRS), regardless of their operating principles, must speak a common language. That common language is in terms of the Earth's magnetic declination. Consequently, magnetic-related navigational aids are integrated, in the form of computer hardware and software, into virtually every major weapons system of the Army, Air Force, Navy, and Marines. In order to maintain optimum performance, these systems must be periodically updated with regard to the Earth's magnetic field, which is a dynamic entity that changes slowly but erratically with time.

For well over a century, it has been the responsibility of the U.S. Naval Oceanographic Office to monitor the Earth's changing magnetic field and periodically report on these changes in the form of magnetic charts and mathematical models. For the past forty years, this task has involved an intensive data collection effort through the Project MAGNET program, which in April 1990 made the transition from primarily aeromagnetic surveying to satellite surveying with the launch of the Polar Orbiting Geomagnetic Survey (POGS) satellite. Follow-on satellite missions to secure data for future needs, well into the twenty-first century, are now being vigorously pursued.

This report is a comprehensive summary of the cooperative effort between the U.S. Naval Oceanographic Office and the British Geological Survey in producing the 1990 Epoch World Magnetic Model, WMM-90.

ROBERT Y FELT Captain, U.S. Navy

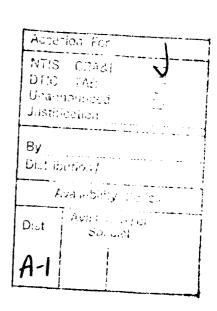
Commanding Officer

REPORT D	OCUMENTATIO	N PAGE			Form Approved OMB No 0704 0188			
1a REPORT SECURITY CLASSIFICATION UNCLASSIFIED		15 RESTRICT VE None	VAR NGS	-				
28 SECURITY CLASSIFICATION AUTHORITY N/A			ad for pub		elease:			
26 DECLASSIFICATION DOWNGRADING SCHEDUL N/A	Ē		oution unl					
4 PERFORMING ORGANIZATION REPORT NUMBE	R(S)	5 MONITORING	ORGANIZATION R	PORT NU	V3:95			
TR 304								
6a NAME OF PERFORMING ORGANIZATION	6b OFFICE SYMBOL (If applicable)		ONITORING ORGA					
Naval Oceanographic Office 6c. ADDRESS (City, State, and ZIP Code)			ty, State and ZIP C		aphy Command			
Stennis Space Center, MS 3952	2–5001		Space Cente		39529-5000			
8a NAME OF FUNDING SPONSORING ORGANIZATION	8b OFFICE SYMBOL (If applicable)	9 PROCUREMEN	IT NS RUMENT DI	ENTIFICAT	ON NUMBER			
Naval Oceanographic Office		10 (0) 05 05	5 10 16 5 10 50	-				
8c. ADDRESS (City, State, and ZIP Code)		PROGRAM	PROJECT	TASK	WORK UNIT			
Stennis Space Center, MS 3952	2-5001	ELEMENT NO	NO	NO	ACCESSION NO			
11 TITLE (Include Security Classification)					<u>.</u>			
The Joint US/UK 1990 Epo	ch World Mag	netic Mode	el					
12 PERSONAL AUTHOR(S)	Dechal I	Danie Mini	bool D . I	ab.a.s	Chamban E			
Quinn, John M.; Coleman, 13a TYPE OF REPORT 13b TIME CO			DRT (Year, Month.					
Technical FROM 19	90 to 1995	1991 Octobe	er		217			
16 SUPPLEMENTARY NOTATION								
17 COSATI CODES	18 SUBJECT TERMS (C							
FIELD GROUP SUB-GROUP		c; World Magnetic Model; WMM-90; GVAR: DE-2; MAGSAT: POGS: Project						
	MAGNET; 199		•		_			
19 ABSTRACT (Continue on reverse if necessary								
A detailed summary of the data used, analyses performed, modeling techniques employed, and results obtained in the course of the 1990 Epoch World Magnetic Modeling effort are given. Also, use and limitation of the GEOMAG algorithm are presented. Charts and tables related to the 1990 World Magnetic Model (WMM-90) for the Earth's main field and secular variation in Mercator and polar stereographic projections are presented along with useful tables of several magnetic field components and their secular variation on a 5-degree worldwide grid.								
20 DISTRIBUTION AVAILABILITY OF ABSTRACT			CURITY CLASS FICA	AT:ON				
¥ UNCLASSIFIED UNLIMITED ☐ SAME AS R	PT DTIC USERS	Unclas:	sified Unclude Area Code	11226 05	e de Krigadi			
John S. Breyer		(601) 689-84			306			

TABLE OF CONTENTS

Acknowledgements	ix
Section 1. The GEOMAG Algorithm and the 1990 Model	1
1.0 Introduction	1 2 5 7
Section 2. The 1990 Epoch World Magnetic Model (Derivation).	15
2.0 Overview	15 20 45 50
Section 3. Discussion	69
3.0 Modeling Results	69 73
References	195
Appendix	
FORTRAN Listing of GEOMAG Subroutine with the WMM-90 Model Coefficients	197





LIST OF TABLES

Table	1	Arrangement of Main Field Coefficients in Array $C_{\mathtt{AM}}$	8
Table	2	Arrangement of Secular Variation Coefficients in Array \dot{C}_{nm}	Ç,
Table	3	WMM-90 Schmidt Normalized Gauss Coefficients	12
Table	4	Secular Variation Models	46
Table	5	WC-85 (Revised) Schmidt Normalized Gauss Coefficients	51
Table	6	RMS Errors Relative to IGRF/DGRF Models	56
Table	7	Number of Records	56
Table	8	Average Number of Records Per Cell	56
Table	9	Project MAGNET Flight Statistics Relative to IGRF/DGRF Models	57
Table	10	Dip Pole Positions	72
Table	11	WMM-90 Main Field and Annual Change Grid Values	75
		North Component (X) WMM-90	76
		East Component (Y) WMM-90	88
		Vertical Component (Z) WMM-90	100
		Horizontal Component (H) WMM-90	112
		Total Intensity (F) WMM-90	124
		Declination (D) WMM-90	136
		Inclination (I) WMM-90	148

LIST OF CHARTS

Chart	1.	Project MAGNET Data Distribution	16
Chart	2.	MAGSAT Data Distribution	17
Chart	3.	DE-2 Data Distribution	18
Chart	4.	Geomagnetic Observatory Distribution	19
Chart	5.	North Magnet c Pole Movement	70
Chart	6.	South Magnetic Pole Movement	71
Chart	7.	Geomagnetic Coordinates	74
		Main Field World Mercator Charts	
Chart	8.	Horizontal Intensity (H)	160
Chart	9.	Vertical Component (Z)	161
Chart		-	162
Chart	11.	Declination (D)	163
Chart	12.	Inclination (I)	164
		Secular Variation World Mercator Charts	
Chart	13.	Horizontal Intensity (\dot{H})	165
		Vertical Component ($\dot{\mathbf{Z}}$)	166
Chart	15.	Total Intensity (\dot{F})	167
Chart	16.	Declination (\dot{D})	168
Chart	17.	Inclination ($\dot{\mathbf{I}}$)	169
		Main Field North Polar Stereographic Charts	
Chart	18.	Horizontal Intensity (H)	170
		Vertical Component (Z)	171
Chart	20.	Total Intensity (F)	172
Chart	21.	Declination (D)	173
Chart	22.	Inclination (I)	174
Chart	23.	Grid Variation (GV)	175
		Secular Variation North Polar Stereographic Charts	
Chart	24.	Horizontal Intensity (\dot{H})	176
		Vertical Component ($\dot{\mathbf{Z}}$)	177
Chart	26.	Total Intensity (\dot{F})	178
		Declination (\dot{D})	179
Chart	28.	Inclination ($\dot{\mathbf{I}}$)	180
Chart	29	Grid Variation (\vec{GV})	181

Main Field South Polar Stereographic Charts

Chart	30.	Horizontal Intensity (H)	182
Chart	31.	Vertical Component (Z)	183
Chart	32.	Total Intensity (F)	184
Chart	33.	Declination (D)	185
Chart	34.	Inclination (I)	186
Chart	35.	Grid Variation (GV)	187
		Secular Variation South Polar Stereographic Charts	
Chart	36.	Horizontal Intensity (\dot{H})	188
Chart	37.	Vertical Component (Ż)	189
Chart	38.	Total Intensity (\dot{F})	190
Chart	39.	Declination (\dot{D})	191
Chart	40.	Inclination ($\dot{\mathbf{l}}$)	192
Chart	41.	Grid Variation (\dot{GV})	193

LIST OF FIGURES

Annu	al M	Magnetic Means at Selected Geomagnetic Observatories	
Figure	la.	North X Component at Honolulu (HON)	21
Figure	1b.	East Y Component at Honolulu (HON)	22
Figure	1c.	Vertical Z Component at Honolulu (HON)	23
Figure	1d.	Declination D Component at Honolulu (HON)	24
Figure	le.	Inclination I Component at Honolulu (HON)	25
Figure	1f.	Total Intensity F Component at Honolulu (HON)	26
Figure	2a.	North X Component at Huancayo (HUA)	27
Figure	2b.	East Y Component at Huancayo (HUA)	28
Figure	2c.	Vertical Z Component at Huancayo (HUA)	29
Figure	2d.	Declination $oldsymbol{\mathcal{D}}$ Component at Huancayo (HUA)	30
Figure	2e.	Inclination I Component at Huancayo (HUA)	31
Figure	2f.	Total Intensity F Component at Huancayo (HUA)	32
Figure	3a.	North X Component at Pilar (PIL)	33
Figure	3b.	East Y Component at Pilar (PIL)	34
Figure	3c.	Vertical Z Component at Pilar (PIL)	35
Figure	3d.	Declination $oldsymbol{D}$ Component at Pilar (PIL)	36
Figure	3e.	Inclination I Component at Pilar (PIL)	37
Figure	3f.	Total Intensity F Component at Pilar (PIL)	38
Figure	4a.	North X Component at Rude Skov (RSV)	39
Figure	4b.	East Y Component at Rude Skov (RSV)	40
Figure	4c.	Vertical Z Component at Rude Skov (RSV)	41
Figure	4d.	Declination $oldsymbol{D}$ Component at Rude Skov (RSV)	42
Figure	4e.	Inclination I Component at Rude Skov (RSV)	43
Figure	4f.	Total Intensity F Component at Rude Skov (RSV)	44

ACKNOWLEDGEMENTS

Overall coordination and production of the joint US/UK World Magnetic Model for the 1990 Epoch was the responsibility of Dr. David R. Barraclough of the British Geological Survey (BGS) and Mr. John M. Quinn of the U.S. Naval Oceanographic Office. Needless to say, however, these models could not be produced without the assistance of those many unnamed individuals around the world who collect magnetic field data on a day-to-day basis. Most particularly, we would like to acknowledge those who operate the geomagnetic observatories, the geophysicists, engineers, and technicians from the Naval Oceanographic Office who have collected and processed Project MAGNET data over the past ten years, and the military personnel from VXN-8 in Patuxent River, Maryland, who flew and maintained the Project MAGNET aircraft during this period. We also thank both the National Aeronautics and Space Administration and the U.S. Geological Survey for making the MAGSAT data available and M. Sugiura, J.R. Ridgeway, and Robert Langel for making the DE-2 data available. Finally, we appreciate the extraordinary abilities and dedication of our secretary, Nanette Williams, who was responsible for typing this manuscript and its many revisions.

1.0 <u>Introduction</u>

The Earth's magnetic field, as measured by a magnetic sensor on or above the Earth's surface, is actually a composite of several magnetic fields generated by a variety of sources, which are superimposed on each other and which interact with each other. The most important of these geomagnetic sources are:

- a. the Earth's fluid outer core;
- b. the Earth's crust/upper mantle;
- c. the ionosphere; and
- d. the magnetosphere.

The magnetic variation algorithm (GEOMAG) is a Fortran subroutine which is based on a spherical harmonic expansion of the Earth's magnetic field, the coefficients of which comprise the World Magnetic Model (WMM). These coefficients are produced jointly by the U.S. Naval Oceanographic Office (NAVOCEANO)'s Geopotential Division and the British Geological Survey (BGS). The WMM is distributed by NAVOCEANO for the Defense Mapping Agency (DMA) in accordance with DMA Instructions 8000.1 and 8000.2. The WMMs are usually produced at 5-year intervals and are composed of two parts: a main field model, which describes the Earth's magnetic field at some base epoch, and a secular variation model, which accounts for the slow temporal variations in the main geomagnetic field from the base epoch to a maximum of 5 years beyond the base epoch. For example, the base epoch of the WMM-90 magnetic field model is 1990.0. This model is therefore considered valid between 1990.0 and 1995.0 and will subsequently be replaced at 1995.0 by the WMM-95 magnetic field model.

It is extremely important to recognize that the WMM series of geomagnetic models and the charts produced from these models characterize only that portion of the Earth's magnetic field which is generated by the Earth's fluid outer core. The portions of the geomagnetic field generated by the Earth's crust, mantle, ionosphere, and magnetosphere are not represented in these models. Consequently, a magnetic sensor such as a compass or magnetometer may observe spatial and temporal magnetic anomalies when referenced to the appropriate In particular, certain local, regional, and temporal magnetic declination anomalies can exceed 10 degrees. Anomalies of this magnitude are not common, but they do exist. Declination anomalies on the order of 3 or 4 degrees are not uncommon, but are of small spatial extent and relatively isolated. On land, spatial anomalies are produced by mountain ranges; ore deposits; ground which has been struck by lightning; geological faults; and cultural features such as trains, planes, tanks, railroad tracks, power lines, etc. In ocean spatial anomalies are produced by continental margins, seamounts, oceanic ridges, trenches and fault zones, and ships and submarines. Temporal anomalies in either ocean or land areas can last from a few minutes to several days and are produced by ionospheric and magnetospheric processes which are driven by the solar wind.

Magnetic storms in particular can cause severe and persistent magnetic anomalies. Even in periods of quiet solar activity, significant spatial and temporal magnetic anomalies are found in the polar and equatorial regions of the Earth, where magnetic fields produced by ionospheric current systems, such as the auroral electrojets and the equatorial electrojet, are always present. Most of the possible sources of magnetic anomalies are comparatively isolated in either space or time. Therefore, from a global perspective, the root-mean-square (RMS), declination (DEC), and inclination (DIP) errors at sea level of the WMM are estimated to be less than 0.5 degrees in ocean areas and less than 1.0 degrees in land areas at the Earth's surface over the entire 5-year life of a particular model. Also, the RMS errors at sea level of the horizontal (H) and total intensity (F) components of the WMM over ocean and land areas are estimated to be less than 200 nanoteslas (nT) over the entire 5-year life of the models.

1.1 The Mathematical Model

The Earth's magnetic field has associated with it a geomagnetic potential $V(r,\theta,\phi,\tau)$, which can be expressed in spherical coordinates in terms of a spherical harmonic expansion of the following form:

$$V(r,\theta,\phi,\tau) = R_E \sum_{n=1}^{N} \left(\frac{R_E}{r} \right)^{n+1} \sum_{m=0}^{n} \{ g_{nm}(\tau) \cos m\phi + h_{nm}(\tau) \sin m\phi \} P_n^m(\theta)$$
 (1)

where the spherical coordinates (r,θ,ϕ) correspond to the radius from the center of the Earth, the colatitude (i.e., 90° - latitude), and the longitude. R_E is the mean radius of the Earth; $g_{nm}(\tau)$ and $h_{nm}(\tau)$ are referred to as the Gauss coefficients at time τ , where τ is the time in years (e.g., 1987.312). $P_n^m(\theta)$ represents a particular associated Legendre polynomial of degree n and order m. These polynomials are functions of the colatitude θ . The Gauss coefficients are slowly varying functions of time and are expressed in the form:

$$g_{nm}(\tau) = g_{nm}(T_{EPOCH}) + \dot{g}_{nm}(\tau - T_{EPOCH})$$
 (2a)

$$h_{nm}(\tau) = h_{nm}(T_{EPOCH}) + \dot{h}_{nm}(\tau - T_{EPOCH})$$
 (2b)

where T_{EPOCH} is the base epoch of the model, which for WMM-90 is 1990.0. Thus, $g_{nm}(T_{EPOCH})$ and $h_{nm}(T_{EPOCH})$ are the Gauss coefficients of the WMM at the model's base epoch, while \dot{g}_{nm} and \dot{h}_{nm} (pronounced g_{nm} dot and h_{nm} dot) are the annual rates of change of the Gauss coefficients. The Gauss coefficients $g_{nm}(T_{EPOCH})$ and $h_{nm}(T_{EPOCH})$ and their annual rates of change are spherical harmonic coefficients. The Gauss coefficients $g_{nm}(T_{EPOCH})$ and $h_{nm}(T_{EPOCH})$ characterize the Earth's main magnetic field at the base epoch of the model, T_{EPOCH} , while \dot{g}_{nm} and \dot{h}_{nm} characterize the

secular change of the Earth's main magnetic field during the 5-year life of the model. These coefficients, up to degree and order 12 for the main field and up to degree and order 8 for the secular variation of the main field, comprise the WMM. Currently, the secular variation model from degree 8 through degree 12 is padded with zeros.

The Earth's magnetic field $\overrightarrow{B}(r,\theta,\phi,\tau)$ is a vector quantity having three components which correspond to the projection of the magnetic field vector onto the three coordinate axes. Thus, $B_r(r,\theta,\phi,\tau)$ is that portion of the field pointing in the radial direction (i.e., perpendicular to the surface of the Earth), $B_{\theta}(r,\theta,\phi,\tau)$ is that portion of the field pointing locally due south, and $B_{\phi}(r,\theta,\phi,\tau)$ is that portion of the field pointing locally due east. The magnetic field vector can be computed from the geomagnetic potential by taking its gradient, thus:

$$\vec{B}(r,\theta,\phi,\tau) = -\vec{\nabla}V(r,\theta,\phi,\tau) \tag{3}$$

Consequently, the magnetic field components are related to the geomagnetic potential as follows:

$$B_r(r,\theta,\phi,\tau) = -\frac{\partial V(r,\theta,\phi,\tau)}{\partial r}$$
 (4a)

$$B_{\theta}(r,\theta,\phi,\tau) = -\frac{1}{r} \frac{\partial V(r,\theta,\phi,\tau)}{\partial \theta}$$
 (4b)

$$B_{\phi}(r,\theta,\phi,\tau) = -\frac{1}{r\sin\theta} \frac{\partial V(r,\theta,\phi,\tau)}{\partial \phi}$$
 (4c)

which yield the following spherical harmonic expansions:

$$B_r(r,\theta,\phi,\tau) = \sum_{n=1}^{N} (n+1) \left(\frac{R_E}{r}\right)^{n+2} \sum_{m=0}^{n} \{g_{nm}(\tau)\cos m\phi + h_{nm}(\tau)\sin m\phi\} P_n^m(\theta)$$
 (5a)

$$B_{\theta}(r,\theta,\phi,\tau) = -\sum_{n=1}^{N} \left(\frac{R_E}{r}\right)^{n+2} \sum_{m=0}^{n} \left\{g_{nm}(\tau)\cos m\phi + h_{nm}(\tau)\sin m\phi\right\} \frac{dP_n^m(\theta)}{d\theta}$$
 (5b)

$$B_{\phi}(r,\theta,\phi,\tau) = \frac{1}{\sin\theta} \sum_{n=1}^{N} \left(\frac{R_E}{r}\right)^{n+2} \sum_{m=0}^{n} m\{g_{nm}(\tau)\sin m\phi - h_{nm}(\tau)\cos m\phi\} P_n^m(\theta)$$
 (5c)

It must be noted that the Gauss coefficients $g_{nm}(\tau)$ and $h_{nm}(\tau)$, as well as the associated Legendre polynomials and their derivatives, are Schmidt normalized by an international agreement (circa 1930) of the International Union of Geodesy and Geophysics. This particular

normalization allows one to determine which terms of the spherical harmonic model are the most significant simply by a cursory inspection of the model coefficients. The Schmidt-normalized associated Legendre Polynomials $P_n^m(\theta)$ are related to the unnormalized associated Legendre Polynomials $P_n^{nm}(\theta)$ (note position of indices) by the following relation:

$$P_n^m(\theta) = S^{nm} P^{nm}(\theta) \tag{6}$$

The Schmidt normalization factors S^{nm} and the unnormalized associated Legendre Polynomials $P^{nm}(\theta)$ are computed via recurrence relationships as follows:

$$P^{\infty}(\theta) = 1 \tag{7a}$$

$$P^{nm}(\theta) = \sin \theta P^{n-1,m-1}(\theta) \qquad m = n \neq 0$$
 (7b)

$$P^{nm}(\theta) = \cos \theta P^{n-1,m} - \kappa^{nm} P^{n-2,m} \qquad m \neq n, n \ge 1$$
 (7c)

$$\frac{dP^{\infty}(\theta)}{d\theta} = 0 \tag{7d}$$

$$\frac{dP^{nm}(\theta)}{d\theta} = \sin\theta \quad \frac{dP^{n-1,m-1}(\theta)}{d\theta} + \cos\theta P^{n-1,m-1}(\theta) \qquad , m = n \neq 0$$
 (7e)

$$\frac{dP^{nm}(\theta)}{d\theta} = \cos\theta \frac{dP^{n-1,m}}{d\theta} - \sin\theta P^{n-1,m}(\theta) - \kappa^{nm} \frac{dP^{n-2,m}}{d\theta} , m \neq n, n \geq 1$$
 (7f)

where:

$$\kappa^{nm} = \frac{(n-1)^2 - m^2}{(2n-1)(2n-3)} \tag{8}$$

and where it is understood that the undefined polynomials $P^{-1,0}(\theta)$ and $\frac{dP^{-1,0}}{d\theta}(\theta)$ are to be set equal to zero. Similarly,

$$S^{\infty} = 1 \tag{9a}$$

$$S^{no} = \left(\frac{2n-1}{n}\right) S^{n-1,0} \qquad , n > 0$$

$$S^{nm} = \sqrt{\frac{(n-m+1)J}{n+m}} S^{n,m-1}, \qquad \begin{cases} J=2 & for & m=1\\ J=1 & for & m>1 \end{cases}$$
 (9c)

Also, computed via recursion relations are the longitudinally dependent functions $cos(m\phi)$ and $sin(m\phi)$, which are computed as follows:

$$\sin(m\phi) = 0 \qquad , m = 0 \tag{10a}$$

$$\cos(m\phi) = 1 \qquad , m = 0 \tag{10b}$$

$$\sin(m\phi) = \sin(\phi)\cos(m-1)\phi + \cos(\phi)\sin(m-1)\phi , m > 0$$
 (10c)

$$\cos(m\phi) = \cos(\phi)\cos(m-1)\phi - \sin(\phi)\sin(m-1)\phi , m > 0$$
 (10d)

1.2 Coordinate Transformations

GEOMAG is intended to compute various components of the geomagnetic field in a geodetic coordinate system that uses the WGS-84 ellipsoid as the reference ellipsoid. However, the mathematical analysis in the previous section is based on spherical coordinates. Consequently, some coordinate transformations are necessary. A three-step procedure is required.

- a. Convert the geodetic latitude, longitude, and altitude (λ, ϕ, h) to spherical coordinates (r, θ, ϕ) .
- b. Compute the magnetic field components $B_r(r,\theta,\phi,\tau)$, $B_\theta(r,\theta,\phi,\tau)$, and $B_\phi(r,\theta,\phi,\tau)$.
- c. Rotate the magnetic field components from spherical coordinates to geodetic coordinates yielding the magnetic field components $B_X(\lambda, \phi, h, \tau)$, $B_Y(\lambda, \phi, h, \tau)$, and $B_Z(\lambda, \phi, h, \tau)$, which are the projections of the magnetic field vector $\overrightarrow{B}(\lambda, \phi, h, \tau)$ onto the X-north, Y-east, and Z-vertically down coordinates of a local rectangular coordinate system defined by the tangent plane to the ellipsoid which is concentric about the WGS-84 reference ellipsoid but which encompasses the point (λ, ϕ, h) .

The transformations in step a are as follows:

$$\cos\theta = \frac{\sin\lambda}{\sqrt{Q^2\cos^2\lambda + \sin^2\lambda}}$$
 (11a)

$$\sin\theta = \sqrt{1 - \cos^2\theta} \tag{11b}$$

where, if a and b are respectively the semi-major and semi-minor axes of the WGS-84 ellipsoid:

$$Q = \frac{h\sqrt{a^2 - (a^2 - b^2)\sin^2\lambda} + a^2}{h\sqrt{a^2 - (a^2 - b^2)\sin^2\lambda} + b^2}$$
(12)

Furthermore:

$$r^{2} = h^{2} + 2h\sqrt{a^{2}(a^{2} - b^{2})\sin^{2}\lambda} + \frac{a^{4} - (a^{4} - b^{4})\sin^{2}\lambda}{a^{2} - (a^{2} - b^{2})\sin^{2}\lambda}$$
(13)

The transformation in step c depends on the rotation angle α through which the magnetic field vector must be rotated in going from spherical to geodetic coordinates. This rotation angle is defined by the following rotations:

$$\cos \alpha = \{h + \sqrt{a^2 \cos^2 \lambda + b^2 \sin^2 \lambda} \}/r$$
 (14a)

$$\sin \alpha = (a^2 - b^2)\cos \lambda \sin \lambda / \{r \sqrt{a^2 \cos^2 \lambda + b^2 \sin^2 \lambda} \}$$
 (14b)

$$\alpha = \lambda - \frac{\pi}{2} + \theta \tag{14c}$$

Consequently, the components of the magnetic field vector in geodetic coordinates may be computed as follows:

$$B_{\nu}(\lambda, \phi, h, \tau) = -\cos \alpha B_{\theta}(r, \theta, \phi, \tau) - \sin \alpha B_{r}(r, \theta, \phi, \tau)$$
 (15a)

$$B_{\gamma}(\lambda, \phi, h, \tau) = B_{\phi}(r, \theta, \phi, \tau) \tag{15b}$$

$$B_2(\lambda, \phi, h, \tau) = \sin \alpha B_{\theta}(r, \theta, \phi, \tau) - \cos \alpha B_r(r, \theta, \phi, \tau)$$
 (15c)

From these rectangular components of the geomagnetic field, it is possible to construct all others. In particular, the following parameters may be computed:

$$B_{\mu}(\lambda, \phi, h, \tau) = \sqrt{B_{\nu}^{2}(\lambda, \phi, h, \tau) + B_{\nu}^{2}(\lambda, \phi, h, \tau)}$$
 (Horizontal Intensity) (16a)

$$B_F(\lambda, \phi, h, \tau) = \sqrt{B_H^2(\lambda, \phi, h, \tau) + B_Z^2(\lambda, \phi, h, \tau)}$$
 (Total Intensity) (16b)

$$B_D(\lambda, \phi, h, \tau) = \tan^{-1} \left\{ \frac{B_Y(\lambda, \phi, h, \tau)}{B_X(\lambda, \phi, h, \tau)} \right\}$$
 (Declination) (16c)

$$B_{I}(\lambda, \phi, h, \tau) = \tan^{-1} \left\{ \frac{B_{Z}(\lambda, \phi, h, \tau)}{B_{H}(\lambda, \phi, h, \tau)} \right\}$$
 (Inclination) (16d)

$$B_{G}(\lambda, \phi, h, \tau) = \begin{cases} B_{D} - \phi & \lambda \ge 0 \\ B_{D} + \phi & \lambda < 0 \end{cases}$$
 (Grid Variation) (16e)

1.3 The Computer Algorithm

The Gauss coefficients at the base epoch, T_{EPOCH} , are stored in array C so that the lower half of array C is occupied by the even harmonic Gauss coefficients $g_{nm}(T_{EPOCH})$, while the upper half of array C is occupied by the odd harmonic Gauss coefficients $h_{nm}(T_{EPOCH})$. Table 1 illustrates the details of the storage scheme, which is equivalent to the following mathematical assignments:

$$C_{nm} = \begin{cases} g_{nm} & , m \le n \\ h_{m,n+1} & , m > n \end{cases}$$
 (17)

which implies that:

$$g_{nm} = C_{nm} , m \le n$$
 (18a)

$$h_{nm} = C_{m-1,n}$$
 , $m \le n, m \ne 0$ (18b)

The annual rates of change of the Gauss coefficients are stored in array CD (which stands for C) so that the lower half of array CD is occupied by the even harmonic coefficients g_{nm} , while the upper half of the array is occupied by the odd harmonic coefficients \dot{h}_{nm} . Table 2 illustrates the details of the storage scheme for array CD. It is essentially the same as table 1 for array C and corresponds to the following mathematical assignments:

$$\dot{C}_{nm} = \begin{cases} \dot{g}_{nm} & , m \le n \\ \dot{h}_{m,n+1} & , m > n \end{cases}$$
(19)

which implies that:

$$\dot{g}_{nm} = \dot{C}_{nm} \qquad , m \le n \tag{20a}$$

$$\dot{h}_{nm} = \dot{C}_{m-1,n}, \quad , m \le n, m \ne 0$$
 (20b)

TABLE 1. ARRANGEMENT OF MAIN FIELD COEFFICIENTS IN ARRAY $C_{\scriptscriptstyle{\mathsf{AM}}}$

n\m	0	1	2	3	4	5	6	7	8	9	10	11	12
0	800	h_{11}	h_{21}	h ₃₁	h ₄₁	h ₅₁	h ₆₁	<i>h</i> ₇₁	h ₈₁	h ₉₁	$h_{10,1}$	$h_{11,1}$	$h_{12,1}$
1	g 10	g 11	h ₂₂	h ₃₂	h ₄₂	h ₅₂	h ₆₂	h ₇₂	h ₈₂	h ₉₂	h _{10,2}	$h_{11,2}$	h _{12,2}
2	820	g ₂₁	822	h ₃₃	h ₄₃	h ₅₃	h ₆₃	h ₇₃	h ₈₃	h ₉₃	h _{10,3}	$h_{11,3}$	$h_{12,3}$
3	8 30	g ₃₁	g ₃₂	833	h ₄₄	h ₅₄	h ₆₄	h ₇₄	h ₈₄	h ₉₄	h _{10,4}	h _{11,4}	$h_{12,4}$
4	840	841	842	g ₄₃	844	h ₅₅	h ₆₅	h ₇₅	h ₈₅	h ₉₅	h _{10,5}	h _{11,5}	h _{12,5}
5	8 50	8 51	852	853	854	855	h ₆₆	h ₇₆	h ₈₆	h ₉₆	h _{10,6}	h _{11,6}	h _{12,6}
6	860	861	g ₆₂	863	864	865	866	h ₇₇	h ₈₇	h ₉₇	h _{10,7}	h _{11,7}	$h_{12,7}$
7	<i>8</i> 70	g ₇₁	g ₇₂	873	874	875	876	877	h ₈₈	h ₉₈	h _{10,8}	h _{11,8}	h _{12,8}
8	880	g ₈₁	g ₈₂	883	884	885	886	887	g ₈₈	h ₉₉	h _{10,9}	h _{11,9}	h _{12,9}
9	890	891	892	g ₉₃	894	895	8%	897	g ₉₈	899	h _{10,10}	h _{11,10}	h _{12,10}
10	g _{10,0}	810,1	g _{10,2}	810,3	810,4	g _{10,5}	810,6	810,7	g _{10,8}	810,9	810,10	$h_{11,11}$	h _{12,11}
11	g _{11,0}	g _{11,1}	g _{11,2}	g _{11,3}	g _{11,4}	g _{11,5}	811,6	811,7	g 11,8	g 11,9	811,10	811,11	h _{12,12}
12	g _{12,0}	g _{12,1}	g _{12,2}	g _{12,3}	g _{12,4}	812,5	g _{12,6}	g _{12,7}	812,8	g _{12,9}	812,10	g _{12,11}	812,12

n/m	0	1	2	3	4	5	6	7	8	9	10	11	12
0	ġ ₀₀	\dot{h}_{11}	\dot{h}_{21}	\dot{h}_{31}	\dot{h}_{41}	<i>h</i> ₅₁	Й ₆₁	<i>h</i> ₇₁	h ₈₁	h ₉₁	$\dot{h}_{10,1}$	$\dot{h}_{11,1}$	$\dot{h}_{12,1}$
1	ġ 10	ġ 11	h ₂₂	<i>h</i> ₃₂	h ₄₂	h ₅₂	<i>h</i> ₆₂	h ₇₂	h ₈₂	h ₉₂	$\dot{h}_{10,2}$	$\dot{h}_{1i,2}$	$\dot{h}_{12,2}$
2	\$ 20	ġ ₂₁	ġ 22	\dot{h}_{33}	<i>h</i> ₄₃	h 53	h 63	<i>h</i> ₇₃	<i>h</i> ₈₃	\dot{h}_{93}	$\dot{h}_{10,3}$	$\dot{h}_{11,3}$	$\dot{h}_{12,3}$
3	ġ 30	ġ 31	ġ ₃₂	ġ 33	h ₄₄	h ₅₄	h ₆₄	h ₇₄	h ₈₄	h ₉₄	$\dot{h}_{10,4}$	$\dot{h}_{11,4}$	$\dot{h}_{12,4}$
4	ģ ₄₀	ģ ₄₁	ġ 42	ġ 43	ģ 44	h 55	h ₆₅	h ₇₅	h ₈₅	Н ₉₅	<i>h</i> _{10,5}	$\dot{h}_{11,5}$	$\dot{h}_{12,5}$
5	ġ 50	ġ 51	ġ 52	ġ 53	ġ 54	ģ 55	h	h ₇₆	h ₈₆	<i>h</i> %	<i>h</i> _{10,6}	$\dot{h}_{11,6}$	$\dot{h}_{12,6}$
6	ġ 60	ġ 61	ġ ₆₂	ġ 63	ġ 64	ġ 65	ġ 66	h ₇₇	Й ₈₇	h ₉₇	À 10,7	$\dot{h}_{11,7}$	$\dot{h}_{12,7}$
7	ġ 70	ġ 71	ġ ₇₂	ġ 73	ġ 74	ġ 75	ġ 76	ġ 77	\dot{h}_{88}	h ₉₈	$\dot{h}_{10,8}$	$\dot{h}_{11,8}$	$\dot{h}_{12,8}$
8	ġ 80	ġ ₈₁	ģ ₈₂	ģ ₈₃	ġ ₈₄	ġ 85	ġ 86	ġ ₈₇	ġ 88	h ₉₉	$\dot{h}_{10,9}$	$\dot{h}_{11,9}$	$\dot{h}_{12,9}$
9	ġ ₉₀	ġ 91	ġ ₉₂	ģ ₉₃	\$ 94	ġ 95	ġ _%	ġ ₉₇	ġ 98	ġ 99	$\dot{h}_{10,10}$	$\dot{h}_{11,10}$	$\dot{h}_{12,10}$
10	\$ 10,0	છે 10, 1	ġ 10,2	છે 10,3	ġ 10,4	\$ 10,5	છે 10,6	ġ _{10,7}	ġ 10,8	. 10,9	ġ _{10,10}	$\dot{h}_{11,11}$	h 12,11
11	ġ 11,0	ģ 11,1	ġ 11,2	ġ 11,3	ġ 11,4	ģ 11,5	ġ _{11,6}	ġ 11,7	ġ _{11,8}	Ė 11,9	ġ _{11,10}	ġ 11,11	$\dot{h}_{12,12}$
12	ġ _{12,0}	છે 12,1	ġ _{12,2}	ģ 12,3	ġ 12,4	ġ 12,5	ġ 12,6	ġ _{12,7}	ġ _{12,8}	ġ 12,9	ġ _{12,10}	ġ 12,11	ġ 12,12

The numerical values of the Gauss coefficients at the base epoch and their corresponding annual rates of change for the WMM-90 geomagnetic model are listed in table 3. These numerical values are inserted into arrays C and CD through data statements. The base epoch of the model is also assigned through a data statement. In order to update the GEOMAG algorithm to a new epoch geomagnetic model such as WMM-95, it is necessary to replace only the data statements with the new model coefficients and the new base epoch.

Important parameters in the GEOMAG routine and their mathematical correspondences are:

```
A \sim a = 6378.137 \ km
B \sim b = 6356.7523142 \text{ km}
RE \sim R_E = 6371.2 \ km
TIME \sim \tau
EPOCH \sim T_{EPOCH}
DT \sim \tau - T_{EPOCH}
ALT \sim h
SNORM(N,M) \sim S^{nm}
K(N,M) \sim \kappa^{NR}
GLAT \sim \lambda
GLON ~ 0
SP(M) \sim \sin(m\phi)
CP(M) \sim \cos(m\phi)
ST \sim \sin(\theta)
CT \sim \cos(\theta)
CA \sim \cos(\alpha)
SA \sim \sin(\alpha)
BR \sim B.
    ~ B<sub>e</sub>
RT
BP \sim B_{\bullet}
BX \sim B_{x}
BY \sim B_{Y}
BZ \sim B_z
BH \sim B_H
DEC \sim B_D
DIP \sim B_I
TI \sim B_{TI}
MAXDEG ~ N
MAXORD \sim M = N
P(N,M) \sim P^{nm}
DP(N,M) \sim \frac{dP^{mn}}{dr}
```

$$TC \sim C + (\tau - T_{EPOCH}) \dot{C}$$
 $CD \sim \dot{C}$
 $Q2 \sim Q^2$

Note that $R_{\rm E}$ is not intended to be the mean radius of the WGS-84 ellipsoid. It is the mean radius of a modified IAU-66 ellipsoid.

The GEOMAG algorithm is organized into two modules, each with its own entry point. The first is an Initialization Module. Its purpose i 5 to compute all constants such as the recursion relation factors for the associated Legendre polynomials K^{LM} , the Schmidt normalization factors S^{LM} , and any other parameters that do not depend on position or time. The entry point for this module is GEOMAG (MAXDEG). The parameter MAXDEG determines the maximum degree and order of the magnetic model to be used in the computations. Normally, MAXDEG = 12, which is the maximum degree and order of the WMM series geomagnetic models. In order to reduce computation time, MAXDEG may be set to a number less than 12 (e.g., 8 or 10). However, the accuracy of the computed magnetic parameters is correspondingly reduced. MAXDEG must be set in the calling program. The second module is the Processing Module, which has the entry point

GEOMG1 (ALT, GLAT, GLON, TIME, DEC, DIP, TI, GV).

The purpose of this module is to compute the magnetic declination, inclination, total intensity, and grid variation of each geodetic position and time supplied to it. The units of the parameters in the argument list of the GEOMG1 entry point are as follows:

ALT ~ kilometers (e.g., 5.314)	(In)
GLAT ~ degrees (e.g., 33.716)	(In)
GLON ~ degrees (e.g., -163.315)	(In)
TIME ~ years (e.g., 1992.427)	(In)
DEC ~ degrees (e.g., -121.734)	(Out)
DIP ~ degrees (e.g., 48.387)	(Out)
TI ~ nanoteslas (e.g., 35781.7)	(Out)
GV ~ degrees (e.g., 51.768)	(Out)

The computed magnetic field parameters are referenced to the WGS-84 ellipsoid. The last parameter, GV, is the grid variation which is computed only in the polar regions (i.e., above + 55° latitude or below - 55° latitude). Outside of this region, a value of -999.0 is dummied in. It is referenced to grid north of a polar stereographic projection. The model is considered valid at altitudes ranging from sea level to 1000 km.

TABLE 3. WMM-90 SCHMIDT NORMALIZED GAUSS COEFFICIENTS (nT)

n	m	8 _{nm}	h _{nm}	ġ nm	h _{мм}
1122233334444455555566666667777777777888888888888	01012012301234012345012345601234567012345678	-29780.5 -1851.7 -2134.3 3062.2 1691.9 1312.9 -1244.7 1246.8 808.6 933.7 1246.8 808.5 784.9 323.7 139.2 -208.3 352.2 246.8 -162.3 -37.0 60.3 -181.3 -62.1 30.7 7.9 10.9 21.7 -17.5 2.7 -17	-19.3 6.6 -20.1 13.4	16.0 9.3 -11.7 3.7 1.8 2.1 -7.6 0.0 -5.8 1.0 -7.4 1.7 0.0 -2.7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	.0 -13.8 .0 -12.8 -14.9 .0 3.1 .8 -11.3 .0 3.3 3.7 2.8 .0 .0 -2.1 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.0 6 6 6 6 0 0 0 0 0 0 0 0 0 0

TABLE 3. WMM-90 SCHMIDT NORMALIZED GAUSS COEFFICIENTS (con.)

n	m	8 п.т	h _{am}	ġ nm	h _{лт}
9 9 9 9 9 9 9 9 9 9 9 10 10 10 10 10 10 11 11 11 11 11 11 11	012345678901234567890012345678901101234567890112	3.65 9.97 10.72 10.38 10.53 10.5	.09 14.35 -6.4 9.57 -6.4 9.01 9.62 -6.70 -1.78 -6.50 -1.60 -1.77 -1.53 -1.22 -1.22 -1.36 -1.22 -1.36 -	000000000000000000000000000000000000000	000000000000000000000000000000000000000

SECTION 2. THE 1990 EPOCH WORLD MAGNETIC MODEL (DERIVATION)

2.0 Overview

There were four major data sets available for the 1990 model. These were: the MAGSAT satellite data collected during 1979 and 1980; the DE-2 satellite data collected from 1981 through 1983; Project MAGNET aeromagnetic data collected between 1980 and 1990; and geomagnetic observatory annual magnetic means data collected between 1980 and 1990. The global distribution of these data is illustrated in charts 1 through 4.

Four factors which affect the quality of the model produced and which influence the overall approach taken to produce the model are:

- a. The age of the data relative to the model epoch;
- b. The temporal coherence of the data;
- c. The spatial uniformity of the data; and
- d. The data density.

With respect to these factors, none of the four data sets are ideal. All four data sets, especially the satellite data sets, are dominated by older data. The Project MAGNET data, in addition, are neither temporally coherent nor spatially uniform. Furthermore, the observatory annual means data are sparse and suffer from severe spatial nonuniformity.

The modeling objective is to create two spherical harmonic models. One model characterizes the Earth's main (core-generated) magnetic field at the 1990.0 epoch. The other model characterizes the Earth's secular (slow temporal) magnetic variations of Earth core origin for five years beyond the 1990 epoch.

Given the objective and the available data, the following procedure was adopted:

- a. Use the observatory annual magnetic means to create two definitive secular variation models, the first covering the 5-year interval 1980 to 1985, and the second covering the 5-year interval 1985 to 1990. These are referred to as the 1982.5 and 1987.5 definitive secular variation models, respectively.
- b. Use the observatory annual magnetic means to create, by extrapolation, one <u>predictive</u> secular variation model covering the 5-year interval 1990 to 1995. It is referred to as the 1992.5 predictive secular variation model.
- c. Use the two definitive secular variation models to push the satellite and aircraft magnetic field observations forward or backward, as appropriate, to 1985.0.

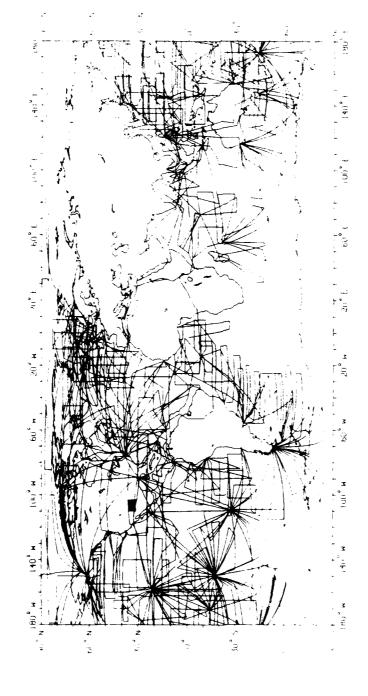


CHART 1. PROJECT MAGNET DATA DISTRIBUTION (FROM SURVEYS PERFORMED DURING THE PERIOD 1980-1989)



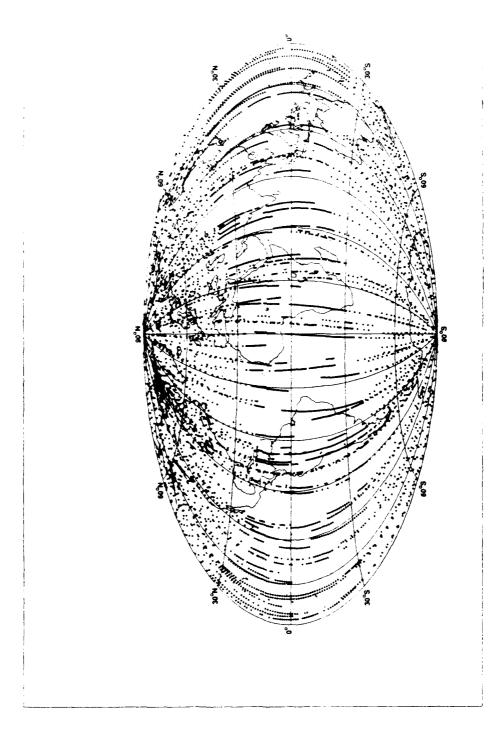


CHART 3. DE-2 DATA DISTRIBUTION

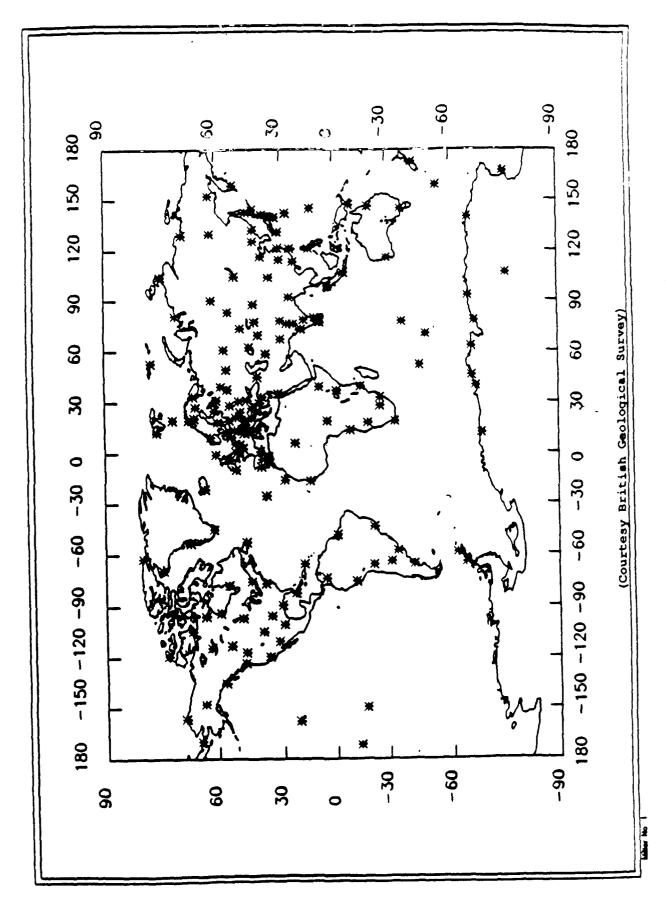


CHART 4. GEOMAGNETIC OBSERVATORY DISTRIBUTION

- d. Create a 1985.0 epoch main field model using the time-adjusted satellite and aircraft magnetic field observations via a weighted least-square inversion.
- e. Use the 1987.5 definitive secular variation model to push the spherical harmonic coefficients of the 1985.0 epoch main field model forward to the 1990.0 epoch, thereby yielding the 1990.0 epoch main field model.
- f. Combine the 1990 epoch main field model coefficients with the 1992.5 predictive secular variation model coefficients to form the 1990 World Magnetic Model, WMM-90.

A by-product of this procedure is a revised 1985.0 epoch World Chart Model which is obtained by combining the 1985.0 main field coefficients generated in step d with the 1987.5 definitive secular variation model coefficients generated in step a.

2.1 <u>Secular Variation Data Analysis</u> (British Responsibility)

The only data available for secular variation modeling are the observatory magnetic annual means, the first time derivative which provides information concerning the slow (greater than one year) rates of change of various components of the Earth's main magnetic field at various geographic locations (roughly 200) around the world. Because of the sparsity and spatial nonuniformity of this data, it is possible to generate only a degree and order 8 spherical harmonic model of the secular variation. Furthermore, the predictive model is necessarily based on extrapolations of each magnetic component at each observatory site. Examples of observatory annual means from a few selected sites such as Honolulu, Huancayo, Pilar, and Rude Skov, for the X-north, Y-east, and Z-vertically down components of the Earth's magnetic field, are given in figures (la), (lb), (lc), (ld), (1e) and (1f) through (4a), (4b), (4c), (4d), (4e) and (4f). discontinuities in the field components at Honolulu are due to repositioning of the observatory at two separate instances. In several instances, the rate of change of one or more field components at an observatory has reversed direction over time intervals as short as two or three years. The sudden, unpredictable nature of the Earth's field is well illustrated by these observatories. The first-order time derivative of these data contains magnetic field contributions from the Earth's core as well as from the ionosphere and magnetosphere. It is difficult to remove the external field effects from these data because much of it is related to the solar cycle and many observatories do not have a sufficiently long history for a detailed analysis. Consequently, some external field effects are not removed from these data at the expense of a somewhat larger uncertainty in the secular variation model coefficients.

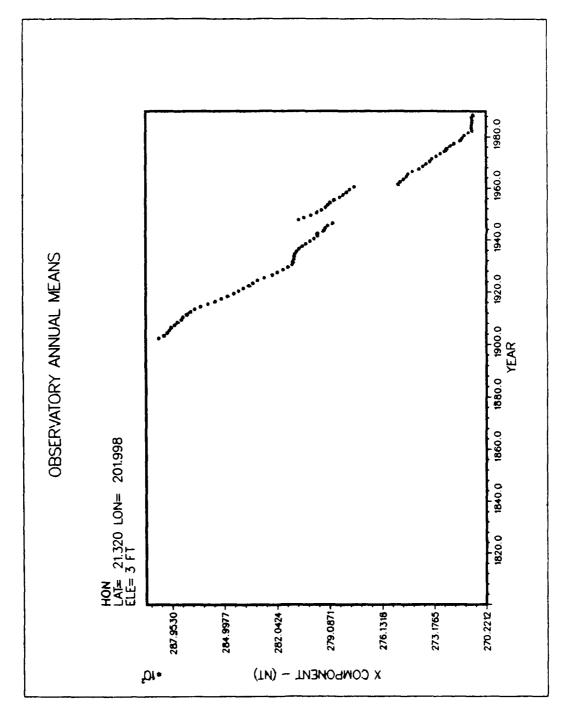


FIGURE 1a. NORTH X COMPONENT AT HONOLULU (HON).

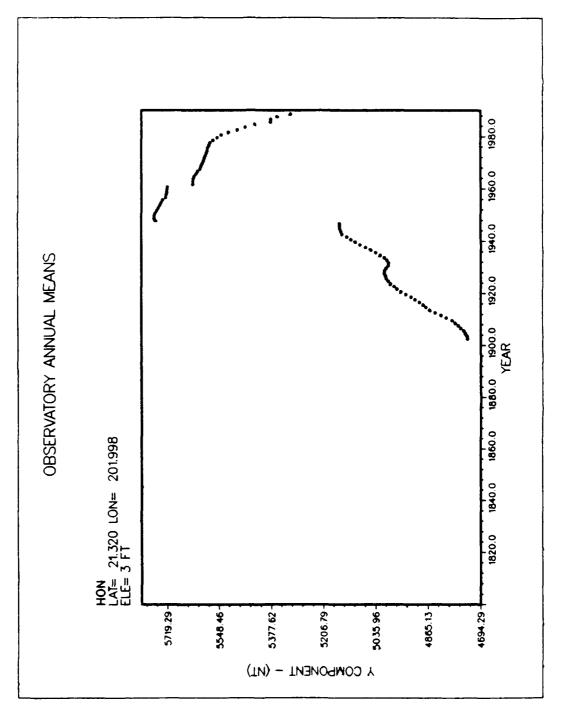


FIGURE 1b. EAST Y COMPONENT AT HONOLULU (HON).

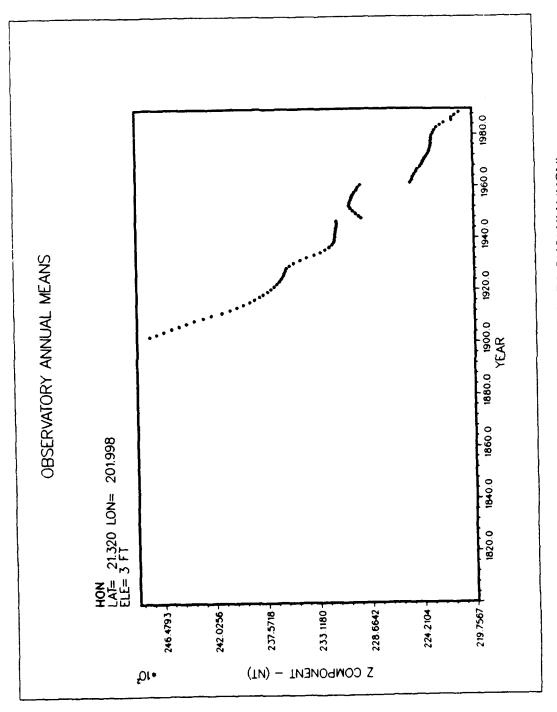


FIGURE 1c. VERTICAL Z COMPONENT AT HONOLULU (HON).

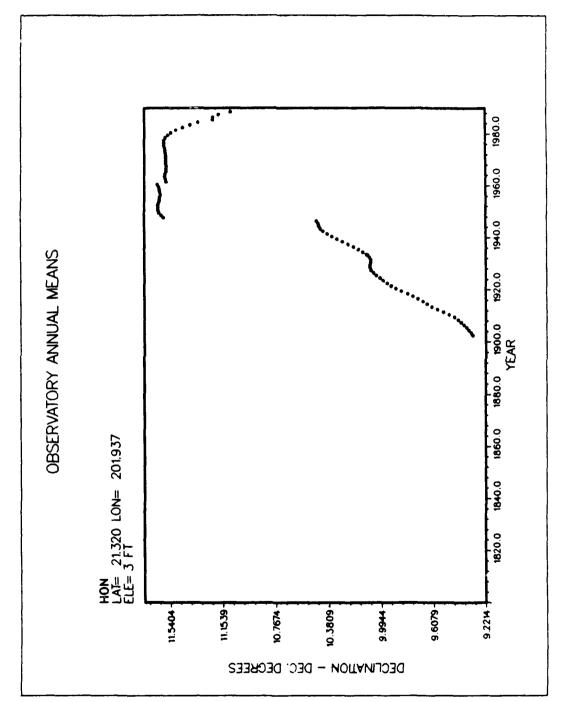


FIGURE 1d. DECLINATION D COMPONENT AT HONOLULU (HON).

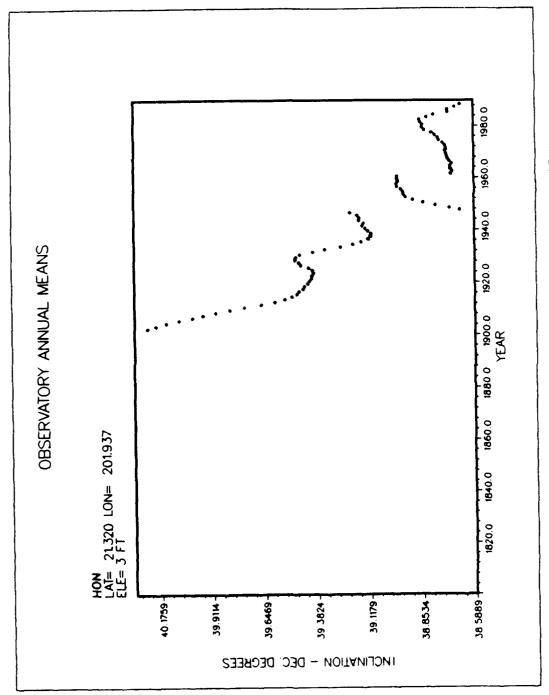


FIGURE 16. INCLINATION I COMPONENT AT HONOLULU (HON).

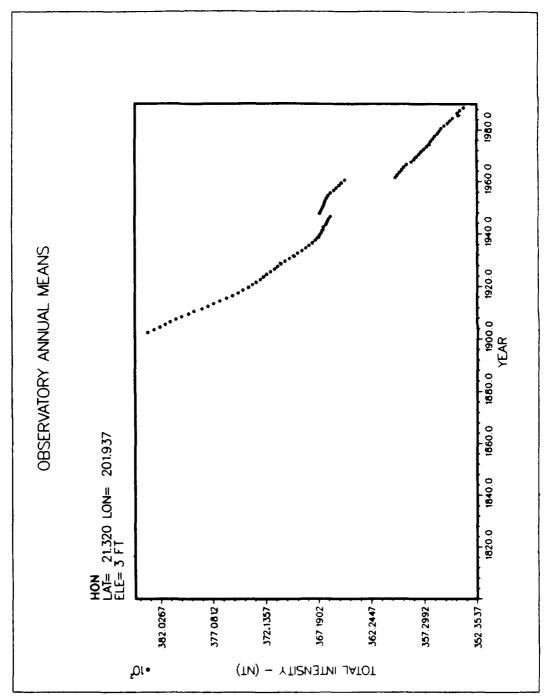


FIGURE 1f. TOTAL INTENSITY F COMPONENT AT HONOLULU (HON).

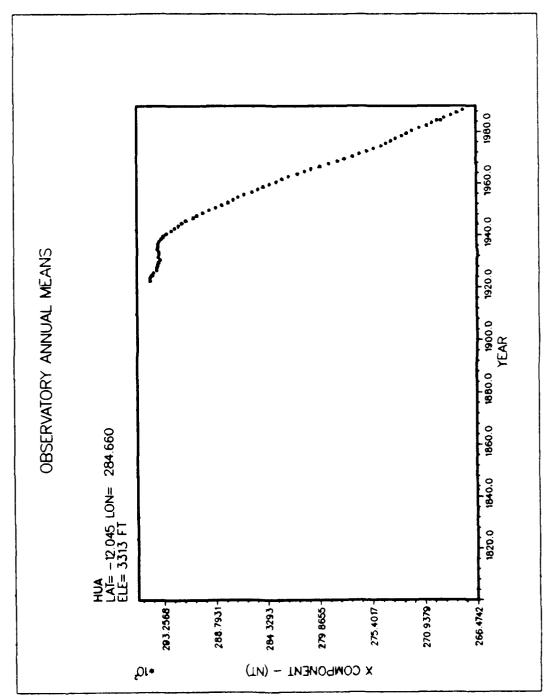


FIGURE 2a. NORTH X COMPONENT AT HUANCAYO (HIUA).

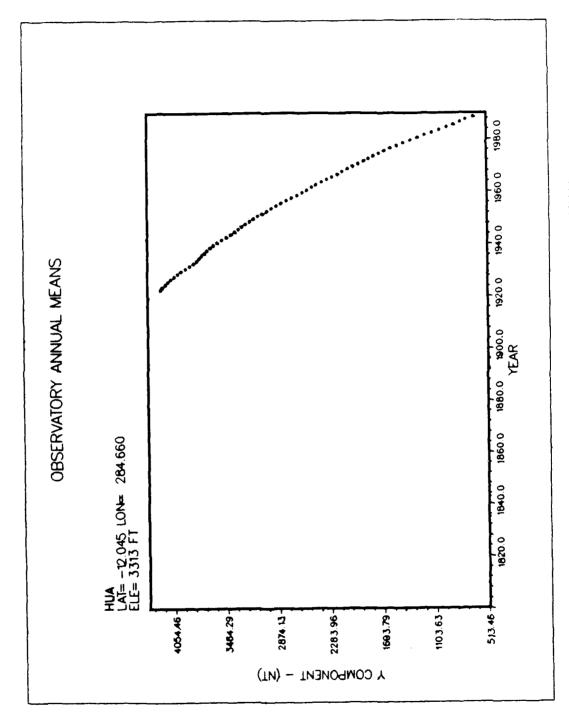


FIGURE 2b. EAST Y COMPONENT AT HUANCAYO (HUA).

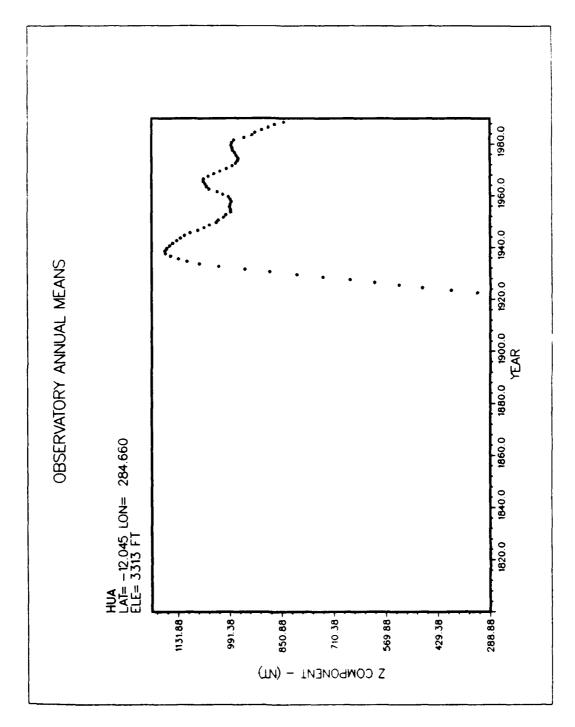


FIGURE 2c. VERTICAL Z COMPONENT AT HUANCAYO (HUA).

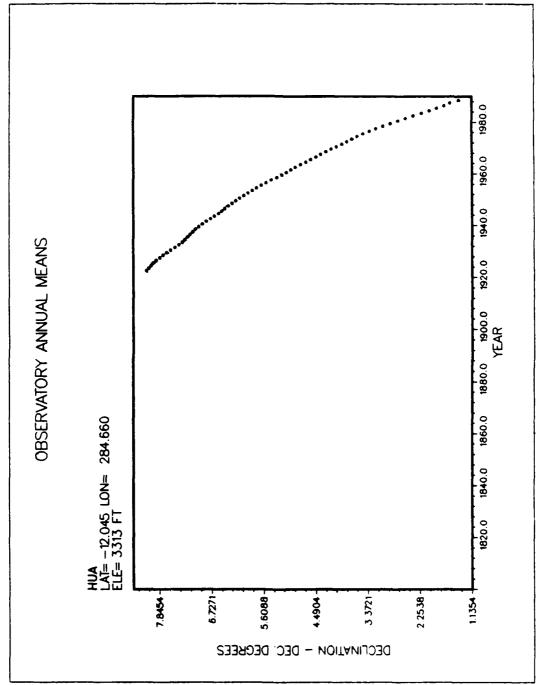


FIGURE 2d. DECLINATION D COMPONENT AT HUANGALO (HUA).

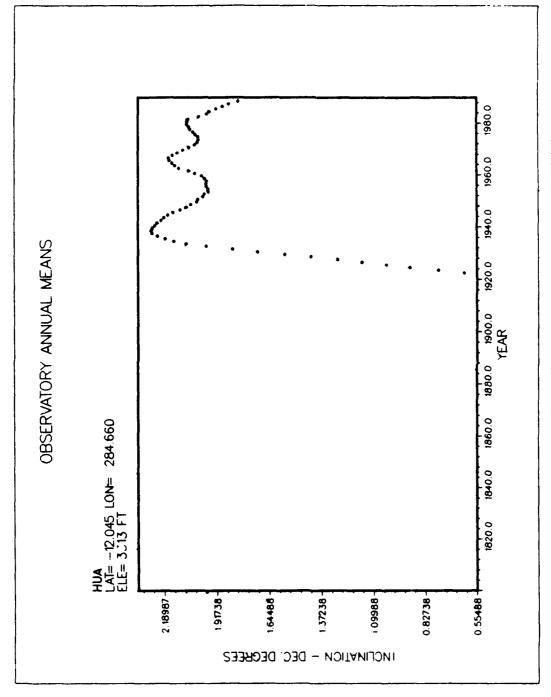


FIGURE 26. INCLINATION I COMPONENT AT HUANCAYO (HUA).

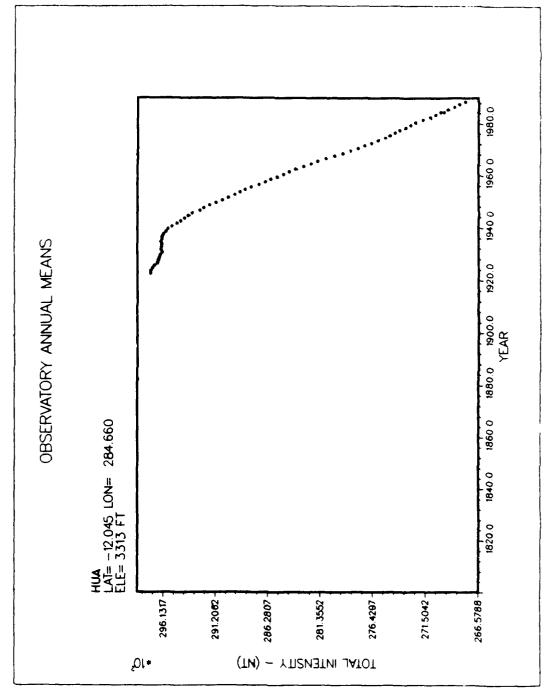


FIGURE 26. TOTAL INTENSITY F COMPONENT AT HUANCAYO (HUA).

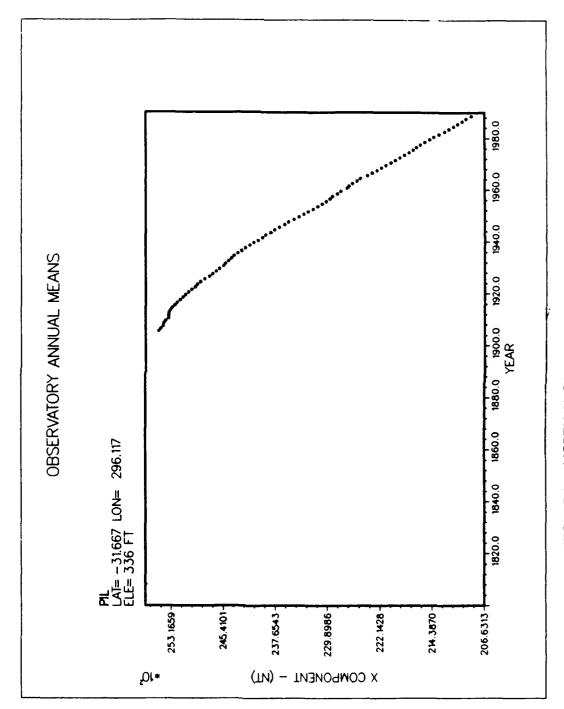


FIGURE 3a. NORTH X COMPONENT AT PILAR (PIL).

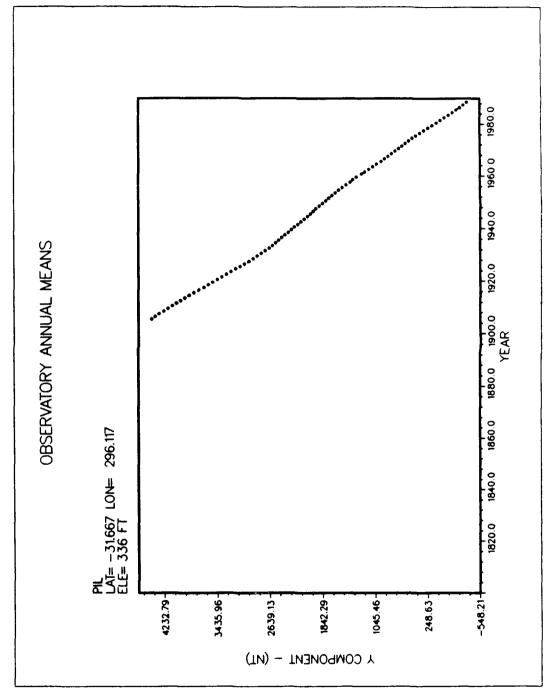


FIGURE 3b. EAST Y COMPONENT AT PILAR (PIL).

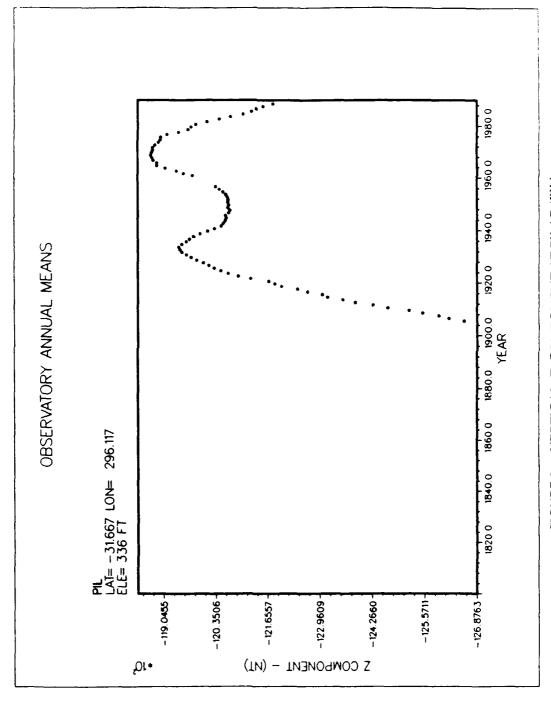


FIGURE 3c. VERTICAL Z COMPONENT AT PILAR (PIL.).

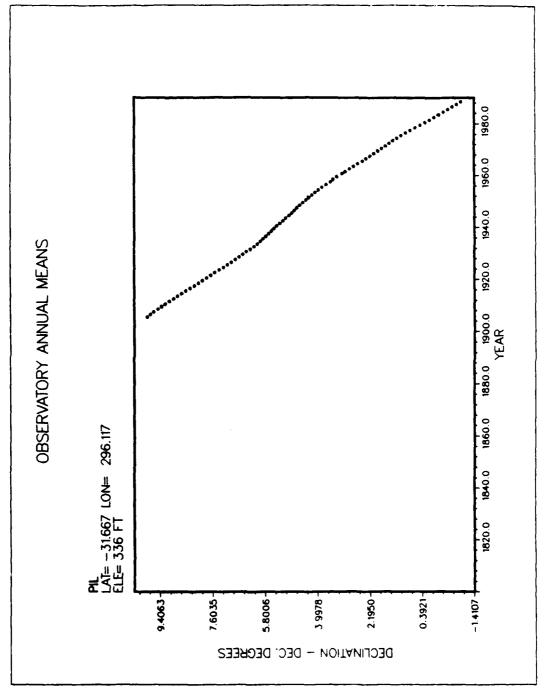


FIGURE 3d. DECLINATION D COMPONENT AT PILAR (PIL).

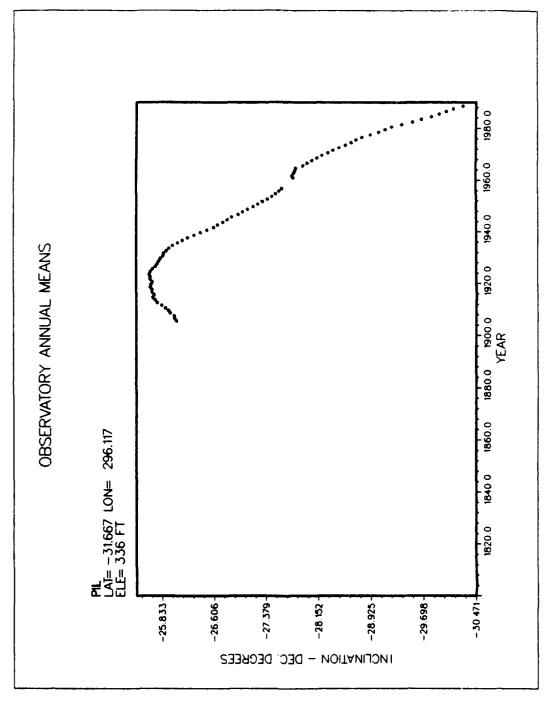


FIGURE 3e. INCLINATION I COMPONENT ATPILAR (PIL).

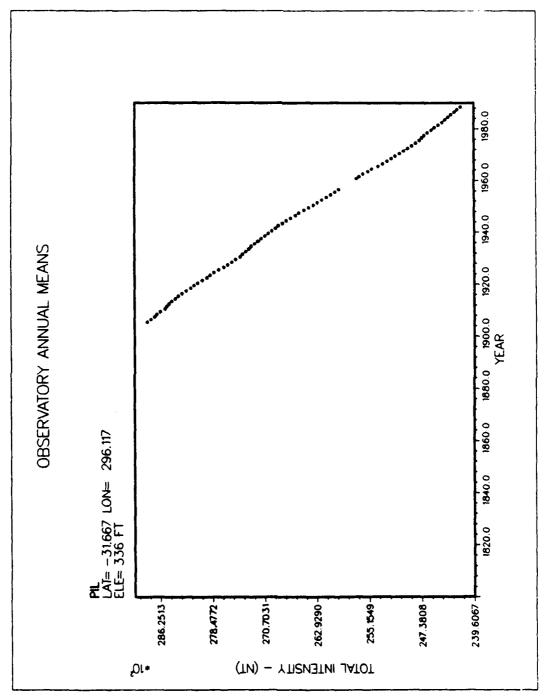


FIGURE 3f. TOTAL INTENSITY F COMPONENT AT PILAR (PIL).

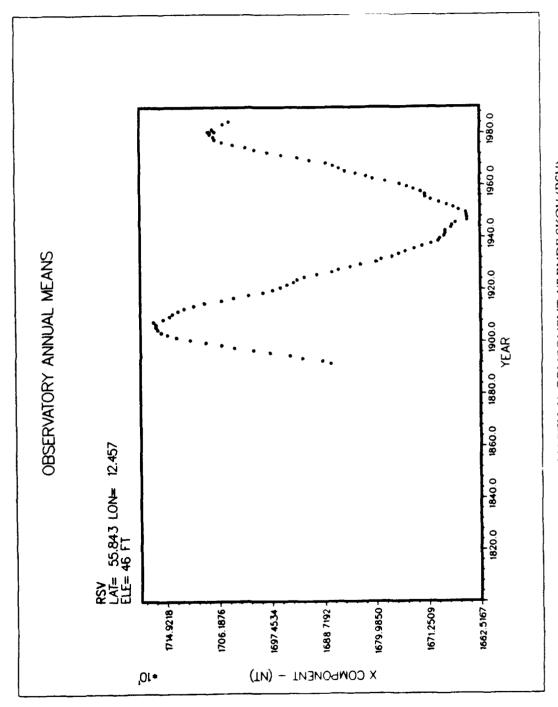


FIGURE 4a. NORTH X COMPONENT AT RUDE SKOV (RSV).

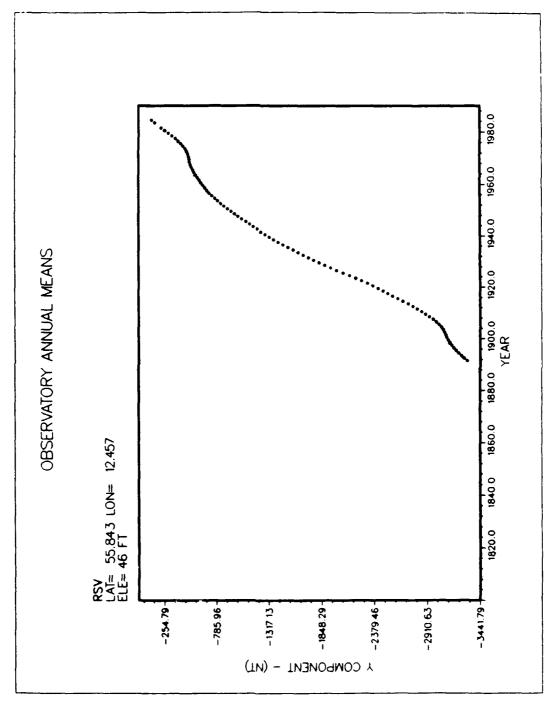


FIGURE 4b. EAST Y COMPONENT AT RUDE SKOV (RSV).

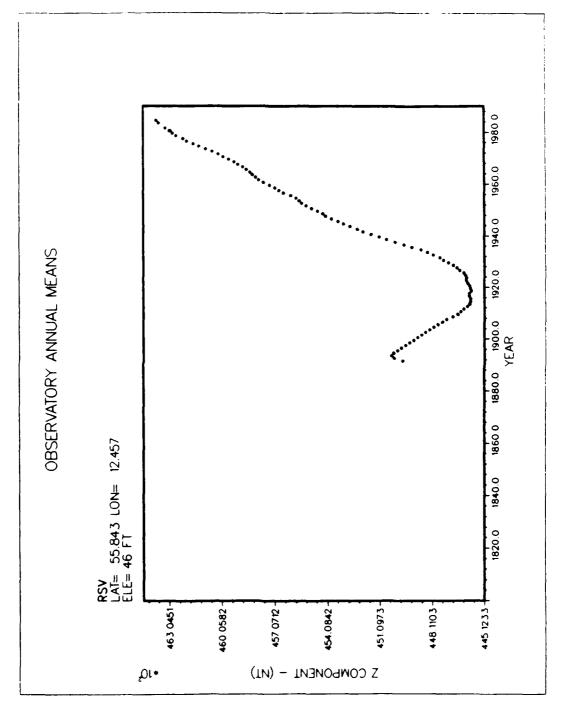


FIGURE 4c. VERTICAL Z COMPONENT AT RUDE SKOV (RSV).

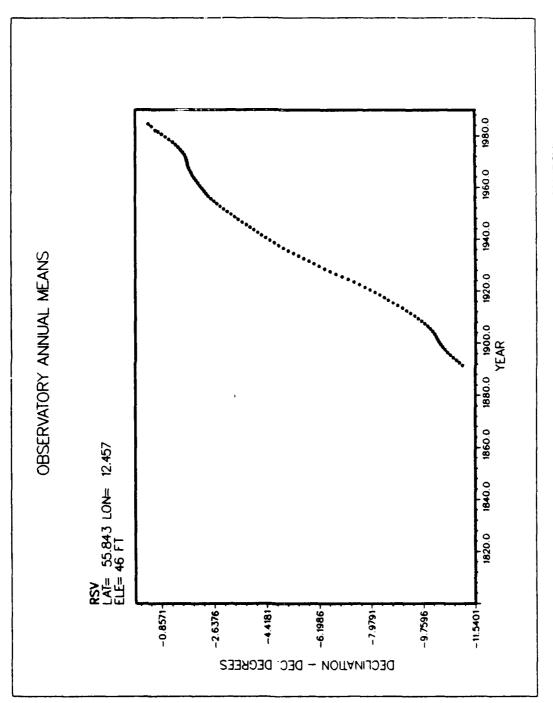


FIGURE 4d. DECLINATION D COMPONENT AT RUDE SKOV (RSV).

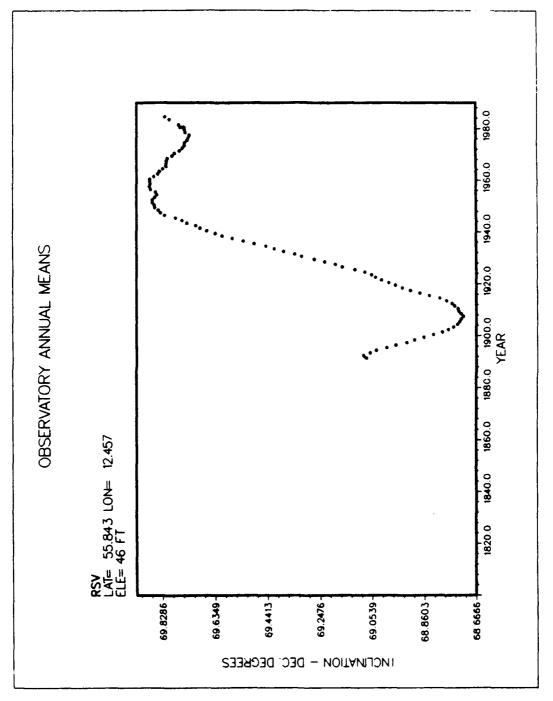


FIGURE 4e. INCLINATION I COMPONENT AT RUDE SKOV (RSV).

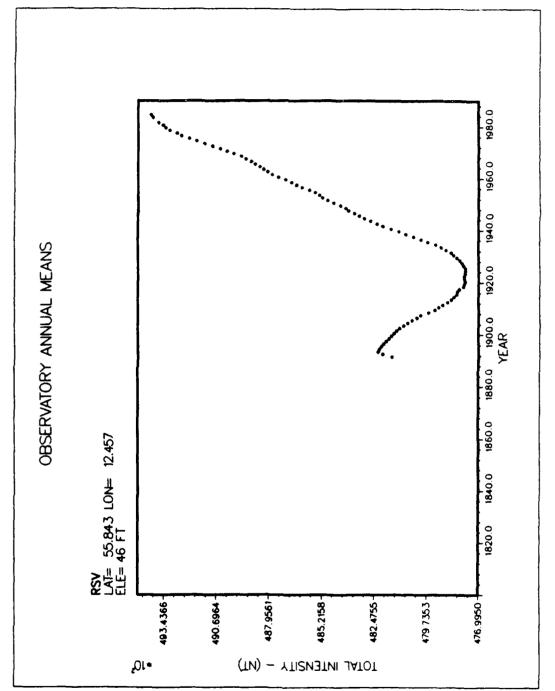


FIGURE 4f. TOTAL INTENSITY F COMPONENT AT RUDE SKOV (RSV).

Three secular variation models are generated by performing a weighted, least-square fit of the degree and order 8 spherical harmonic model to the first-order time derivative of the observatory annual means. These models were supplied by the British Geologica survey and are given in table 4.

2.2 Main Field Data Analysis (United States Respondibility)

The observatory annual magnetic means were not used in the main field modeling because those data contain, in addition to small external field contributions, some rather large local and regional magnetic biases of crustal origin. A detailed survey at each observatory site would be necessary to remove these biases. Such surveys have rarely been performed due to the prohibitive cost, logistics, and international politics involved.

The MAGSAT data consisted of 30,473 vector magnetic field values selected from 401 of the first 804 orbits. To minimize solar influences, the K_P magnetic index was required to be equal to, or less than, $2(K_P \le 2)$. These orbits were individually edited by an interactive graphics process to delete field aligned current effects and spurious data. Also, the following corrections for magnetospheric effects due to the ring current, magnetopause currents, and magnetotail currents were applied:

$$B_{x}(r,\theta,\phi,\tau) = -q_{1}^{0}(\tau)\sin\theta + \{q_{1}^{1}(\tau)\cos\phi + s_{1}^{1}(\tau)\sin\phi\}\cos\theta$$
 (21a)

$$B_{\nu}(r,\theta,\phi,\tau) = c(\tau)\sin\phi - s_{1}^{1}(\tau)\cos\phi \tag{21b}$$

$$B_{Z}(r,\theta,\phi,\tau) = q_{1}^{0}(\tau)\cos\theta + \{q_{1}^{1}(\tau)\cos\phi + s_{1}^{1}(\tau)\sin\phi\}\sin\theta$$
 (21c)

where the time-dependent coefficients are functions of the Disturbance Storm Time (Dst) index:

$$q_1^0(\tau) = 19.69 - 0.63Dst(\tau)$$
 (22a)

$$q_1^{1}(\tau) = -0.38 - 0.06Dst(\tau) \tag{22b}$$

$$s_1^1(\tau) = -2.90 + 0.17Dst(\tau)$$
 (22c)

These corrections are derived from the external magnetic field potential:

TABLE 4. SECULAR VARIATION MODELS (units: nanotesles/year)

	1982.5	Epoch	1987.5	Epoch	1992.5	Epoch
n m	ġ ^m	h™,	ġ ^m	h, ^m	ġ ^m	h'''
1 1 1 2 2 2 3 3 3 3 3 4 4 4 4 4 4 4 5 5 5 5 5 5 5 5	22.601 10.491 -14.454 3.389 5.043 2.839 -5.747 -1.857 -1.130 0.000 -6.929 0.000 -6.192 0.952 -0.577 -1.578 -3.916 0.000 1.018 0.962 0.000 1.678 0.000 1.678 0.000 1.583 0.893 0.376 -0.6457 1.583 0.893 0.000 -0.176 0.000 -0.176 0.000 -0.176 0.000 -0.842 -0.222 0.000 -0.394 -0.516	0.000 -20.091 0.000 -14.476 -20.686 0.000 4.810 3.013 -10.049 0.000 5.277 1.770 4.323 0.771 0.000 -0.402 -0.501 0.000 -1.107 -0.821 -0.954 0.349 0.456 0.000 0.223 0.321 0.375 0.880 0.000 0.459 -0.332 0.321 0.375 0.880 0.000 0.459 -0.332 0.321 0.375 0.880 0.000 0.459 -0.332 0.321 0.375	2.001 1.296 0.000 1.799 0.834 -0.667 0.000 0.663 0.670 -0.483 0.000 1.010 1.903 0.597 0.000 0.543 0.237 -0.692 -0.367 0.000 -1.292 0.000 0.423 0.000	0.000 -17.836 0.000 -15.523 -15.631 0.000 4.285 1.498 -10.351 0.000 3.375 2.994 3.812 0.000 -0.593 0.000 -0.593 0.000 -1.712 0.464 0.000 -1.277 0.000 -1.664 0.000 0.381 0.000 0.381 0.000 0.390 0.000 0.390 0.000 0.390 0.000 0.399 -0.195 0.519 0.	0.000 -0.869 1.457 2.650 -1.020 0.000 0.000 -1.089 0.000 -2.114 0.000 0.978 0.000	0.000 -13.759 0.000 -12.790 -14.865 0.000 3.082 0.844 -11.342 0.000 3.281 3.680 2.799 0.000 0.000 -2.096 1.226 1.193 0.650 0.000 -0.583 -0.644 0.000 -2.266 0.000 0.000 0.599 0.793 0.000 0.000 0.599 0.793 0.000

$$V_{ext}(r,\theta,\phi,\tau) = a \sum_{n=1}^{N_{ext}} \sum_{m=0}^{n} \left(\frac{r}{a}\right)^{n} \left\{q_{n}^{m}(\tau)\cos m\phi + s_{n}^{m}(\tau)\sin m\phi\right\} P_{n}^{m}(\cos\theta)$$
 (23)

when $N_{ext} = 1$, via the relations:

$$B_X = -B_{\theta} = \frac{1}{r} \frac{\partial V}{\partial \theta}$$
 (24a)

$$B_{\gamma} = +B_{\phi} = -\frac{1}{r\sin\theta} \frac{\partial V}{\partial \phi}$$
 (24b)

$$B_{z} = -B_{r} = \frac{\partial V}{\partial r}$$
 (240)

A further correction takes into account the magnetic fields induced in the Earth by the external fields which, because of their time dependence and the generally low but finite conductivity of the crust and mantle, induce electric currents in the crust and mantle, which in turn generate secondary magnetic fields. These secondary fields are of internal origin and primarily affect the g_1^0 coefficients of the internal magnetic potential:

$$V_{\text{int}}(r,\theta,\phi,\tau) = a \sum_{n=1}^{N_{\text{int}}} \sum_{m=0}^{n} \left(\frac{a}{r}\right)^{n+1} \{g_n^m(\tau)\cos m\phi + h_n^m(\tau)\sin m\phi\} P_n^m(\cos\theta)$$
 (25)

Taking derivatives as before with n=1 and m=0, the magnetic field corrections due to induction effects are:

$$B_{X}(r,\theta,\phi,\tau) = -\left(\frac{a}{r}\right)^{3}g_{11}^{0}(\tau)\sin\theta \qquad (26a)$$

$$B_{r}(r,\theta,\phi,\tau) = 0 (26b)$$

$$B_{z}(r,\theta,\phi,\tau) = -2 \left(\frac{a}{r}\right)^{3} g_{11}^{0}(\tau) \cos\theta \qquad (26c)$$

where the induced part of the g_1^0 coefficient is given as:

$$g_{11}^{0}(\tau) = 0.27q_{1}^{0}(\tau) \tag{27}$$

The external and induced magnetic field corrections given above were subtracted from the MAGSAT observations. These corrections are based on previous analyses of MAGSAT data by Langel and Estes (1985) and by Quinn, Kerridge, and Barraclough (1986).

No attempts were made to remove magnetic influences due to ionospheric currents such as those generated by solar quiet (SQ) currents, auroral electrojet currents, and equatorial electrojet currents, which are located below the MAGSAT orbit altitudes. These influences, though generated external to the Earth's surface, are nevertheless part of $V_{\rm m}(r,\theta,\phi,\tau)$ because their sources are internal to the point of observation. Consequently, separating core-generated fields from crustal and ionospherically generated fields measured by satellite magnetometers is difficult and is still a research matter. Fortunately, fields generated in the Earth's crust and ionosphere are significantly attenuated at satellite altitudes. Therefore, errors in the main field model coefficients due to contamination of the satellite data by these two sources are comparatively small.

MAGSAT was a joint National Aeronautics and Space Administration (NASA)/U.S. Geological Survey mission. These data were supplied by NASA in the form of investigator B tapes.

The DE-2 satellite data set consisted of 5,100 data points gleaned from the low-altitude end of a comparatively eccentric orbit. This data set contained only scalar total intensity measurements of the Earth's magnetic field. However, this data set exhibited a substantially higher rms error relative to the DGRF-80 model than the MAGSAT data. Consequently, for this and other reasons, the DE-2 data were not used in the final main field model determination. This data set originated with M. Sugiura of Japan (formerly of NASA). It was edited by J.R. Ridgeway of Science Applications Research Corporation and it was subsequently supplied to NAVOCEANO by Dr. Robert Langel of NASA.

The Project MAGNET aeromagnetic data consisted of 338 high-level flights ($\geq 15,000$ feet) of vector component measurements. These data are routinely processed by NAVOCEANO at a 2-second sample rate and sent to the National Geophysical Data Center (NGDC) in Boulder, Colorado. A weak low-pass filter with a cut-off wavelength of approximately 7 km is routinely applied to this high-level data. The cut-off wavelength will vary slightly, depending on the average speed of the aircraft, which depends on prevailing wind conditions at the time of flight. Typical flights last 10 to 12 hours and are flown at an average speed of 440 km/hr. They are generally flown at night in order to minimize solar-driven external field effects which contribute to the Daily Variation (DV) of the Earth's field. Project MAGNET flights are of long range in remote ocean areas, which precludes the monitoring of DV. Therefore, no explicit DV corrections are

made to the data. Also, the aircraft's vector magnetometer is calibrated at the NASA Coil Room Facility at the Goddard Space Flight Center in Maryland at least once a year.

The magnetic field observations returned from each Project MAGNET flight are routinely reduced in accordance with the following procedures:

- a. Rotate vector measurements from magnetometer coordinates to instantaneous aircraft coordinates. This rotation involves only small misalignments relative to an imaginary coordinate system rigidly attached to the aircraft.
- b. Compensate in aircraft coordinates for the perturbing magnetic effects associated with the presence of the aircraft by removing a field phenomenologically modeled as:

$$\vec{B}_{C}(\tau) = \vec{B}_{Perm} + \vec{\alpha} \vec{B}_{M}(\tau) + \vec{\beta} \frac{d\vec{B}_{M}(\tau)}{d\tau}$$
 (28)

where the first term represents the permanent magnetic field generated by the remnant magnetization of the aircraft's metal parts, the second term represents the field induced in the aircraft's metal structure by the presence of the ambient field $\overline{B}_M(\tau)$, and the third term represents magnetic fields generated by eddy currents created on the aircraft's metal surfaces by the aircraft's motion through the Earth's spatially varying field. Here, $B_M(\tau)$ is the magnetic field measured by the magnetometer after it has been rotated into aircraft coordinates as indicated in step a. The compensation model contains 21 coefficients, 3 in the vector \overline{B}_{Perm} , 9 in the 3x3 matrix α , and 9 in the 3x3 matrix $\overline{\beta}$.

- c. Rotate the compensated field from instantaneous aircraft coordinates to geodetic coordinates, taking into account the misalignment of the inertial attitude device relative to the instantaneous aircraft coordinates.
- d. Visually edit the data in each flight via interactive graphics techniques.

The compensation coefficients are determined by performing calibration flights at an altitude of 1,500 feet above a designated magnetic observatory. These flights consist of a set of yaw, pitch, and roll maneuvers performed along the four cardinal headings (north, south, east, and west). The coefficients are then determined by a least-squares procedure that minimizes the squared difference between

the observatory field (upward continued and rotated into instantaneous aircraft coordinates using the inertial attitude devices on the aircraft) and the field measured by the aircraft's magnetometer.

Using this minimization technique, the 21 compensation coefficients are determined simultaneously with 6 Euler angles (3 for the magnetometer misalignment mentioned in step a and 3 for the inertial attitude device misalignment mentioned in step c. The overall process is, therefore, nonlinear, requiring several iterations to converge. Note, however, that it is possible to determine only the relative misalignment between the magnetometer axes and the inertial system axes. Therefore, the three magnetometer bias angles are arbitrarily set to zero so that, in practice, only the three inertial system bias angles (Euler angles) are computed.

After compensation and editing, the aeromagnetic data were decimated to a 200-second sample interval (i.e., every hundredth point was selected), yielding 54,656 vector magnetic observations. The resulting Project MAGNET data set was finally converted from geodetic coordinates to spherical coordinates, using the coordinate transformations of the previous section.

For modeling, it is desirable to have all data sets pushed forward or backward to a common epoch. Consequently, the MAGSAT data set, which was originally in spherical coordinates, was pushed forward to 1985.0 via the 1982.5 secular variation model. The portion of the Project MAGNET data set collected prior to 1985.0 was pushed forward to 1985.0 via the 1982.5 secular variation model, while the portion of the Project MAGNET data set collected after 1985.0 was pushed backward to 1985.0 by the 1987.5 secular variation model. Subsequently, a revised 1985.0 epoch main field model was generated by performing a weighted least-squares fit of the degree and order 12 spherical harmonic model to the combined MAGSAT and Project MAGNET data sets. The resulting main field model, when combined with the 1987.5 secular variation model, is referred to as WC-85 (revised). These coefficients are listed in table 5. The 1990.0 main field model was produced by pushing the WC-85 (revised) main field spherical harmonic coefficients forward in time using the 1987.5 secular variation coefficients. The resulting 1990.0 epoch main field model was then combined with the 1992.5 secular variation model to form WMM-90, the coefficients of which are listed in table 3 of section 1.3.

2.3 Mathematical Details of Main Field Inverse Modeling

The modeling procedure used was a modification of that formulated by Cain et al. (1967). The objective was to minimize the chi-square (χ^2) function

$$\chi^{2} = \chi_{r}^{2} + \chi_{\theta}^{2} + \chi_{\phi}^{2} + \chi_{F}^{2} \tag{29}$$

TABLE 5. WC-85 (REVISED) SCHMIDT NORMALIZED GAUSS COEFFICIENTS

n	m	8 m	h_n^m	8 m (n T / v r)	h _π (nT/γr)
	<u> </u>	(nT)	(nT)	(nT/yr)	(+(+/ f ÷ l
1	0	-29874.2	.0	18.7	.0
1	1	-1904.5	5496.4	10.6	-17.8
2	0	-2071.6	.0	-12.6	.0
2	1	3045.7	-2200.6	3.3	-15.5
2	2	1688.7	-306.1	.7	-15.6
3	0	1294.7	.0	3.6	.3
3	1	-2210.1	-306.4	-6.9	4.3
3	2	1246.8	284.2	.0	1.5
3	3	832.4	-300.7	-4.8	-10.4
4	0	933.5	.0	.0	. 0
4	1	782.5	232.5	.5	3.4
4	2	360.5	-247.6	-7.4	3.0
4	3	-424.2	72.2	.5	3.8
4	4	166.0	-296.5	-5.3	.0
5	0	-212.3	.0	. 8	.0
5	1	354.0	43.7	4	6
5	2	255.2	148.7	-1.7	.0
5	3	-94.6	-154.6	-3.3	.0
5	4	-162.3	- 76.2	.0	1.7
5	5	-47.2	95.0	2.0	.5
6	0	52.5	.0	1.3	.0
6	1	63.7	-14.7	.0	.0
6	2	51.0	88.6	1.8	-1.3
6	3	-185.4	70.0	.8	.0
6	4	3.8	-47.8	7	-1.7
6	5	15.4	-1.4	.0	.0
6	6	-99.3	17.7	.7	1.4
7	0	72.8	.0	.7	. 0
7	1	-59.7	-83.5	5	1.0
7	2	1.3	-26.7	.0	.0
7	3	25.1	-1.9	1.0	. 4
7	4	-4.8	19.9	1.9	.0
7	5	4.9	17.9	. 6	.0
7	6	10.1	-21.5	.0	.0
7	7	8	-6.8	.5	.0

TABLE 5. WC-85 (REVISED) SCHMIDT NORMALIZED GAUSS COEFFICIENTS (con.)

n	m	g _n ^m	h_{s}^{m}	ġ ^m	h,"
		(nT)	(nT)	(nT/yr)	(nT/yr)
8	C	21.7	.0	.2	.0
8	1	5.8	7.7	7	. 4
8	2	.6	-18.3	4	2
8	3	-11.7	3.7	.0	. 6
8	4	-11.0	-22.7	-1.3	. 5
8	5	2.2	10.8	.0	. 5
8	6	3.6	13.5	. 4	7
8	7	3.0	-15.4	.0	7
8	8	-4.2	-9.1	6	. 0
9	0	3.6	.0	.0	.0
9	1	9.5	-21.9	.0	.0
9	2	9	14.3	.0	.0
9	3	-10.7	9.5	.0	.0
9	4	10.7	-6.7	.0	.0
9	5	-3.2	-6.4	.0	.0
9	6	-1.4	9.1	.0	.0
9	7	6.3	8.9	.0	.0
9	8	.8	-8.0	.0	.0
9	9	-5.5	2.1	.0	.0
10	0	-3.3	.0	.0	.0
10	1	-2.6	2.6	.0	.0
10	2	4.5	1.2	.0	.0
10	3	-5.6	2.6	.0	.0
10	4	-3.6	5.7	.0	.0
10	5	3.9	-4.0	.0	.0
10	6	3.2	4	.0	.0
10	7	1,7	-1.7	.0	.0
10	8	3.0	3.8	.0	. 0
10	9	3.7	8	.0	.0
10	10	.7	-6.5	.0	.0

TABLE 5. WC-85 (REVISED) SCHMIDT NORMALIZED GAUSS COEFFICIENTS (con.)

n	m	g _n ^m	h, ^m	ġ ^m	h [™] n
		(nT)	(nT)	(nT/yr)	(nT/yr)
11	0	1.3	.0	.0	. Ç
11	1	-1.4	.0	.0	.0
11	2	-2.5	1.0	.0	.0
11	3	3.2	-1.6	.0	.0
11	4	.2	-2.2	.0	.0
11	5	-1.1	1.1	.0	.0
11	6	.3	7	.0	.0
11	7	3	-1.7	.0	.0
11	8	.9	-1.5	.0	.0
11	9	-1.1	-1.3	.0	.0
11	10	2.4	-1.1	.0	.0
11	11	3.0	.6	.0	.0
12	0	-1.3	.0	.0	.0
12	1	.1	.7	.0	.0
12	2	.5	.7	.0	.0
12	3	.7	1.3	.0	.0
12	4	. 4	-1.5	.0	.0
12	5	2	.3	.0	.0
12	6	-1.1	.2	.0	.0
12	7	.9	-1.1	.0	.0
12	8	6	1.2	.0	.0
12	9	.8	2	.0	.0
12	10	.2	-1.3	.0	.0
12	11	. 4	.6	.0	.0
12	12	.2	.6	. 0	.0

with respect to the 168 internal Gauss coefficients of a degree and order 12 spherical harmonic model, where:

$$\chi_r^2 = \sum_{i=1}^{l_r} w_{ri} (B_{ri} - b_{ri})^2$$
 (30a)

$$\chi_{\Theta}^{2} = \sum_{i=1}^{l_{\Theta}} w_{\Theta_{i}} (B_{\Theta_{i}} - b_{\Theta_{i}})^{2}$$
 (30b)

$$\chi_{\phi}^{2} = \sum_{i=1}^{l_{\phi}} w_{\phi} (B_{\phi} - b_{\phi})^{2}$$
 (30c)

$$\chi_F^2 = \sum_{i=1}^{l_F} w_{F_i} (B_{F_i} - b_{F_i})^2$$
 (30d)

where the upper case B's refer to the model values of their respective magnetic components, while the lower case b's refer to the observed (measured) values of their respective magnetic components. The subscript i refers to a particular data point, the total number I of which may differ for each magnetic component. Each data point is weighted by a weight factor, w, which depends on several factors:

a. Data type W_m

MAGSAT = 1

Project MAGNET = 1/4

Project MAGNET observatory airswing calibrations yield rms errors on the order of 35 nT, while MAGSAT rms differences from degree 12 spherical harmonic models yield rms values on the order of 9 nT. Consequently, the relative weight of the two data sets is taken to be $\cong \frac{9}{35} \cong \frac{1}{4}$. This factor characterizes the relative quality of the two data sets.

- b. The relative number of data points per equal area (5°x5° at the equator) cell; each cell was given equal weight. Therefore, data points corresponding to cells with more than the average number of points per cell, \overline{N} , received less weight and vice versa.
- c. The relative rms error of data in a particular flight or orbit relative to the rms error, $\overline{\sigma}$, for all data of the corresponding data type (MAGSAT or Project MAGNET).

- d. The relative rms error of data of a specified type in an equal area cell relative to all data of that type, $\bar{\sigma}$.
- e. The age of the data relative to the model epoch 1985.0. Thus, data collected five years away from this epoch get a weight of approximately 1/3, while data collected at the model epoch get a weight of 1.
- f. Distance of geomagnetic latitude, $\boldsymbol{\Theta}_{t}$ from the geomagnetic equator.

$$|\Theta_{M}| \le 20^{\circ} \begin{cases} w_{\theta mn} = 1 & for \quad k = 1, 2, 3(r, \theta, \phi) \\ w_{\theta mn} = 0 & for \quad k = 4(F) \end{cases}$$
; $n = 1$ (31a)

$$|\Theta_{M}| > 20^{\circ} \quad \begin{cases} w_{\theta mn} = 0 & for \quad k = 1, 2, 3(r, \theta, \phi) \\ w_{\theta mn} = 1 & for \quad k = 4(F) \end{cases} ; \quad n \equiv 2$$
 (31b)

This weighting scheme then takes the following mathematical form:

$$W_{ijklmn} = W_m w_{\theta_{mn}} \left(\frac{\overline{N}_{km}}{N_{kmj}} \right) \left(\frac{\overline{\sigma}_{km}}{\sigma_{kml}} \right) \left(\frac{\overline{\sigma}_{km}}{\sigma_{kmj}} \right) e^{-\left(\frac{s\tau_i}{\tau} \right)^2}$$
(32)

where the indices correspond to the following:

ith - data point

jth - equal area cell (1654 total)

kth - magnetic component (r, θ, ϕ, F)

lth - aircraft flight or satellite orbit

mth - data type (MAGSAT, Project MAGNET)

nth - geomagnetic latitude band (n=1 or n=2)

The decay constant t was arbitrarily chosen to be 5 years, while:

$$\Delta \tau_i = \tau_i - T_{EPOCH} \tag{33}$$

where t_i is the time of observation in years and T_{EPOCH} is 1985.0.

Table 6 gives the overall rms errors of a particular magnetic component for each of the three separate data sets relative to the DGRF/IGRF series of WMMs. Table 7 lists the number of data points associated with each mangetic component for each of the three data sets. Table 8 lists the average number of data points per 5°x5° equal area cell for each magnetic component for each data set. Rms statistics relative to the DGRF/IGRF series of models for the Project MAGNET data set are further broken down by Project ID and flight number in table 9. Due

TABLE 6. RMS ERRORS RELATIVE TO IGRE/DGRF MODELS

	σ_x	σ, rms (nT)	σ_z	σ_F
MAGSAT	14.7	12.0	13.2	12.7
Project MAGNET	101.7	107.9	105.5	96.4
DE-2				122.4

TABLE 7. NUMBER OF RECORDS

	N_x	Ν,	N_{z}	N_F
MAGSAT	30473	30473	30473	30473
Project MAGNET	54656	54656	54656	54656
DE-2				5100

TABLE 8. AVERAGE NUMBER OF RECORDS PER CELL

	\bar{N}_x	Ñ,	\overline{N}_{z}	$\overline{\widetilde{N}_F}$
MAGSAT	18.4	18.4	18.4	18.4
Project MAGNET	33.0	33.0	33.0	33.0
DE-2				3.1

TABLES 9. PROJECT MAGNET FLIGHT STATISTICS RELATIVE TO IGRF/DGRF MODELS (RMS units: nT)

			JULIAN	RMS	RMS	RMS	RMS
PROJECT	<u>FLIGHT</u>	<u>YEAR</u>	DAY	<u>X</u>	¥	<u>Z</u>	E
A32-153	6005	1981	129	116.4	92.3	159.0	156.6
A32-153	6006	1981	133	141.4	98.4	106.1	104.6
A32-153	6007	1981	139	223.7	242.1	191.5	200.9
A32-153	6008	1981	143	88.5	121.4	138.6	137.5 113.9
A32-153	6009	1981	146	138.3	86.6 135.3	105.3 151.6	151.5
A32-153	6010	1981	149 153	132.5 200.1	115.8	177.9	176.0
A32-153 A32-153	6011 6012	1981 1981	155	107.8	233.3	107.0	106.8
A32-153 A32-153	6013	1981	157	283.0	128.6	181.6	175.2
A32-153	6014	1981	159	146.4	166.2	110.6	111.3
A32-153	6015	1981	162	111.3	101.2	135.2	135.8
C32-252	1074	1982	62	60.1	51.9	49.2	73.2
C32-252	2007	1982	64	68.9	96.6	87.4	82.1
C32-252	2009	1982	67	79.4	76.6	85.1	74.0
C32-252	2011	1982	74	84.0	108.4	103.9	103.4
C32-252	2012	1982	77	95.1	74.4	65.7 64.8	94.5 61.8
C32-252	2013	1982	89 96	63.4 80.5	60.0 70.8	79.8	76.8
C32-252 C32-253	2014 1077	1982 1982	135	85.4	68.7	93.7	93.8
C32-253	1077	1982	149	86.0	121.8	58.9	66.3
C32-253	1081	1982	161	133.6	48.8	48.8	126.9
C32-253	1084	1982	171	63.0	54.8	99.1	91.1
C32-253	1085	1982	175	58.4	61.6	78.1	73.5
C32-253	1086	1982	177	164.8	103.3	162.0	185.9
C32-253	1087	1982	180	98.2	87.1	119.7	122.7
C32-253	1088	1982	182	122.5	134.2	160.7	154.8
C32-253	1091	1982	186	112.4	66.2	98.3 64.1	100.1 70.2
C32-254	4027	1982	231 233	86.4 155.3	91.4 81.4	81.1	76.4
C23-245 C32-254	4028 4049	1982 1982	235	120.9	87.9	89.2	78.1
C32-254	5022	1982	243	100.2	71.1	50.6	60.9
C32-254	5023	1982	246	87.9	74.2	67.2	60.8
C32-254	5026	1982	251	88.4	63.5	71.6	84.4
C32-254	5037	1982	260	81.1	79.5	60.3	83.0
C32-254	5030	1982	274	81.1	80.3	83.0	84.0
C32-254	5031	1982	277	131.6	46.9	90.3	81.1
C32-351	1097	1982	304	150.6	91.3	128.3	147.6
C32-351	3074	1982	305	109.4	126.3	63.6 89.6	101.4 99.9
C32-351	3075	1982	307 309	105.5 103.6	137.6 57.3	79.9	96.1
C32-351 C32-351	403. 4032	1982 1982	312	86.5	128.3	88.9	91.8
C32-351	4032	1982	314	94.9	101.6	97.9	100.0
C32-351	4034	1982	320	73.0	92.1	115.1	93.1
C32-351	4035	1982	322	59.1	144.1	64.6	66.8
C32-351	4036	1952	324	71.6	85.6	105.2	100.3
C32-351	5033	1982	327	208.2	191.1	118.5	124.3

TABLES 9. PROJECT MAGNET FLIGHT STATISTICS RELATIVE TO IGRF/DGRF MODELS (RMS units: nT)(con.)

PROJECT	FLIGHT	YEAR	JULIAN DAY	RMS <u>X</u>	RMS <u>Y</u>	RMS <u>Z</u>	RMS <u>E</u>
PROJECT C32-351 C32-351 C32-351 C32-351 C32-351 C32-351 C32-351 C32-352 C32-352 C32-352 C32-352 C32-352 C32-352 C32-352 C32-352 C32-353 C32-451 C32-451 C32-451 C32-451 C32-452 C32-452	FLI 4038 4039 40441 40441 10995 50446 1077 10995 50446 11077 10995 50446 11077 10995 5046 11095	1982222233333333333333333333333333333333	33333333333333333333333333333333333333	$\frac{x}{4}$ 33.9668044169656442831001726784564.890618477399.35316.10017267844.61.896561.8238641.0017267845.564.90661.8477399.31053.5864.109.84790739.31053.58661.8238	\$\frac{\cupage}{75.6890.9280.22555752693.87491.511.7971.3691.440.68288.58291.665.890.9280.225557526.9356.87491.511.7971.3691.440.68288.58291.665.891.958.691.3856.891.958.691.3856.891.958.691.3856.891.958.691.3856.991.440.68288.58291.665.991.991.991.991.991.991.991.991.991.99	2 87892608333962598715882222597849088254588992299750760 887892608333179136.2598715882222597849088254588992299750760 119652597849088254588992299750760 119652597849088254588992299750760	£ .5.5.5.2.6.9.5.3.5.1.3.0.3.2.5.8.1.6.3.6.7.8.6.4.0.4.5.9.9.8.1.5.3.6.6.8.4.6.1.5.4.6.5.3.0.3.3.3.3.2.3.6.6.8.4.6.1.5.4.6.5.3.0.3.3.3.3.2.3.6.6.8.4.6.1.5.4.6.5.3.0.3.3.3.3.2.3.6.6.8.4.6.1.5.4.6.5.3.0.3.3.3.3.2.3.6.6.8.4.6.1.5.4.6.5.3.0.3.3.3.3.2.3.4.6.4.6.1.5.4.6.5.3.0.3.3.3.3.2.3.4.6.4.6.4.6.4.6.4.6.4.6.4.6.4.6.4.6.4
C32-452	4060	1984	88	_ - - •			

TABLE 9. PROJECT MAGNET FLIGHT STATISTICS RELATIVE TO IGRF/DGRF MODELS (RMS units: nT) (con.)

PROJECT	FLIGHT	YEAR	JULIAN <u>DAY</u>	RMS <u>X</u>	RMS <u>Y</u>	RMS <u>Z</u>	.cm3 _E
C32-452 C32-453 C32-454 C32-4551 C32-551	4061 11092 30994 30995 30997 30997 30997 30997 31002 31104 110721 1112 1112 1112 1112 1112 1112 11	198444444444444444444444444444444444444	91 937 1407 1571 1641 18160 18190 19221 1937 1641 18190 18190 1937 1937 1937 1937 1937 1937 1937 1937	76.28 76.28 76.37 10.38 10	62.7 7.13.19.86.3.5.5.6.84.4.6.5.5.2.7.2.5.2.5.5.84.6.84.8.4.1.3.5.7.9.3.9.0.7.9.8.8.4.7.5.9.3.9.0.7.9.8.8.4.7.5.9.3.9.0.7.9.8.8.4.7.5.9.3.9.0.7.9.8.8.4.7.5.9.3.9.0.7.9.8.8.4.7.5.9.3.9.0.7.9.8.8.4.7.5.9.3.9.0.7.9.8.8.4.7.5.9.3.8.9.0.7.9.8.8.4.7.5.9.3.8.4.8.4.1.3.5.7.9.3.9.0.7.9.8.8.4.7.5.9.3.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.8.9.0.7.9.0.7.9.8.9.0.7.9.0.7.9.8.9.0.7.9.0.7.9.8.9.0.7.9.0.0.7.9.0.0.0.0	93.1 93.6.8 93.6.8 93.6.8 93.6.8 93.6.8 93.6.8 93.6.8 94.8 94.8 95.3 101.5 96.3 101.6 96.3 101.3 1	95.45.967.99220812626805180.9110.5439822087716.9342.3640.75 91153.967.9922081266.8051.80.9110.54398220.87716.9342.3640.75 1013822568051.80.9110.543982.20.87716.9342.3640.75 10115520.98220.87758623.9977.442.17985.9985.40.75 10115520.98220.87758623.998542.17985.758623.9985.40.75

TABLE 9. PROJECT MAGNET FLIGHT STATISTICS RELATIVE TO IGRF/DGRF MODELS (RMS units: nT) (con.)

PROJECT	FLIGHT	YEAR	JULIAN <u>DAY</u>	RMS <u>X</u>	RMS ¥	RMS <u>Z</u>	RMS <u>E</u>
C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-552 C32-553 C32-553 C32-553 C32-553 C32-553 C32-553 C32-553 C32-553 C32-553 C32-553 C32-553 C32-553 C32-554 C32-5554 C32-554 C32-554 C32-554 C32-5554	2017 2029 2030 2031 20031 20033 20033 20023 20023 20023 70010 7013 20129 70011 1134 31108 31107 31113 3113 31113 3	55555555555555555555555555555555555555	33570344937126915044603696048477091460237004902150 811222123448477091460237004902150 1112121111111111111111111111111111	X 019464360350746613913721960023804832810736403633475173115789354721960023804832810736403638231222334522233106655176633822333232335660855176633822333566085656086560866086608666086666666666	136.3 182.5 137.3 10.4 10.2 11.0 11.0 12.0 13.1 10.4 10.2 11.0 10.2 11.0 10.4 10.2 10.3 10.4 10.2 10.3 10.4 10.2 10.3 10.4 10.	919643897535371688459275927592759114127079993964502110 9196473897535371688755927592759114127079993964502110 1138835	E 598511060156310622489273219399263730586992084 63701744583706357799755576861113221189844152172620 111321189117357
C32-651 C32-651 C32-651 C32-651	3125 3126 5053 4077	1985 1985 1985 1985	301 305 314 317	61.4 77.3 97.0	236.2 110.8 178.2 202.1	95.8 80.4 105.1 114.7	62.6 98.0 112.4

TABLE 9. PROJECT MAGNET FLIGHT STATISTICS RELATIVE TO IGRF/DGRF MODELS (RMS units: nT) (con.)

PROJECT	FLIGHT	YEAR	JULIAN <u>DAY</u>	RMS <u>X</u>	RMS <u>Y</u>	RMS Z	RMS E
C32-651 C32-651 C32-651 C32-651 C32-651 C32-651 C32-652 C32-751 C32-751 C32-751 C32-751 C32-751 C32-753 C32-753 C32-754	5054 50578 4079 4081 4088 4088 4088 4088 4088 5059 5059 5059 5059 5059 5061 5065 5065 5065 5065 5065 5065 5065	1998555555555566666666666666666666666666	321 324 327 3314 343 345 345 323 442 471 336 427 477 781 885 891 104 292 333 345 345 345 345 345 345 345 345 345	83.66.66.55.87.26.63.33.47.52.00.28.70.3.95.01.62.21.37.61.4.42.81.1.95.66.88.8 83.66.66.55.87.26.63.33.47.52.00.28.70.3.95.01.62.21.37.61.4.42.81.1.95.66.88.8 83.66.66.55.87.26.63.33.47.52.00.28.70.3.95.01.62.21.37.61.4.42.81.1.95.66.88.8 83.66.66.65.58.72.66.33.34.75.20.02.87.03.95.01.62.21.37.61.44.28.1.1.95.66.88.8 83.66.66.65.58.72.66.33.34.75.20.02.87.03.95.01.62.21.37.61.44.28.1.1.95.66.88.8 83.66.66.65.58.72.66.33.34.75.20.02.87.03.95.01.62.21.37.61.44.28.1.1.95.66.88.8 83.66.66.66.55.88.72.66.33.34.75.20.02.87.03.95.01.62.22.1.37.61.44.28.1.1.95.66.88.8 83.66.66.66.55.88.72.66.33.34.75.20.02.88.7.03.95.01.62.22.1.37.61.44.28.1.1.95.66.88.8 83.66.66.66.55.88.72.66.33.34.75.20.02.88.7.03.95.01.62.22.1.37.61.44.28.1.1.95.66.88.8 83.66.66.66.55.88.72.66.33.34.75.20.02.88.7.03.95.01.62.22.1.37.62.88.8 83.66.66.66.55.88.72.66.33.34.75.20.02.88.7.03.95.01.62.22.1.37.62.88.8 83.66.66.66.55.88.72.66.33.34.75.20.02.88.7.03.95.01.62.22.1.37.62.88.8 83.66.66.66.55.88.72.66.33.34.75.20.02.88.7.03.95.01.62.22.1.37.62.88.8 83.66.66.66.55.88.72.66.88.8 83.66.66.66.55.88.72.66.88.8 83.66.66.66.55.88.72.66.88.8 83.66.66.66.55.88.72.66.88.8 83.66.66.66.88.88.88.88.88.88.88.88.88.88.	1296.6 129.6 131.5 132.5 132.5 132.5 133.5 134.7 136.0 137.5 137.3 137.5 137.3 137.5 137.3 1	16.4 68.2.1 68.2.1 68.2.1 68.2.1 68.2.1 68.2.1 68.2.1 68.2.1 68.2.1 68.2.1 69.2.1	22657567.1155335743988252926645286874285147542041856 5484693.3.3.57669222614.9.8.2.5.2.9.2.6.6.4.5.2.8.5.1.4.7.5.4.2.0.4.1.8.5.6 1846693837669222614.9.5.4.9.6.8.7.0.8.5.1.2.9.3.8.3.3.2.9.3.8.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3

TABLE 9. PROJECT MAGNET FLIGHT STATISTICS RELATIVE TO IGRF/DGRF MODELS (RMS units: nT) (con.)

PROJECT	FLIGHT	YEAR	JULIAN <u>DAY</u>	RMS <u>X</u>	RMS ¥	RMS 2	RMS <u>E</u>
C32-754 C32-754 C32-754 C32-754 C32-851 C32-851 C32-851 C32-851 C32-851 C32-851 C32-851 C32-851 C32-851 C32-851 C32-852 C32-952 C32-952 C32-951 C32-951 C32-951 C32-951 C32-951 C32-951	5071 3145 4100 3148 3149 3152 3155 3155 3157 3158 3157 3158 3167 4102 4103 4104 4107 4111 4108 3163 3167 4117 81178 1178 1178 1178 1178 1178 11	XE 199887777777777777777777777777777777777	251 2451 251 251 251 251 251 251 251 251 251 2	X 43.69693965153878215789994934289158466236633796642017 10753844517884934934289115866616309670.017 107538445178899949349349311556970.017 10753844517889994934934931151818236633796642017 10753849318181818181818181818181818181818181818	¥ 1.938063747661863269173722916837262621821286825400108971367697885327903665544168897952.12868254403	28.524.01.14.5.16.93.4.5.03.9.13.6.6.4.7.5.7.4.8.5.4.9.4.5.8.6.6.5.5.0.5.6.7.0.11.4.5.16.9.3.4.5.0.3.9.13.6.6.4.7.5.7.4.8.5.4.9.4.5.8.8.2.3.5.9.8.6.6.5.5.0.5.6.7.0.10.10.10.10.10.10.10.10.10.10.10.10.1	5783994305798595738367224264629258600079846826550 6569081067688053013445774001426462925860000798468222310 656908106768805734457740786397563977788398344577887671639756398222310 6569081067688057344577478747563971433983447788767163977983468222310
C32-951 C32-951 C32-951	4135 5084	1988 1988	345	71.1 78.8	39.9 44.6	79.4 108.0	48.7 81.1

TABLE 9. PROJECT MAGNET FLIGHT STATISTICS RELATIVE TO IGRF/DGRF MODELS.(RMS units: nT) (con.)

PROJECT	FLIGHT	YEAR	JULIAN <u>DAY</u>	RMS <u>X</u>	RMS ¥	RMS <u>Z</u>	RMS <u>E</u>
C32-253 C32-853 C32-853 C32-853 C32-853 C32-853 C32-853 C32-853 C32-853 C32-853 C32-853 C32-853 C32-851 C32-951 C32-951 C32-951 C32-951 C32-951 C32-951 C32-951 C32-954 C32-9554	1079 5073 5082 1169 5083 4117 4117 4117 4112 4129 4133 4132 4133 4133 4133 4139 4139 4139 4139 4139	1988 1988 1988 1988 1988 1988 1988 1988	145 117 119 122 105 174 131 164 168 177 289 318 328 331 328 212 228 229 234 255 263 252 252	59.4 173.9 145.9 22.255 108.9 104.8 103.5 104.8 104.9 104.5 104.5 104.5 104.5 104.5 104.5 104.5 104.5 104.5 104.5 104.5 104.6 104.5 104.6 104.6 104.6 104.6 104.6 104.6 104.6 104.6 104.6 104.6 104.6 104.6 104.6 104.6 105.6 10	53.4 93.1 154.1 110.7 957.7 966.5 717.9 966.5 717.9 103.7 970.6 111.6 136.4 171.6 112.3 119.7 111.6 119.7 111.6 119.7 119.	80.5 261.8 1909.3 666.3 257.0 857.0 91.4 755.3 257.3 140.5 101.5 140.5 101.5 101.6 1	75.1 263.4 182.8 584.0 184.5 88.2 14.3 88.2 14.3 87.4 12.2 126.6 83.9 118.7 83.1 126.3 118.7 126.3 118.7 126.3 118.7 126.3 118.7 126.3 126

to the uniformity of satellite data, the orbit-by-orbit statistics for MAGSAT and DE-2 data were taken to be the same as for each entire data set for each magnetic component. Note that data occupying cells for which there were fewer than 10 points were discarded due to the presumed unreliability of their cell statistics.

Now, the double summation expression over degree n and order m for $B_r(r,\theta,\phi)$, $B_\theta(r,\theta,\phi)$ and $B_\phi(r,\theta,\phi)$ can be converted to single summation expressions over the coefficient number l which ranges from 1 to 18%. Then, we may write:

$$B_r(r,\theta,\phi) = \sum_{l=1}^{168} C_l Q_{rl}(r,\theta,\phi)$$
 (34a)

$$B_{\theta}(r,\theta,\phi) = \sum_{l=1}^{168} C_l Q_{\Theta}(r,\theta,\phi)$$
 (34b)

$$B_{\phi}(r,\theta,\phi) = \sum_{l=1}^{168} C_l Q_{\phi l}(r,\theta,\phi)$$
 (34c)

$$B_F(r,\theta,\phi) = \sum_{l=1}^{168} C_l Q_{Fl}(r,\theta,\phi)$$
 (34d)

where the set of coefficients $\{C_l\}_{l=1}^{l68}$ are the Gauss coefficients g_{nm} and h_{nm} arbitrarily arranged so that:

$$C_{l} = \begin{cases} g_{nm}; & l(n,m) = n(n+1)/2 + m \\ h_{nm}; & l(n,m) = n(n-1)/2 + m + 90 \end{cases}$$
(35)

This ordering then requires:

$$Q_{rl}(r,\theta,\phi) = \begin{cases} (n+1) \left(\frac{R_E}{r}\right)^{n+2} \cos m\phi P_n^m(\theta) & ; \quad l(n,m) = n(n+1)/2 + m \\ (n+1) \left(\frac{R_E}{r}\right)^{n+2} \sin m\phi P_n^m(\theta) & ; \quad l(n,m) = n(n-1)/2 + m + 90 \end{cases}$$
(36a)

$$Q_{\Theta}(r,\theta,\phi) = \begin{cases} -\left(\frac{R_{\rm E}}{r}\right)^{n+2} \cos m\phi \frac{dP_n^m(\theta)}{d\theta} ; \quad l(n,m) = n(n+1)/2 + m \\ -\left(\frac{R_{\rm E}}{r}\right)^{n+2} \sin m\phi \frac{dP_n^m(\theta)}{d\theta} ; \quad l(n,m) = n(n-1)/2 + m + 90 \end{cases}$$
(36b)

$$Q_{ol}(r,\theta,\phi) = \begin{cases} m \left(\frac{R_{E}}{r}\right)^{n+2} \sin m\phi P_{n}^{m}(\theta)/\sin \theta & ; \quad l(n,m) = n(n+1)/2 + m \\ -m \left(\frac{R_{E}}{r}\right)^{n+2} \cos m\phi P_{n}^{m}(\theta)/\sin \theta & ; \quad l(n,m) = n(n-1)/2 + m + 90 \end{cases}$$
(36c)

$$Q_{Fl} = \frac{1}{B_{F}(r,\theta,\phi)} \{ B_{r}(r,\theta,\phi) Q_{rl}(r,\theta,\phi) + B_{\theta}(r,\theta,\phi) Q_{\theta l}(r,\theta,\phi) + B_{\bullet}(r,\theta,\phi) Q_{\phi l}(r,\theta,\phi) \}$$
(36d)

These expressions are the most useful forms in which the spherical harmonic equations for the magnetic field components can be cast for a least-squares problem.

Minimization of the chi-square function then requires that

$$\delta \chi^2 = \sum_{j=1}^{168} \frac{\partial \chi^2}{\partial C_j} \delta C_j$$
 (37)

be a minimum, where the symbol δ means variation. This in turn requires:

$$\frac{\partial \chi^2}{\partial C_i} = 0 \qquad j = 1, ..., 168 \tag{38}$$

Therefore, we must have:

$$\frac{\partial \chi_r^2}{\partial C_i} + \frac{\partial \chi_\theta^2}{\partial C_i} + \frac{\partial \chi_\phi^2}{\partial C_i} + \frac{\partial \chi_F^2}{\partial C_i} = 0 \qquad j = 1,...,168$$
 (39)

which is a nonlinear system of 168 equations for the 168 unknown coefficient set $\{C_i\}_{i=1}^{168}$. This system of equations is nonlinear since χ^2 depends on B_F which depends nonlinearly on the coefficients through the expression:

$$B_{\varepsilon}(r,\theta,\phi) = \sqrt{B_{\varepsilon}^{2}(r,\theta,\phi) + B_{\theta}^{2}(r,\theta,\phi) + B_{\phi}^{2}(r,\theta,\phi)}$$
(40)

where, $B_{\text{\tiny o}},~B_{\text{\tiny e}},$ and $B_{\text{\tiny o}}$ all depend linearly on the coefficients.

Consequently, after noting that:

$$\frac{\partial \chi_r^2}{\partial C_i} = \sum_{l=1}^{168} C_l \sum_{i=1}^{l_r} w_{ri} Q_{rl}(r_i, \theta_i, \phi_i) Q_{rj}(r_i, \theta_i, \phi_i) - \sum_{i=1}^{l_r} w_{ri} b_{ri} Q_{rj}(r_i, \theta_i, \phi_i)$$
(41a)

$$\frac{\partial \chi_{\theta}^2}{\partial C_i} = \sum_{l=1}^{168} C_l \sum_{i=1}^{l_{\theta}} w_{\theta_i} Q_{\theta_l}(r_i, \theta_i, \phi_i) Q_{\theta_j}(r_i, \theta_i, \phi_i) - \sum_{i=1}^{l_{\theta}} w_{\theta_i} D_{\theta_i} Q_{\theta_j}(r_i, \theta_i, \phi_i)$$
(41b)

$$\frac{\partial \chi_{\phi}^{2}}{\partial C_{i}} = \sum_{l=1}^{168} C_{l} \sum_{i=1}^{I_{\phi}} w_{\phi i} Q_{\phi i}(r_{i}, \theta_{i}, \phi_{i}) Q_{\phi j}(r_{i}, \theta_{i}, \phi_{i}) - \sum_{i=1}^{I_{\phi}} w_{\phi i} b_{\phi i} Q_{\phi j}(r_{i}, \theta_{i}, \phi_{i})$$

$$(410)$$

$$\frac{\partial \chi_F^2}{\partial C_i} = \sum_{l=1}^{168} C_l \sum_{i=1}^{1_F} w_{F_i} \{ Q_{rl}(r_i, \theta_i, \phi_i) Q_{rj}(r_i, \theta_i, \phi_i) + Q_{\theta l}(r_i, \theta_i, \phi_i) Q_{\theta j}(r_i, \theta_i, \phi_i) + (42.1) \}$$

$$Q_{\phi i}(r_i, \theta_i, \phi_i)Q_{\phi j}(r_i, \theta_i, \phi_i)\} - \sum_{i=1}^{I_F} w_{Fi}b_{Fi}Q_{Fj}$$

we have:

$$\sum_{l=1}^{168} C_l Q_{lj} = \Re, \qquad j = 1, ..., 168$$
 (42)

where:

$$Q_{lj} = \sum_{i=1}^{l_{r}} w_{ri} Q_{rl}(r_{i}, \theta_{i}, \phi_{i}) Q_{rj}(r_{i}, \theta_{i}, \phi_{i}) + \sum_{i=1}^{l_{\theta}} w_{\theta i} Q_{\theta l}(r_{i}, \theta_{i}, \phi_{i}) Q_{\theta j}(r_{i}, \theta_{i}, \phi_{i}) + \sum_{i=1}^{l_{\theta}} w_{\theta i} Q_{\theta l}(r_{i}, \theta_{i}, \phi_{i}) Q_{\theta j}(r_{i}, \theta_{i}, \phi_{i}) + \sum_{i=1}^{l_{\theta}} w_{Fi} \{Q_{rl}(r_{i}, \theta_{i}, \phi_{i}) Q_{rj}(r_{i}, \theta_{i}, \phi_{i}) + Q_{\theta l}(r_{i}, \theta_{i}, \phi_{i}) Q_{\theta j}(r_{i}, \theta_{i}, \phi_{i}) + Q_{\theta l}(r_{i}, \theta_{i}, \phi_{i}) Q_{\theta j}(r_{i}, \theta_{i}, \phi_{i}) + Q_{\theta l}(r_{i}, \theta_{i}, \phi_{i}) Q_{\theta j}(r_{i}, \theta_{i}, \phi_{i}) \}$$

$$(43)$$

and

$$\Re_{j} = \sum_{i=1}^{I_{r}} w_{ri} b_{ri} Q_{rj}(r_{i}, \theta_{i}, \phi_{i}) + \sum_{i=1}^{I_{0}} w_{0i} b_{0i} Q_{0j}(r_{i}, \theta_{i}, \phi_{i}) + \sum_{i=1}^{I_{0}} w_{\phi i} b_{\phi i} Q_{\phi j}(r_{i}, \theta_{i}, \phi_{i}) + \sum_{i=1}^{I_{p}} w_{Fi} b_{Fi} Q_{Fi}(r_{i}, \theta_{i}, \phi_{i})$$
(44)

This system of 168 equations can be written in matrix form as:

$$CQ = \Re$$

which has the inverse:

$$C = O^{-1}\Re$$

This is <u>not</u> the solution to the problem, however, since the right-hand side of this equation also depends on the unknown coefficients C_l . That is, each element, \Re_l , of the vector \Re depends on $Q_F(r,\theta,\phi)$, which depends on the unknown coefficients C_l in a very nonlinear way.

In order to solve this system of equations, we must iterate. If ρ is the iteration index, then we can let:

$$C_t^{(p)} = C_t^{(p-1)} + \delta C_t \tag{(3)}$$

Then, in matrix form, we choose the following iteration scheme:

$$C^{(\rho)} \equiv Q^{-1} \mathfrak{R}^{(\rho-1)} \qquad \rho = 1, 2, \dots \rho_{\max}$$
 (48)

The maximum number of iterations ho_{max} is determined by requiring that:

$$\sum_{l=1}^{168} \delta C_l \leq 1 \quad nanotesla \quad at \quad \rho = \rho_{max}$$
 (43)

This condition must be tested after each iteration until it is satisfied.

The rate of convergence of the algorithm depends strongly on the amount of noise (i.e., crustal influences, etc.) in the data. Aeromagnetic data have a great deal of crustal noise in them. Filtering the data to remove short wavelength (≤ 700 km) features from the data can improve the convergence rate by an order of magnitude. However, it has been shown that one-dimensional filters along the survey track leave short wavelength biases in the cross-track direction which adversely affect the final model. Consequently, no filtering (except for a very short wavelength (≤ 7 km) low-pass filter) was done on the aeromagnetic data. The number of iterations required for the model was $\rho_{\text{max}} = 14$.

In order to implement the algorithm it is necessary to have an initial guess solution $C^{(0)}$ that is as close as possible to the actual solution. The a priori model coefficients used were the existing WC-85 model coefficients (Quinn, Kerridge, and Barraclough, 1986).

Notice that in this iteration scheme, the Q matrix, which has (168 x 168) elements (as does its inverse Q^{-1}), needs to be computed only once since it does **not** depend on the coefficients C_l . Note, too, that Q is a symmetric matrix so that only half of the elements in Q actually need to be computed.

3.0 Modeling Results

An indication of the erratic nature of the geomagnetic field is provided by the wandering of the North and South Geomagnetic Poles. The pole movements since 1945 are illustrated in charts 5 and 6 which are based on the International Geomagnetic Reference Field (IGRF) models, WC-85 (revised) and WMM-90. The pole movements illustrate a poorly understood phenomena known as the geomagnetic jerk which occurred around 1970. The South Magnetic Pole movement in particular illustrates a sudden change in direction at about that time. These jerks occur only a few times per century and are thought to be due to a sudden release of magnetic energy built up from the electromagnetic coupling between the top of the fluid core and the lower mantle, both of which have substantial electrical conductivities. The numerical pole positions at one-year intervals for both poles are listed in table 10.

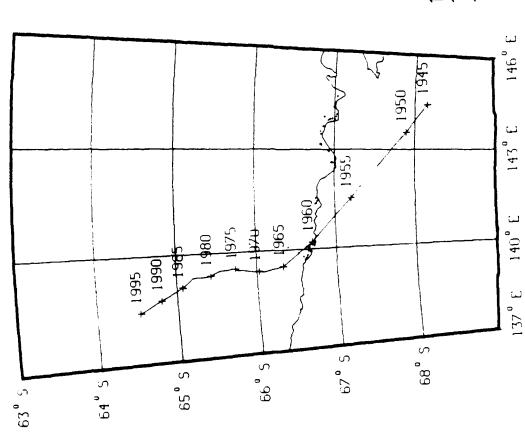
It should be noted that roughly 90 percent of the Earth's magnetic field is contained in the degree 1 spherical harmonic coefficients: g_1^0 , g_1^1 , and h_1^1 . These three coefficients characterize the Earth's magnetic dipole field and form the basis of the geomagnetic coordinate system, which for the 1990 epoch is illustrated in chart 7. The axis of the geomagnetic coordinate system pierces the Earth's surface at the Earth's magnetic dipoles, which are different from the dip poles. The location of the dipole poles is determined when the horizontal (H) component of the dipole field, computed from just the degree n=1coefficients, is equal to zero. The dip poles on the other hand are determined when the horizontal (H) component of the field is computed using all 168 coefficients of the full-degree n=12 model is equal to zero. For the WMM-90 model at 1990.0, the North magnetic dipole pole position is located at +79.35 degrees latitude and -71.10 degrees longitude, while the South magnetic dipole pole position is located at -79.35 degrees latitude and +108.86 degrees longitude. displacement vector for the eccentric dipole for 1990.0 in the usual Earth-fixed spherical coordinate system (i.e., Z-axis is the rotation axis, X-axis points to the prime meridian and the Y-axis is orthogonal to the other two, thereby creating a right-handed system) is 512 km radially outward from the Earth's center, with a colatitude 21.12 degrees and a longitude of 145.70 degrees.

A grid of main field and annual change values of the Earth's magnetic field derived from WMM-90 are tabulated in table 11 for seven basic magnetic field components (X,Y,Z,H,F,D,I). Contours of five of these components (Z,H,F,D,I) for the main field are illustrated in charts 8 through 12. Contours of the annual change of these five components are illustrated in charts 13 through 17. These charts were plotted on a corrected Mercator projection.

77° N 75° N

1945–1984 DGRF MODELS 1985–1989 WC–85 (REVISED) 1990–1995 WMM–90

CHART 5. NORTH MAGNETIC POLE MOVEMENT



1945—1984 DGRF MODELS 1985—1989 WC—85 (REVISED) 1990—1995 WMM—90

CHART 6. SOUTH MAGNETIC POLE MOVEMENT

North Pole

South Pole -

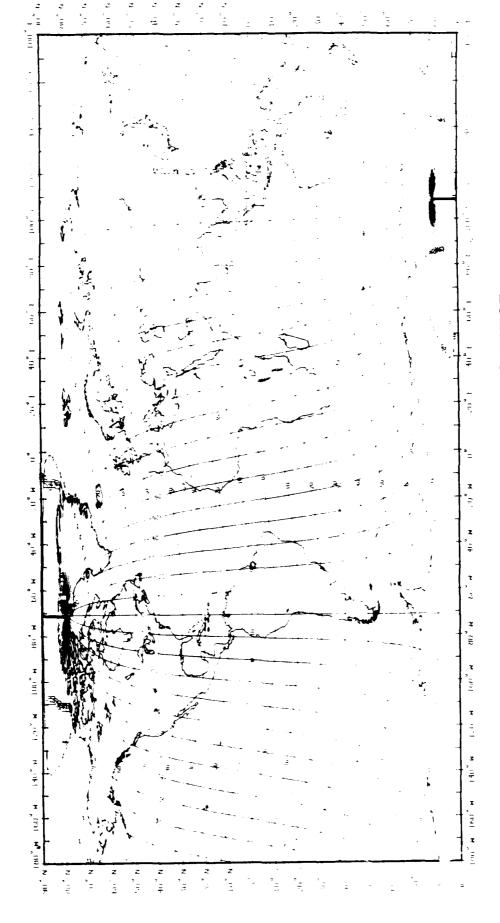
	<u>Year</u>	<u>Latitude</u> (degrees)	<u>Longitude</u> (degrees)	<u>Latitude</u> (degrees)	Longitude (degrees)
1234567890123456789012345678901234567890123456789	Year 1945.000 1946.000 1947.000 1948.000 1950.000 1951.000 1952.000 1953.000 1953.000 1955.000 1956.000 1957.000 1958.000 1963.000 1964.000 1963.000 1964.000 1965.000 1967.000 1968.000 1968.000 1970.000 1971.000 1972.000 1973.000 1977.000 1977.000 1977.000 1977.000 1977.000 1977.000 1977.000 1977.000 1977.000 1977.000 1977.000 1977.000 1977.000 1978.000 1979.000 1988.000 1988.000 1988.000 1988.000 1988.000 1988.000 1988.000 1988.000 1988.000 1988.000 1988.000 1988.000 1989.000	73.90 74.20 74.350 74.350 74.350 74.350 74.355 74.355 75.225 75.330 75.330 75.330 75.330 75.330 75.330 75.330 75.330 75.330 75.330 75.330 75.330 75.330 77.35.330 77.35.300 77.3	-100.20 -100.35 -100.45 -100.60 -100.75 -100.85 -100.95 -101.10 -101.25 -101.35 -101.35 -101.15 -101.25 -101.35 -101.25 -101.35 -101.25 -101.35 -101.35 -101.35 -101.55 -101.3	Gereland State of the state of	144.258.1.3.22.1.3.7.5.2.2.8.3.9.7.1.3.4.3.7.5.2.2.8.3.9.7.5.1.8.1.4.3.3.5.2.2.3.5.2.2.3.3.1.4.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3
50 51	1994.000 1995.000	78.70 78.85	-104.80	-64.53	138.43

Contours of these same five main field magnetic components plus grid variation in the north polar region are given in charts 18 through 23, while contours of their secular variations are given in charts 24 through 29. Similarly, for the south polar region, the main field contours are given in charts 30 through 35, while the corresponding secular variations are given in charts 36 through 41. These polar charts were plotted on a polar stereographic projection. Both the Mercator and polar stereographic charts were generated with respect to the 1984 World Geodetic System (WGS-84) ellipsoid.

3.1 Final Comments

The Polar Orbiting Geomagnetic Survey (POGS) satellite was launched in April of 1990, too late to be used in the 1990 epoch model. WMM-90, having been derived from data sets independent of POGS, will be a useful tool for evaluating POGS data and vice versa. Initial quantitative comparisons between WMM-90 and the POGS data indicate excellent agreement between the two. The POGS data will be used to fabricate the 1995 epoch model. Furthermore, if the satellite remains operational for its maximum expected lifetime of three years, it will for the first time be possible to generate a secular variation model to the same degree and order as the main field (i.e., N=M=12).

Looking toward the end of this century and beyond, efforts have been made to secure data for 'odeling purposes via the Defense Meteorological Satellite Program (DMSP) platform. Efforts are underway to secure scalar data from a boom-mounted POGS-type magnetometer on the S-15 DMSP satellite. This data will support the Epoch 2000 WMM. Further out, efforts are being made to secure full vector magnetic capability from DMSP Block 6 satellites that will operate during the first quarter of the next century.



U. S. NAVAL OCEANOGRAPHIC OFFICE

CHART 7. GEOMAGNETIC COORDINATES

TABLE 11. WMM-90 MAIN FIELD AND ANNUAL CHANGE GRID VALUES

1. 10%6	ü	~	10	15	u?	\$	30	3	0,	\$	ē,	•	t. tone
													1 4 1
76	4 × 0 - 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0	197	201	-19.2	-11-3	-12.3	-13.2	-4171	-2153	-{120	2070	-1601	16
~	12.1	-1355	-1815	4627	-48.5	-1821	3084-	-2855	-\$878	-3863	-343	-3184	æ)
30	67.5	-15.8	4.21	401-	\$\$85-	-\$718	-9332	6 304 -2 3.6	9776-	-24.3	5348 -24.3	5003	3 8
7.5	4100	8934	8999	4096	10.0	-21-2	-255-	8151	-23.6	7708	7329	\$ 605	7.5
20	10/01	10918	19989	13280	14823	19808	10639	10421	13153	9850	9508	9113	0.0
\$ 9	12840	12940	12984	12978	17928	12838	12710	12548	12351-16.3	12122	11862	11576	Ş
۷0	154.8	15098	15312	15089	15838	14965	14874	14368	148.3	143.2	14353	36847	90
\$\$	17413	17439	17422	1737P	17519	17255	17188	17126	17070	17018	16972	16929	\$\$
\$0	10053	19955	19922	19965	19801	19743	19693	19663	10652	19666	0.9-	19777	20
\$\$	80822	22808	22889	35.825	82822	32,425	22405	\$5352	£1822	72469	82822	3222	4.5
0 \$	1.01	25321	25,327	25317	25, 125	525.89	25285	\$5552	25328	25406	355.49	25757	ŋ ,
٠,	27875	7.974	28049	75103	20149	28189	28.222	28254	28299	28385	2#5#5 -5.8	28780	3.5
30	\$2555	21575	39868	39704	30828	30833	31918	\$2012	31,13	47874	31388	31848	0,
\$	\$2162	16571	32645	12975	34041	13251	34385	13481	33570	33682	33859-	34110	2.5
02	\$1245 25.22	15659	13996	14.321	34608	16346	35035	35177	35307	35461 -A-6	35678	15986 -16.2	2.0
1.5	3.61	18.7	34.340	4774	lites	12858	32958	18852	36076	38303	36594	39873	15
10	3,447	3.5021	31566	34050	34434	34840	35119-8-3	35412 -12.0	35695	36026	36428 - 18.0	36914	10
~	30506	11906	31599	12138	12008	\$3008	33368	33723 -10.8	35119	34578	35123	35748	~
o	47466	7.21-	28627	29164	29643	30271	30487	30934	31453	34865	\$2771	33555	0
LAT 4. 10%6	٤	٠	10	15	u~	\$	30	3	6.4	\$	8.0	\$\$	1 A 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
nT (units: nT)													

1. 1046	0.4	\$	۲.	2.2	10	8.5	0.6	\$ 6	100	105	110	115	1. 1046
141													1 4 1
0.6	1973	1827	1714	159	1460	1314	1156	760	-13.7	-12.9	-12.0	-16.9	06
88	4128	2863 -20-2	- 19.6	- 13.62	-18.2	-1913	1221-	-1556	14.18	-13.8	1232	-1183	R S
0	\$6.28 -25.8	4252	1887	3547	3231	-2060	-19.6	2574	-45.8	-16.30	- 36 s 5 -	-1534	0.
2.2	6501	9014-	5661	5277	4918	4619	4386	4231	4160	4180	4291	4489	۲\$
7.0	8236-	-2335	-23.5	755A -24.R	25.36-	-24.9	-\${1}	-9583	7,56-	-\$\$18	\$6.56-	\$683°	7.0
\$9	112.79	14051	10632	19328	19948	-24.5	-24.3	29562	9579	-2988	9909	19344	45
۷0	14908	11829	11628	13663	13578	8114	13855	13858	138 R.	135.3	13968	13808	0 4
\$\$	16883	16959	16918	62201	85257	18332	19348	19799	19893	13951	13881	13869	~
20	19470	19981	20101	\$2.502	20347	20465	20582	29703	20834	20990	21181	21514	\$ 0
\$	25677	2313	23438	3025	23968	24208	24421	24904	8:352	24892	23918	23358	4.5
94	8.652	82800	65852	377.3	62822	23822	27853	29378	8:342	58835	29823	2469.5	0.
5 k	20110	29515	8.8-	30441	36898	31311	31653	71907 -15.5	32049	32092	32043	31921	35
40	11399	32440	32939	13459	33964	34418	34785	35038	35158	35143	350n4 -13.0	34762	30
\$	54504	14967	35489 -20.6	36934	36561	37030	37401	37642	37730	37660	37445	37105 -5.3	* ~
90	56592	*6881 -2**	17475	17985 -23.0	38523	38994	39359	39582	39642	39532	39567	38865 0.	2.0
15	\$7439 -19.6	97978	32557	39145	39699	40179	40544 -11.8	40767	40810	40689	40410	\$ 000x	15
10	37476	30995	34742	39382	39978	40489	40879	41110	41193	41111	40828	40474	10
~	36438	47169	31912	18636	39305	19881	7.94	6.004	0.02,	40778 20.4	4.98.18	40324	V *
0	80838	458 cz	2173	1,88.	6:35:	18 3 RB	34848	10365 30.8	38834	1382	13833	33305	O
[A]													4)
1 1040	Ş	Š	۲,	٤	80	85	0.6	Ś	100	105	ا ان	115	1 1 0 N C

1. 1046	0.74	175	110	135	140	145	150	1.5	160	165	176	175	1. 10NG
[4]													1 4 1
06	**************************************	1000	307-	-481	199-	-145	-1014	5.11-	1332	-1477	- 16 10 8 - 8	-1731	06
~	1155	11158	1156	1194	1528	1365	1298	1321	1331	1321	1290	1236	\$
0	-14.8	-14.2	- 3973	-1316	-1365	1918	-1953	1458	-1123	-4534	1884-	-1879	3
22	4747	5113	5511	5942	-19.6	-19.9	7223	7576	7860	8061	8168 -21.4	8172	2
0,4	7468	8602	9459	9023	9598	10155	10667	11110	11462	11705	11827	11821	92
65	17681	11204	11791	12414	13039	13639	14181	14640	14993	15225	15324	15285	65
9	14243	14757	15328	15925	16517	12072	17560	17956	14243	18407	17643	18450	09
\$	17968	18409	18691	19387	19865	29393	20,652	20915	21873	21813	2.958	20883	\$\$
\$0	275.7	22006	22340	22622	24873	23834	23381	23457	23436	23325	12182	22847	\$ 0
\$	2.288 -18.2	25436	25581	25704	25783	25795	25739	7.55	25369	25070	24712	24115	4.5
0 7	2965 1108	42682	23869	28.45 F	28525	20002	19822	27,89	2.825	50403	8.852	21452	0 7
\$	51741	11513	31236	10801	30505	30035	108-2	20818	82852	61672	5692	26316	\$
30	34435	14036	33548	13029	32419	31742	31011	\$0545 10545	29451	28658	27878 -16.5	27171	3.0
35	35661	36129	35511	1 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8	34042	13211	37546	31446	30556	29687	28865 -24.3	24119	\$
0,0	67845	8820	37923	8554	35368	34456	33518	32528	31858	19782	\$3868	2887	20
1 5	39456	16.914	38080	17.204	36392	15482	34562	33655	32783	11962	31213 -21.8	30555	15
10	39973	39468 15.2	38675 15.5	17211	17101	36271	35444	4442	31879	33169	32527	31963	10
~	32912	14.99	38 803	11.50	37464	16771	36091	0.45	34826	14.260	33745	13288	^
o	10284	11.9	18450	11547	37421	*6896 5.9	36386	15903	15.50	35033	12.9	1.597	0
247													1 v s
1. 1046	176	175	1 50	135	140	145	150	155	160	165	170	175	9 NO 1 . 1

The case Cas	1. 1046	187	- 45	147	105	70 <i>0</i>	502	210	215	220	\$ <i>?</i> ?	7.50	5.2	1. 1046
1.	141													1 4 1
17.00	06	- 18 19	19.3	3.82-	-4373	-3123	-3354	-4173	1773-	-3153	-\$159	8.83-	-4804	36
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	~	5511	1047	915	76.	2 8 8 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4	000	£02	×.,	-197	V E K -	6°6 6'6	-715	€.
1,11, 1,12	0 %	4496	6440	4140	5 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	5 8 5 E	3166	2763	2438	1906	147A	1069	691	C •
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	2	0.12-	7465	7566-	1163	-6684 -15.7	4139	5543	7.4-	82.35	3630	\$9.5	24.34	2.2
1,117 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17 1,17	7.0	11685	11420	11014	10537	9943	9269	12.5	1759	6962	616 8.1	5397	0.8	20
1113	65	14109	14400	14365	13816	13168	12438	11643	10405	9944	9080	8	10.4	\$9
	۷0	19132	17796	17349	16907	16169	15463	14699	13894	13061	12222	11390	10583	9
1.81.3 1.81.5	\$\$	4.0613 -5.8	2025B	19625	19321	18762	18148	17491	16801	160 45	15355	14619	13888	\$\$
24819 24829 <th< td=""><td>20</td><td>1314</td><td>22135</td><td>12212</td><td>2128A</td><td>20830</td><td>20353</td><td>19854</td><td>19355</td><td>18705</td><td>18235</td><td>17657</td><td>17064</td><td>0 \$</td></th<>	20	1314	22135	12212	2128A	20830	20353	19854	19355	18705	18235	17657	17064	0 \$
4513 74878 74879	\$\$	1.800	\$\$\$\$	63452	62182	82832	2.843	21823	21,503	85812	\$6902	80802	83261	4.5
45714 24843 24841 24843 24843 24854 <th< td=""><td>0,</td><td>\$1677</td><td>400C 400C</td><td>24878</td><td>23759</td><td>£1845</td><td>24828</td><td>£28x2</td><td>3.652</td><td>82822</td><td>8:322</td><td>\$1.825</td><td>litie</td><td>0 7</td></th<>	0,	\$1677	400C 400C	24878	23759	£1845	24828	£28x2	3.652	82822	8:322	\$1.825	litie	0 7
25516 2983 2983 2983 2983 2983 2983 2983 2983 2983 2983 2983 2983 2983 2983 2983 2983 2983 2763 2763 2763 2763 2763 2763 2763 2763 2763 2763 2764 <t< td=""><td>*</td><td>95257</td><td>\$\$256</td><td>24842</td><td>24598</td><td>5.8.2</td><td>24367</td><td>24343</td><td>24.751</td><td>24358</td><td>24353</td><td>24815</td><td>24246 -846</td><td>45</td></t<>	*	95257	\$\$256	24842	24598	5.8.2	24367	24343	24.751	24358	24353	24815	24246 -846	45
234.6 246.6 264.5 264.5 264.5 264.5 264.5 264.5 264.5 264.5 264.5 264.5 264.5 264.5 264.5 264.5 274.6 <td< td=""><td>0 2</td><td>24542</td><td>200°</td><td>5.646</td><td>254452</td><td>25347</td><td>25 35 5 R. A.</td><td>25,625</td><td>25528</td><td>25645</td><td>25757</td><td>25852</td><td>25916</td><td>0 \$</td></td<>	0 2	24542	200°	5.646	254452	25347	25 35 5 R. A.	25,625	25528	25645	25757	25852	25916	0 \$
248.9 248.4 248.4 278.9	\$2	8.84.5 5.84.5	28682	24636	5.443	26383	26853	26845	20989	26864	27046	£2852	333.6	52
\$1407	02	80° 08° -	0.835	1:817	\$9812	\$0.87.2	27849	2775	86322	28469	20802	248.28	38863	20
\$1507 \$1801 \$1627 \$1916 \$250 \$1626 \$1927 <	15	50007 -26.3	29580	29276	29085	28990	28973	29015	29105	29233	29391	29569	29742	15
\$28.5 \\ \frac{25.6.5}{15.2} \\ \frac{25.6.5}{15.2} \\ \frac{215.5}{25.2} \\ \frac{215.5}{25.6} \\ \frac{25.6.5}{25.6} \\ \frac{25.6.5}{2	01	31407	41101	50801 -16.8	10577	30417	30312	\$0.55 9.6.9	\$0244 \$450x	\$0273	30 5 5 R	30429	10528	10
1475 1195 1287 18800 15887 18800 18800 18801 18801 18801 18801 18801 18801 18801 18801 18801 18801 18801 18801 18801 18801 1880 188	~	57886 0.0-	45.53	\$3528	11001	31513	1803	31324	31184	31083	31815	30940	30963	•
167 145 197 195 200 205 210 215 220 225 230 235 6.1	c	13014	\$ 304.3	\$ \$ \$ 2 \$	3000	\$2825	1985	34074	31P.U? -342	\$15.70	1987-	\$1174	51027	3
167 145 197 195 230 210 215 220 225 230 225 to t	[4]													4.
	1 . tonc	167	135	161	105	7.30	502	210	215	622	\$22	230	512	4 . 10NC

. 1086	440	597	647	552	u9?	592	270	51 2	780	542	U6~	562	1.10
1 4 3													7
76	-1923	1927	17.18	1595	16.0	-1814	-1358	14.5	1623	15.5	12.0	16.73	
\$ K	-841	13.6	949-	-1004	15.9	16.3	16.5	16.4	16.1	15.5	125	13.5	
0.	10.2	17.5	14.5	30-7	1867	19.3	20.2	20.7	20.05	20.05	20.04	1828	0
25	1911	1401	1004	1921	26.22	25.3	25.97	24.8	36.3	35.8	3838	\$3.9	
7.0	4804	34.7	2929	\$\$.B	32.09	\$358	3355	38.89	35.8	33.8	33.7	39.53	
45	46.4	18.1	5424	24.52	4619	29.4	2345	34.3	\$6.58 35.55	\$923	\$8.6	\$ 0.63	
۷0	0 5 0 0 0 0	01 00 FF	5478	32.0	35.3	3588	4118	8718	33.3	{8;}	86.68	8658	
\$\$	14.8	12494	11863	11304	10841	10496	10290 27.8	10236	10340	10598	10997	11514	
0 \$	16462	12,863	15421	14739	14263	15877	13619	13481	11503	13679	14000	14447	
\$\$	102.2	ยังไหม	18478	17828	17848	17853	19849	35494	19898	19958	16808	82371	
0,	1001 ×	71867	21303	20914	82\$ō2	2014#	19828	800 80 80 80 80 80 80	19659	13843	19879	19839	
.	24128	23954	23623	23430	23338	24782	23860	22183	21983	21885	21909	28867	
ŋ .	76637	25891	25776	25587	25331	25028 -30.8	24.704	24393	24128	23942	23863	23912	
\$6	47492	27542	27510	27586 -44.2	27173	26884	26549	26199 -30.0	25872	25603 -A-6	25426	25369	
90	2 8 8 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	28921	28429	28836 -59.2	22636	2834.5	27987	36522	23318	255.3	26605	26459	
15	. 9 K 9 B	24982	20401	29897	50962	29393	29014	28590	243.5	27755	27417	27177	
10	10614	0.68-	30640	30552	90.79-	30021	296 34	29192 -54.2	28729	28281	27883	27567	
~	9 1 0 C C C C C C C C C C C C C C C C C C	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	\$2452	35 387	82835	39234	5\$865	58858	289.48	\$9882	22812	\$ \$ \$ \$ 5	
ن	\$0605	6.3 5.	12005	38855	88885	38963	24.036	29894	29817	28313	27914	17.75	
1 4 1													z
PACT 1	7.11		-		0 7	• • •			0	200	000		

00												
												[A]
7 E	106 8.6	105	481	4.4	3.5	1014	1177	1332	1477	1610	1731	0.6
~:	1833	1878	1983	25.5%	\$262	\$2.62	3408	3005	38.8	5103	-1903	\$
79.	191	\$ 716	1 7 6 E	37.65	\$229	4	5215	5928	5883	2689	4544	0
00.	3516	21.1	19.5	3400	12.2	6573	7.096	7566	7075	8319	8594	2,2
80.	5249	5941	6634 26.6	7314	19.7	15.7	91.32	9541	9991	10329	10595	7.0
\$1.05	7433 38.7	8152	34.5	9556	10203	10703	11315	11767	12145	12447	12678	\$ 9
~ •	44.4	\$0.531	12408	1287	19895	13858	137.59	113.9	142.3	14838	3.571	09
20·	97721	1.87	14.132	14768	15351	15869	16115	16644	15978	17191	18335	\$\$
~9	15603	18343	163.5	17481	18035	18527	18950	10300	19573	1,02	148.8	3.0
٥٠.	18390	18884	19489	20075	20622	21116	71546	21908	23195	22404	22537	4.5
رسون د پار	80162	15382	33252	15352	£66\\ 2	21833	22808	8:432	23258	25903	23178	0,
èv.	59222	23,272	2584R 54.4	24463	25084	25645	26241	26733	27146	27471	5.05	3.5
5. 6.	74428	24872	75454	26101	26788	27478	28154	24727	39236	29651	29976 \$2.58	30
~,	75694	26093	26639	80 \$22	28849	2 # 806 4 9 2 9	29551	37236	10837	31343	33269	25
~*	79547	26405	2385	24839	59169	29555	36436	31868	31728	32305	35805	20
\$987.	1112	82832	\$1,475	25355	28809	29828	39353	33823	13513	35329	3888	
<u>ئ</u> :	27240	8.5-7	27591	2.622	28418	28955	29529 1A.0	30114	10696	87.51.8	11863	10
22.19	27113	27015	27021	3115	\$2322	3.8-2	27672	24306	28745	\$ 7 2 6 2	89795 5.	•
0.m	\$28.29	82882	28223	23848	85382	25888	53853	25858	£0867	54403	3492	J
												1
400	3 (2)	•										

1. 1040							2 25												\$ E =		1 41
\$ \$									14148								·				
SC		3.382	29618	9:842	? \$\$},	19275	166 16	147.2	1350	188.9	13563	18808	11979	116.9	115 1	19833	9608	3.01-	\$1.75	1573	5.0
\$		34863	29259	8:852	21345	18110	15598	13909	12833	14508	13304	13823	12463	\$2532	13320	13838	10856	9464	7493	4944	\$
67		33833	23885	24151	\$\$ \$02	17068	14600	13029	12258	12073	13338	14333	12836	13043	13059	53185	12023	10710	4.9.5	6.5 v	07
:		\$383	23332	23352	18828	16153	13698	20,521	11369	11500	13889	13533	13097	13554	13797	13881	13101	11021	1001	997	÷
30		33865	2,58,5	82822	19178	15409	12946	11401	19843	11099	11673	13851	13259	13463	14523	141.2	14087	139.0	11478	\$7.36	30
\$2		29973	2988K	28418	19249	14857	12382	19929	19438	10643	13353	2:85	13346	145.2	14963	13551	14980	14952	12363	9959	≈
07		23443	3883	21808	13858	14406	12025	19859	12938	32837	11069	13823	13390	14833	15422	159.9	14782	14984	1.818	11048	0.2
15		28165	25852	23438	17584	14303	11367	10398	-2434	10054	10866	14065	13424	14746	15917	16454	16496	15925	14358	12047	15
1,		7:857	25.08.2	21825	14893	14240	11848	18618	-5815	998 -45.8	10776	1381	13480	14943	16179	16953	17124	16573	1, 109	12964	10
~		24243	55865	20167	13305	14298	12056	19815	9971	1867	10716	1,5254	13583	15140	16496	17408	17685	17231	15841	13779	•
c		8-61-5	25825	5.835	12199	14441	12343	13838	19828	10314	10992	124.8	11753	18181	16812	17804	14175	17798	148.8	14490	c
1. 1046	[4]	6	? -	-10	-15	-20	-25	- 10	-15	07-	-45	0 5 -	-55	٠٠٠	-65	-70	-75	0#-	-#5	96-	1 A T

1986 1986	\$ 9 0		٥,	۲	Ce	8	6	\$6	100	105	110	115	1. 10%6
\$4823	36941	36941	~	37710		18387	38946	39765	39614	39751 28.5	\$9724 25.55	19564	3
\$000.50 \$156.5	12.5 20.6 33503 14439 35310	14430	•	35518		39,108	36795	37.18	377.83	38068	3A210 26.3	18216	•
24639 3586 3539	1366	1366		32328		12821	\$2835	2,28,5	3\$329	35.79.2	36316	36303	- 10
21932 2451 2410 2511 2524 2544 2112 24093 2472 24141 25141 2		2 8 9 9 9		28999		29949	30839	31659	32392	33818	31514	33874	-15
2992 24518 2125 24505 24512 24	22570 23613 24617 33-1 12-4 30-0	24617		25585		26523	27433	28303	29121	29860	30493	30999	0 ~ -
\$155.5	19634 20542 21438	8:312		22299		25/82	24895	24843	25\$74	26464	82122	27786	-25
14873	17871 185			1924 2		19944	27668	21519	8.8152	23962	23693	3-8-5	- 10
11872 15926 15656 15616 15677 11156 11872 15926 15655 15616 15978 14627 11872 15926 15625 15616 15978 14628 14872 15926 15826 15816 15978 14628 14872 15926 15926 15926 15928 15928 14872 1552 1552 1552 15526 15928 15928 14872 1552 1552 1552 15526 15928 15928 14872 1552 1552 1552 1552 15520 15928 14872 1552 1552 15520 15928 15928 14872 15875 15928 15928 15928 14872 15875 15928 15928 15928 14872 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929 15929	15151 15604 16050	16050	. •	16507		16995	17552	19123	19773	19457 -18.6	29139	24784	- 35
13872 15928 15876 12814 13923 14991 14992 14992 15824	13609 15865	15865		14058		19801	14610	14999	15468	15903	16577	17156	07-
-\$6.6	12214 12973 11248	118:8		11854		11833	11878	13928	13878	13614	13923	14681	-45
-48.6 -55.3 -42.7 -50.8 -50.5	31822 18838 18818	19214		29.36		-2323	-3898	-3179	-49.73	-3588	-3508	3068-	- \$0
-48.7 -36.5 -35.2 -35.2 -35.0 -54.0 -54.8 -59.8 -48.1 -148.2 -37.6 -58.8 -59.8 -59.8 -48.1 -37.6 -58.8 -59.8 -59.8 -48.1 -37.6 -58.8 -59.8	10039 9370 8613	-562		7948		-4259	400 CF-	-35.3	-6183	-3046	- 50 39	-28.4	- 55
-48.1 -35.4 -47.5 -57.6 -58.8 -59.8	8061 -8197 -51.2	7687		-43.0		5306	4552	3871	2.55-	-34.8	-54.6	-36.13	-60
-46.3 -36.8 -1958 -36.8 -20.2 -26.7 -26.7 -26.7 -26.7 -26.2	7991 6810 5630	5630 -42.8		144		3189	7381	1487	-43.5	9.78-	-345	-697	\$ 0-
-1552	\$\$\$\$- \$\$\$\$- \$\$\$\$-	\$356-		-4856		3388-	4.803	1.080 1.080 1.080	21858	3488	=385	-36.79	-70
- 36.2	-3502 -5968 -3958	2650		-38.9		-3158	-1552	-2565	-4773	-4754	- \$803	\$°0\$-	-75
-566 -6566 -7765 -8660 -9879 -19795 -765 -46.5 -48.7 -1981 -11898 -14902 -765 -6765 -100 105 110 115 t. 1	3849 2376 907 -17.0 -19.0 -20.9	6.02-		-539		-1945	-3293	-4567	-3820	-6629	-7793	-8631 -54.2	04-
50872 - 48581 - 19592 - 54805 - 14508 - 14505 - 00 00 00 00 00 00	- 8.4 1803 - 341 - 1110 - 25.18	-1110		-45.8		-3928	-5268	-6544	-7745	-8860	-9879	-10792	\$ æ -
90 95 100 105 110 115 1.	\$8\$\$- \$.85- \$66=	3885-		9484-		-619B	2.0-	-40.3	-48 4-2	19891	8.811-	74805	06-
	08 57 77 54 03	25		98.0		∽	06	\$6	100	105	110	115	1 A 1 1 - 1 0 N G

t. 1046																				1 v t	t . 10N6
175	16278	146%	14253	33808	80878	29887	10385	25.98	21840	1887	1888	12387	496	-5308	-28.8	-4264	-8983	-18168	1897		175
170	34650	1863	11.26	33958	32918	29805	2385	24418	27471	19803	15186	11728	7939	-38:3		1.18-	-38.19	-13519	13861		170
165	15833	2958	34248	33769	\$2005	38185	23825	24150	21107	17843	14628	11808	-1614	-}86-}	3888	-5618	-3845	-13163	-15925		165
16.0	35459	35569	1.858	3.8818	31987	29878	5885	2,890	23825	17483	14268	19818	-21.5	-8337	1369	-6194	-14113	-13463	-19168		160
155	35902	35873	\$2\$5\$	33918	31976	29523	8n262	23643	29415	11048	13212	6258-	\$606	-3847	13882	-6687	-19454	1386	1988		155
150	5 4 5 R C 8 - 5	34106	35858	3.60.8	31969	29442	24343	23401	29085	19929	12947	-4963	-5147	1908	-4128	\$662-	-144.5	-13821	-14583		150
145	36896	46549	35613	34828	31959	6.815	19182	23159	19759	16509	12475	-9876	-\$835	-35.36	7885-	-3887	-19793	13835	7584-		145
140	37421	36.896	35812	34153	319 13	29243	293.8	22903	19423	15883	11979	-3928	-30.9	-36.0	-3841	-7549	-10774	-13863	-15808		140
115	17511	15821	10813	34813	1981	29103	25981	22614	19063	15355	11499	-3325	3506	-58.5	1:83:	-7591	-19822	-13567	-18839		135
1 1 1	18450	3 7 5 F B	1215	1,975	31749	27911	10852	3-9-2	18065	14615	1183	-38.1	-34.0	1:92-	-4378	-7494	-1923	-15848	-11846		130
10.5	8084,	87888	\$0 \$13	14214	41929	26642	\$5\$52	21859	18215	14453	10891	-26.4	4359-	-1356	\$687-	-7249	3808	12851-	14449		125
120	39244	300.5	34505	34101	31374	\$2267	24905	21563	17709	1,973	1387	9374	8°58-	481	8.67-	-685 -40.5	4, 35	-11598	1477		120
1. LUNG	0	~	-10	-15	04-	->5	- 30	-35	01-	57 -	- 50	- 5 5	09-	-65	-70	-75	- RO	-#-	06-	141	1. 10%6

2.5 t-	31033	39782		30363	30 50 50 50 50 50 50 50 50 50 50 50 50 50	200 200 200 200 200 200 200 200 200 200	202 202 203 203 203 203 203 203 203 203	20 50 50 50 50 50 50 50 50 50 50 50 50 50	01	01	04 04 04 04 04 04 04 04 04 04 04 04 04 0	24 24 24 24 24 24 24 24 24 24 24 24 24 2	04 04 04 04 04 04 04 04 04 04 04 04 04 0	21 21 21 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	21 71 71 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	04 04 80 80 80 80 80 80 80 80 80 80 80 80 80	04 07 01 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	04 07 01 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	04 04 04 04 04 04 04 06 00 04 04 04 06 06 06 06 06 06 06 06 06 06 06 06 06	04 07 01 40 02 84 07 86 80 94 04 80 04 07 07 07 07 07 07 07 07 07 07 07 07 07	20014 20004 -100 20004 -20015 -15 20176 -20015 -15 20176 -20015 -15 20176 -20016 -15 20016 -20076 -15 20018 -20076 -15 20018 -20076 -15 20018 -20076 -15 20018 -20076 -15 20018 -20076 -15 20018 -20076 -15 20018 -20076 -15 20018 -20076 -15 20018 -20076 -15 20018 -15 2
																				22 22 22 22 22 22 22 22 22 22 22 22 22	
	31570	31881	2313	30708	-47.1	29895	29895 -35895 -35895 -445	200 200 200 200 200 200 200 200 200 200	200 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	25 25 25 25 25 25 25 25 25 25 25 25 25 2	24 24 25 25 25 25 25 25 25 25 25 25 25 25 25	24 25 25 25 25 25 25 25 25 25 25 25 25 25	24 25 25 25 25 25 25 25 25 25 25 25 25 25	24 25 25 25 25 25 25 25 25 25 25 25 25 25	2	2	4 001 001 5	4 901 901 50 50 501 501 501 501 501 501 501 501	4 9V 9V V V V V V V V V V V V V V V V V	4 90 90	4 91 90
	31,07	3863	33A12	31196		30231	30231 -38.8 -28985 -24.3	30 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	20031 20031 20031 2006 27504 25504 25506	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20 21 20 21	1	1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000 000 000 000 000 000 000 000 000 00	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1	0 1 2 1 2 1 2 2 2 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	32074	38363	32825	31593		30559	30559 -39-2 29208	39.2 29.2 29.4 2.2.4 2.4.5	2055 2055 2055 275 275 275 275 275 275 275 275 275 2	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20	201 251 55 55 55 55 55 55 55 55 55 55 55 55 5	201 201 20 20 20 20 20 20 20 20 20 20 20 20 20	201 521 55 52 52 52 52 53 53 53 53 53 53 53 53 53 53 53 53 53	201 521 55 52 52 52 52 53 53 53 53 53 53 53 53 53 53 53 53 53	81 91 91 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	NI NI NI N N N PI PI PI I I I I I I I I	\$1 \$1 \$1 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0
	32367	3313	\$2843	31988		30879	284.7	20879 20879 20879 20879 27687	30 95 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	20 52 52 50 50 50 50 50 50 50 50 50 50 50 50 50	24 42 42 52 52 52 52 52 52 52 52 52 52 52 52 52	20 00 00 00 00 00 00 00 00 00 00 00 00 0	24 42 42 42 42 42 42 42 42 42 42 42 42 4	00 00 00 00 00 00 00 00 00 00 00 00 00	00 90 VL VI V V EI EI EE OV VV BU VI VI BU VV VV BU VI VI BU VV	00 90 VL VI V V EL EL EL VI 00 90 VL VI	00 90 V V V V V V V V V V V V V V V V V	00 90 Vi Vi V V II II BE NV VV BU VU UV UV UV VV VV VV VV VV VV VV VV VV	NI VI V V V EI	21 91 91 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	21 01 01 0 0 0 01 01 01 01 01 01 01 01 01
	32679	33154	\$385	32372	31185	-31.8	29605 2605 -26.9	20.00	20 00 00 00 00 00 00 00 00 00 00 00 00 0	20	20 00 00 00 00 00 00 00 00 00 00 00 00 0	20	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0 VI VI VI VI VI EI EI EI EV VI	2	2	2	2	20	2	1 V1 V1 V1 V V V E1 E1 E1 E1 V1 V V V V
	33306	11533	138:3	35729	11461		29763	29763	29763 2775 2775 2775 2775 2775 2775 2775 277	22 22 22 22 22 22 22 23 24 24 24 24 24 24 24 24 24 24 24 24 24	227.52 227.52 227.52 227.54 23.64 24.75 24	22 22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	22 22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	22 22 22 22 22 22 22 22 22 22 22 22 22	22 22 22 22 22 22 22 22 22 22 22 22 22	22 22 22 22 22 22 22 22 22 22 22 22 22	22 22 22 22 22 22 22 22 22 22 22 22 22	22 22 22 22 22 22 22 22 22 22 22 22 22	01 VI	01 VI VI VI VI VI VI TI TI TI VI	VI VI VI VI VI VI EI EI EI VI
	11322	53887 -0-8	34708	33943	31691		29876	232.4	29874 27777 27777 27777 27777 27777 27777 27777	2387 25.25.2 25.28.2 26.28.2 26.28.2 26.28.2 2	2387 2757 2558 2558 2558 2585 2585 2585 25	2387 2787 2787 2787 2787 2787 2787 2787	200 200 200 200 200 200 200 200 200 200	200 20 20 20 20 20 20 20 20 20 20 20 20	\$50 \$50 \$50 \$50 \$50 \$50 \$50 \$50 \$50 \$50	\$5	25	200 200 200 200 200 200 200 200 200 200	\$1 \$2 \$2 \$2 \$2 \$2 \$2 \$2 \$2 \$2 \$2 \$2 \$2 \$2	24 24 24 24 24 24 24 24 24 24 24 24 24 2	2
	13642	14.510	30175	33206	11860	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	29952	29955	28485 28485 28482	24657 24667 24667 24667 24667 24685 26685 24685 24685 24685 24685 24685 24685 24685 24685 24685 24685	24657 24657	22	VI V	VI V	VI VI VI VI EI EI EI EI EI VI	27	25	21	25	21	25
	3,001	8.848	8.8.8	5.480	11965	31001	6.447	27552	VA 000	24 24 25 25 25 25 25 25 25 25 25 25 25 25 25	71 71 71 71 PT	00 04 000 00 mm 000 00 mm 00 00 00 00 00 00 0	VO VIA 8080 NO NAU NEO 624 VI NIA 614 VI NEO WA 04 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI 614 VI NI	AG AN BORD MON MAN AND GON GOD IN A A A A A A A A A A A A A A A A A A	AG	NO	NO	00 04 000 000 000 000 000 000 000 000 0	\$\text{\$\frac{1}{2}\$} \text{\$\frac{1}{2}\$} \$\	24	24
141	0	?	-10	-15	02-	ļ	S -	C/-	- 40	S	145	\$	\$		\$ 0	04	54 04 04 04 04 04 04 04 04 04 04 04 04 04	0	24	\$ 0	14

9 10 NC	057	597	652	552	760	597	2.0	\$ 2	८ 8√	245)6 /	562	t. 1046
													1 4 1
0	37905	20262	5923	62885	8. 35	30063	29716	20204	28817	28413	27814	1.177	~
	\$2828	2.24	36171	29998	29805	28358	1: 862	1:882	28357	2,832	\$ 18877	£\$ \$ \$ 5	•
-10	0.667	29693	29853	\$\$\$\$2	\$285.	80262	87862	38985	24842	27038	9,837	25911	-10
-15	23446	28903	26505	N. 81	2,040	£\$\$\$	27,923	\$2052	26546	2888 -3888	£\$\$\$\$	25858	-15
-20	\$ 40 ° 5	26016	27645	27289	4.695	26607	26242	25827	25343	24877	24127	4.95-	02-
->\$	27643	2,18,3	82832	30892	2-808	25813	28918	58888	24318	223.3	22920	22189	~ -
0k-	26535	75946	25528	25102	2.6.2	24373	23877	23464	23012	22494	218.2	21189	0 -
- 15	23862	85242	24377	24801	245	23808	23813	35552	85135	21708	\$\$\$\$\$	28318	-35
0*-	2 56 56 8 . 5	73423	23181	72924	22668	22418	2382	23815	21813	\$355	287.99	2022H	0 -
-45	22059	22012	21947	21975	21798	23,722	21637	21525	21362	23318	29262	20291	59-
-\$0	29359	50802	\$8852	29819	4-85-	21096	80082	23877	21274	21174	36895	32882	- 5.0
-45	18485	18865	19255	19649	29937	29505	8.265	29393	21168	21339	21159	28943	ş.
0.4.	15477	17016	17649	18968	15988	19873	29862	20465	20825	23855	2,012	21114	09-
-65	14047	13879	15707	16544	17363	18144	18864	19502	20038	29454	88.89.5	206 8	59-
-70	11308	13378	13328	36261	15388	19323	17808	19801	13801	19898	19378	29128	- 70
-75	8393	9555-	10710	11851	12966	14036	15048	15984	16839	17597	18252	18800	-75
-80	-123	4528	7795	9047	10259	11434	12355	13613	14598	15501	16315	17838	0 % -
- # S	2137	3497	48.4	6386	2483	8748	1400	11118	128.19	15229	14163	15915	\$ a -
06-	1.3	100	2 4×5	3885	8,8,	6198	7489	10.2	11.2	19281	11990	12907	06-
•													- T
	.,				9.7			,	00.	9 0 5			

1 + 1 0 N 6	9	? .	-10	-15	-20	- ->\$	- 30	-35	-40	59-	05-	-45	09-	-65	- 70	- 75	-80	S & -	() 6 -		f . 10NG
\$55	26924 -11.P	25612	20263	17213	1887	12728	11411	10729	10695	133.58	15865	14002	15656	17133	12681	13401	18276	17113	1307		155
150	26461	\$330\$ 2018 2	\$5675	17327	1,4801	13200	11000	11878	11195	13539	12836	14338	15984	17868	12529	1 #968 - 3.4	18667	1.35.5	15868		150
348	26103	23127 -32.8	29187	17566	15411	13756	12588	13828	11809	18874	13318	14766	16373	17829	18.00	19383	18971	17803	15925		345
440	25858	23099	29373	17943	15941	16395	13290	12638	12497	15855	13898	15383	16824	18214	18281	19543	19189	18978	16268		140
3.65	7.27.27	23217 -38.0	58813	18459	16562	15113	14050	13428	13276	13809	12278	15885	17433	18623	18489	19750	19319	19191	1628A		\$ \$ \$
130	25684	2.463 -40.6	£\$\$\$\$	19103	17325 -83.1	15816	14891	16276	14125	18487	15346	16559	17891	19948	19878	19900	19362	1835	19 2 4 5		0 1 0
\$2\$	25730	23810	23882	19845	18152	16782	15778	15178	15032	18373	62861	17285	18469	19475	\$2862	19989	19315	18928	16157		\$5\$
67.	25848	24227	588.3	39855	19016	17696-8-86-8	18608	18117	15975	18598	13839	17016	19076	40836 19936	82862	20002	19176	17888	13808		420
315	26029	24688	23123	18812	19947	18637	18958	17073	16929 -87.8	18358	17891	18777	19650	2025A	29893	18353	18943	25721	1883		3115
410	26270	25173	27812	22323	29829	19579	18605	18219	17863	32187	17.12	10471	20170	22566	12862	18813	17614	16.489	139:8		U 1.
\$0\$	26\$75	25676	9.65-	25154	21750	29501	19527	1585	18743	19853	18458	20083	20604	20787	\$9862	19576	16187	16431	115.28		\$0.5
001	2,6979	26196	25269	24915	72827	21378	20307	19768	19539	18985	₹39%	2.85-	20925	53835	\$7987	19240	17001	37851	6771		30,
141	0	∵	-10	-15	->0	->2	0, -	-35	07-	-45	-\$0	-55	09-	-65	-70	-75	04-	\$ 4 1	06-	141	F. 1046

Table 1	f. 10N6	c	٠,	<u>-</u>	1.5	u?	\$2	30	33	0,	\$	2.0	\$	1. 10N6
	141													[4]
14-1 CC CC CC CC CC CC CC	96	1158	14.5	15.3	15.9	12.0	16.3	10	3.06 6.06	368	6.1	609	\$ 1 m	00
	£	18.1	-944	15.4	13.0	12.2	10.4	7.82 8.7	10.76 8.8	1340	1570	1764	1919	*
1.7.1 0.5 0.5 0.7 </td <th>080</th> <td>-3469</td> <td>1963</td> <td>1962</td> <td>15.35</td> <td>13.19</td> <td>1070</td> <td>1502</td> <td>1201</td> <td>2133</td> <td>29.19</td> <td>2638</td> <td>6627</td> <td>0</td>	080	-3469	1963	1962	15.35	13.19	1070	1502	1201	2133	29.19	2638	6627	0
	2	-1622	-1023	19.22	16.6	14.3	1286	1792	2250	7651	2986	3245	3422	2.5
	0,	-1717	-1061	20.9	17.9	841	15.5	1970	2468	2908	3281	3574	\$7.78	0.2
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	\$\$	-1738	-1057	-392	1551	1867	12.5	1996	2439	2949	3337	\$ \$ \$ \$ \$ \$ \$ \$	3875	6.5
14.1 14.2	0	-1688 -7-1	-1002 28.3	-345	20.1	865 16.3	12.7	1930	2405	2835 4.8	3211	35.25	3751	09
11-11 12-2- 12-2	\$\$	-1500	51.5	26.5	}	1963	13.68	1823	23.45	3.4	2967	3248	3458	\$\$
1863 5874 1878 1879 1879 2514 2514 2515 2515 2515 2516 2515 2517 2518 1879 1879 2519	0	-1677	34.9	36.2	24.6	38. 30.	13.28	\$08.	2005	23.85	5003	2882	3053	80
-1856	\$\$	-1363	30.5	P	\$2 6 5	24.3	8:38	1898	3661	5772	2343	2832	3857	*
1526 5464 5464 557 558 558 558 558 558 558 558 558 558	0.4	-1349	25.32	18.3	34:1	2.00	12:5	4.0 0.0	1331	1919	\$225	8072	20t2	0 7
6771 678 78 6	3.5	-1572	4064	45.6	35.0	26.65	18.0	1374	1586	1723	1771	1738	1644	3.5
62.1 62.2 15.1 15.2	30	-1495	52.8	- 191	39.3	20.3	20.2	13.6	1449	1555	1540	1414	1315	3.0
65.51 65.64 <td< td=""><th>\$2</th><td>-1717</td><td>55.8</td><td>-394</td><td>\$ 9 U \$</td><td>451</td><td>29.2 2.2.8</td><td>10.00</td><td>1308</td><td>1398 3.6</td><td>1331</td><td>1119</td><td>812 1.0</td><td>~</td></td<>	\$2	-1717	55.8	-394	\$ 9 U \$	451	29.2 2.2.8	10.00	1308	1398 3.6	1331	1119	812 1.0	~
-2463 -3689 <td< td=""><th>02</th><td>-3953</td><td>-1865</td><td>3665</td><td>53.52</td><td>193</td><td>23.7</td><td>40°6</td><td>2581</td><td>1531</td><td>1316</td><td>\$ 2 %</td><td>430</td><td>20</td></td<>	02	-3953	-1865	3665	53.52	193	23.7	40°6	2581	1531	1316	\$ 2 %	430	20
-2869 -2164 -1819 2705 32.8 2823 1509 1552 1815 1916 -918 -1954 -1955 - 1855 1815 1918 -918 -1955 - 1955 -	\$\$	2442	-1689	-1073	-567	36.9	200 200 200 200	2 1 - 8	16.51	1928	\$°\$	£0\$	13	1.5
- 18:4 - 63:4 - 59:4 - 18:1 18:4 18:4 18:4 18:4 18:4 18:4 18:4	10	-2968	-2184	-1539	4.4.4	40.0	32.8	3552	10.01	15.3	1353	303	-457	10
-4113 -5134 -2610 -1962 -1523 -739 -281 -45 -105 -470 -1069 -1770 67.0 -51.9 -59.2 -46.2 38.5 40.4 57.5 15.0 -17.0	~	-35.35	9.59-	-3979	-1861	\$ 8 5 7	33.8	101	373	18.81	11.8	804-	-1943	~
0 5 10 15 50 55 50 40 45 5V 1-1	0	-4113	-5338	2.65	-1961	-1323	-739	10.4	22.55	15.0	9.8	-1069	-1770	9
0 5 10 15 50 35 40 45 50 55 1•1	141													1 4 1
	E. 10MC	c	~	10	15	07	\$ 2	30	3.5	0.7	5 7	٥٢	\$\$	3 NO 1 - 4

f. 10MG	9	v «	٠,	\$	94	SC	36	`	169	105	011	115	1 . 1 ONG
141													141
00	1918	3711	1136	27.85	1610	1433	1839	18.81	2818	-\$878	1313	-1338	00
~	20.4	£103	\$775	23.6	\$u{z	2045 846	1850	10.37	8:21-	-1574	11.38	11:09	** *
90	28 R 4	\$067 7067	2854	22.42	2865	2332	2052	1749	-101-	-1081	-10.5	-10.2	၁ ဖ
23	1510	3505	3405	3212	2911	2569	2139	1657	1141	613	\$6 6-	1.0-	2.5
0.0	7.6-	3879	3352	3522	3172	2717	5369	1549	42.00-	-189	-505-	-1147	70
9 2	2008	\$00 ,	3488	3639	258	2348	\$123	1601	-6.3	108-	-1024	-1795	65
40	4882	3904	3798	3555	8215	2645	600 601 601	1518	-363	-539	-1448	702-	90
\$\$	1583	3606	3512	3286 3.4	2920	2411	1763	2.4	122	-809	-1753	-2655	\$
\$0	1147	3157	3067	2862	2530	2063	1461	7.54	-101	-1008	-1941	-2841 6	\$ 0
4.5	2628	7405	2509	2824	2036 8.8	1833	13.3	459		-1138	-2908	1982-	\$
0.	29.72	606 7	187	1717	15.3	13:4	1531	1389	19.4	£111-	1854	\$222-	0,
:	1519	1.83	1241	108	11.7	13.5	332	13.0	-553 10.5	-1134	-1784	-2453	35
3.0	901	7 8 3	605 6.5	₩.80 •\$** •\$**	308	150	1.41	15.45	1-6-	-1023	-1524	-2065	30
\$2	4.95 2.8	\$1.5 \$1.5	1 0	13:1	1351	1329	13.0	10.3	-614	-858	-1193	-1596	52
20	5. ¢	-434	-583 -5.6	11.n	-780	12.3	1000	-615	-581	899-	-10.5	-1083	2.0
15	-473 7.5	~= · · · · · · · · · · · · · · · · · · ·	-1157	10.01	-1290	-1177	7.6-	7 50	-5 \$1	-420 -8.2	-440	-10.8	15
91	-1016	-1969	95%1-	1908	-1919	1598	-1265	868	F 6 9 -	-1418	3-21-	-12.83	10
•	-16.6	-2138 2.8	-2428	-2507	-2580	-2064	-1597	-1047	-512 -6.6	-12.1	-17.8	121	•
o	-24.28 -2.8	1267-	1021-	-3245	\$70x-	\$292-	5202-	-1424	-634 -6.5	-11-0	352-	610	ŋ
1 A T E. 10NG	0.9	\$ 0	07	۲,	6	£	06	*	100	105	110	115	L. 1046

t. tone	150	521	130	115	140	145	150	145	160	145	17.0	175	9 10 1 - 3
[2]													1 4 1
06	-3173	-\$171	-3153	-4323	-39.28	-1804	-1923	-1823	1718	1595	16.0	1314	0
\$	-1174	1901	-1168	-1798	8-41-	-1913	1909	-19-3	8-81-	9.31-	1361-	-1933	\$ €
0	160	76-0-	1 1 2.0 3.0 4.00	528-	-424	904-	326-	-187	-7.5	900 5 * 0	-8.35	832	Û W
23	-821	-1176	-1439	-1594	-1645	-1578	-1400	-1118 -4.0	-747	-401	198	731	22
0,0	-1716	-2181	-2518	-2709	-2742	-2617	-2337	-1917	-1375	-735	-26	723	
6.5	-2476	-3030	-3423	-3632 R. E.S.	-3662	-3453	-3974	-2523	-1828	-1929	-135	794	45
90	4904-	-3678	-4104	-4312	-4289	7503-	-1561	-2897	-2076	-1137	-120	933	9
\$\$	-3456	-4097	-4530	-4721	-4654	16331	-3775	-3718	-2303	-1076	918-	1138	\$\$
20	-3845	-4279	-4695	7-63-	1:87-	1767-	3813	-3885	-1368	-12.3	-18%	-1128	\$0
\$\$	- 3628	-4233	2065-	4125-	-1838	1991	808 k-	-43.18	1808	-1513	2021-	1197	\$
0.	185-	-3978	6687-	24338	-1838	3388	-3849	1636	-1918	-1166	1849	-4365	0.4
45	- *064 -5.8	-3531	-3776	-5752	-3448	-2887	-2114	1188	-172	-1872	1883	-1911	\$
30	-2570	6-11-	-4106	-3006	-2639	-2033	-1240 -9.8	-317	-12.9	1664	2594	3407	10
\$2	-1984	-2256	-2326	-2148	-1721	-1080	-279	654	1570	2494-10.6	3328 -15.5	4016	\$2
20	1349	-1515	-1492	-1237	-756	16-	705	1576	2466	3311	4042	0091-	9.0
1 5	-711	-212	-17.8	-334	191	00.4	1650	12.0	3306 9.5	4064	4698 -6.2	51.5	\$
10	-2115	6.55-	-133	1808	1062	2.7.	3399	\$583	404 845 86	4735	5473	\$6084-	0.
~	-23.5	534 -21.8	-16.8	1234	1810	2485	35.26	3056	1007	\$ 5 9 0	8525	6017	•
0	2.04-	1851	-1255	1928	81.45	1285	15.3	14.88	\$3.28	<i>\$:1</i> }	6358	6285	0
141													1 4 1
F. 1046	170	125	1 30	135	140	145	150	155	160	165	170	175	1. 1046

13.54									
- 13.54									1 7 1
-10.4 -10.5 -1	₩¢	-1873	48.0-	-106	-3.5	87-	199- 199-	200-	06
-113.6 -143.73 -148.04 -148	~	1207	-1153	1065	942	783	2.00 0.00	365 7.8-	Š
14.83 14.83 18.84 18.84 19.85 19	~~	-4878	-4351	-1836	-15.82	-16.8	-1915	-1823	0 M
2555 8565 9566 9566 9566 9566 9566 9566 9		3397	3582	3660	3626	3480	1223 -22.8	2863	2.2
2.242 2.	-0	4459	4737	4876	4872	4723	4434-28-9	4011	7.0
28.54	0·m	5368	5718	5907	5929	5783	5475	5012	\$ 9
\$184- \$1	36.89	-26.7	6455	-9982	-\$6.0	-37.1	6293	5819 -35.4	09
- 45.59 - 45.56 - 15.06 - 1	~	-2584	-4913	-3165	-36.7	7134	6853 -38.4	-36.8	\$\$
- 38.56	۰.	-23.0	-27.6	7359	7456	7386	37.18-	5385	\$0
- 1806 - 1906 - 1506 -	o-4	-1682	-23.8	7898	-32.19	1383	7201	-53.6	\$ 7
-1824 - 16.6 - 1	Nen.	42.9	8-25-	2.68-	-33.28	-3378	-4858	£.28-	0
-50.2 -50.3 -48.8 -48.8 -50.5 -53.5 -53.5 -54.7 -54.6 -54.7 -54.6 -54.5		-11.3	6446	-16679	-22.23	6834	1:16-	-9362	3.5
-55.5 - 55.0 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 54.67 - 55.00 - 54.69 - 56.59 - 54.67 - 54.68 -		-1415	-6843	-933	-6363	-8232	-16.3	6236	0,
-5856 -5328 -5164 -5655 -5576 -5876 -5774 -5620 -5036 -5274 -5620 -5036 -9254 -5428 -2639 -6478 -9498 -5636	9	-1982	5645	5799	5914	5966	5948 -6.5	5856	\$2
5352 -53.76 -32.74 -52.44 -56.20 -54.27 -925.4 -35.00 -40.60 -925.4 -34.98 -26.59 -63.76 -94.98 -35.78	~~	-5505	-1308	5414	5503	5546	\$5.36	3285	20
-55.4 -56.0 -40.6 -9254 -54.98 -26.5 -64.8 -94.98 -58.58	~ c	-5813	5053	5.121	2285	\$199	5184	5145	15
-3498 - 2558- -9498 - 5328	~	-2948	4937	4.60	14977	19.5	1,67	7.67	10
-9498 - \$928	~0	5028 -28.8	4976	2507	4936	27.1	48.48	\$818	~
	œ	-\$658	-\$333	\$3.5	\$863	\$368	\$828	2903	c,
									, T 4 1
E. 10NG 180 185 190 195	5 200	502	210	215	022	\$22	230	515	1. 10M6

F. LONG	549	545	750	255	767	592	270	275	780	285	590	\$67	1 . 10MG
1 4 1													LAI
06	-1014	-1177	-1352	2261-	-1610	-1731	-1839	1933	-2013	-2076	-2124	-2156	06
35	-3.4	1969	7.4-	-383	-1101	-1423	£\$1-	26.95-	-2318	1:82-	-2704	\$288-	8
0	-1873	-1961	-160\$	7.8-	00°9-	-1123	-1642	-2349	-2616	-3045	-3428	1235	80
2	2406	13865	-1855	-13.0	-19:3	-8-8-	-1542	-2234	-2884	-3475	-3991	3-44-	2
0,	3465	2810	2063	1244	1375	-1129	-1415	-2284	-3400	-3840	-4484	-5813	20
\$	4404	3666	2816 -24.8	-217.3	40.01-	-1183	:14:3	2:22-	-3243	-4123	1687-	-5505	65
40	-33.0	\$\$6°	35.86-	-3873	-38.1	1987	-1603	: \$183	-3397	-4309	-5183	-5883	9
\$\$	53.8	5010	4085	3023	1848	589	-714	-2013	-3258	1675-	-5175	-6156	\$
\$0	-43.83	-2859	4555	-3503	-2308	tob?-	-2879	-1274	-3126	-1373	-5456	-6326	\$0
\$\$	6376	8745-	8.86-	-3985	-33:3	-23.5	1-22-	-3563	-33:1	-3568	-\$\$\$\$	4049-	\$
07	-9389	- \$4.7	50%	-2353	-38.8	1328	312	-3369	-3853	<u>-4883</u>	-3355	to 6 8 -	0
45	-5345	-\$6.79	-\$348	-3111	-3878	-385\$	-1878	-40.0	-23.68	-3838	1818=	-8323	\$1
30	< 4905 -14.5	5626	\$099 -15.7	4382	1455	2318	995	-467 -48.2	-2001	-3525	-4944	-6180	30
22	5684	5409	4996-	-1705	3595	2563	1319	96-	-1618	-3169	-4648	-5976	\$2
20	5364	5373	4 7 4 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	-1218	-3733	-2915	-3859	\$6.39-	1994=	-3863	2585	3218-	20
\$	508.3	1973	6.1,	-1561	-28.9	3086	-\$818	-717	-78.0	-5349	-3926	-5428	15
10	4884	19.0	4764	4512	4075	3379	0.44-	1156	-300	-1889	-1519	-5100	10
~	8008	\$233	662,	4829	-56.8	-1863	-2 3 8 8 3 -	1801	P. 88-	-1419	-3086	\$? \$ 5=	~
ن	44 44 44 44	1963	4853	3085	4503	398A	4175	-82.0	663	-928	-8924	-4324	0
LAT 1. 10NG	072	542	7.50	\$\$?	760	585	270	2,5	280	285	990	\$67	1 A 1 ONG.

9N01 .	400	\$41	110	315	07.	325	4 3.0	3.45	140	345	150	\$\$\$	1 . 1 DM
													1 ¥ 1
0.	-2172	-2171	-3153	<u> </u>	15.8	-2004	1923	1827	1718	16.3	14.60	15.6	5
85	111t-	-\$212	42.58	-3255	-3203	-}908	-2954	-2762	-2524	-2863	-1963	1649	•€
0	16.5	-4155	1.94-	-5563	2386-	-\$858	-3846	-3509	-3833	\$255	9:18-	-1853	ec .
23	16.8	-2888	\$368-	-33:1	-3928	-4845	-5569	9.38-	3888-	-3308	-3373	-8808	~
7.0	16.4	-5883	-5815	-5913	36.7	-33.8	-3308	-3673	-\$168	2088-	-3005	-2368	7
65	-5963	-6259	-6.590	-6363	8-63-	- 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2:68-	-497	44. 60. 60.	-3768	-3106	-2424	9
40	12.4	-9813	-9838	\$208-	-4553	-6-18-8 58-88-8	0-13-	-5138	4503	-3018	-3119	-{395	9
45	6779-	16.7	-7175	-7083	6.95 36.95	-6389	-5850	-5225	4532	15003	-3055	-2312 38.9	•
20	6.4	13.0	-7431	-7315	9082-	-6536	4.94	-5275	48.3	-3770	-2986	-2214	\$(
4.5	₹	-1808	9.85-	-{513	-7178	-6678	48055	-5345	\$6.85	-3765	-2945	-{11.1	•
0 4	137.	4.81-	-7819	9:33-	-3378	-6463	86.98	-3479	P. 85-	-\$456	-5864	-\$124	7
35	-7193	1321-	-1992	-7937	-7639	#2{}-	£288_	-\$311	54.9	-3980	-38.9	-2186	*
0 t	25955	8-82-	-6374	\$0 \$ 8-	-7964	-7495	-0.00 A	}•6	1:18-	2.85	2.98-	-{34.}	7
2 \$	-7071	-7876	-6359	17.5	-8373	39.08	47.80	-6542	8:65-	-4614	-3587	-2600	₹
20	-4840	-3895	-8535	-47.2	-98-3	8088-	6:82-	\(\) \(\) \(\	4136	-\$028	-38.88	-8854	₹
15	7-17-	-3863	-8674	4710-	-9265	33.2	44.0	-7682	-6688 \$ 505	-5185	-4463	-3398	45
10	£4 \$ 4\$	-1785	9,91=	998-	-9613	7:88-	Sapa-	\$205	3092-	5688-	2964-	-3908	10
•	-6475	-7823	\$686-	6,85	\$020-	878-	-9320	-8582	4-85 4-85	-6557	1248-	-244 3	•
0	-2839	:1358	-8513	1830	5-20-	-9788	3: 82-	2228-	\$682-	-8818	-8833	-4875	3
A 4													44
9N01 -	400	\$0\$	110	315	u2.	\$2\$	130	515	140	345	350	\$\$\$	1. 10M

141	0	}-	-10	-15	02-	-25	- 30	-35	07-	57-	05-	-55	-40	5 y -	n ₄ -	-75	0 % -	\$ a -	08-	1 4 1	1. 10NG
₹. 2.	8221-	2007-	\$ 28 =	-4967	-6325	-}254	7917-	-19526	-13778	-13879	13838	-14651	-15313	-15821	18168	-19458	-16402	-16128	19851		\$\$
2.0	-1063	-1903	-2014	2.26-	-\$415	6188=	-8833	8656-	-10866	-15608	-12803	-13879	-14592	-15164	-15895	-15869	-14801	-16013	-15808		2.0
Ş	7-4-024-	5121-	-2329	-1518	-5451	-\$685	1587-	-8498	-83.4	-19343	50837-	-12926	-13719	-14371	-14879	-13543	-15479	-15566	-18838		57
0.4	-105	13.5	-1533	-2485	-3581	3.945	25452	=1343	-8598	-9789	-10888	-11876	-12738	-13463	-15453	-19503	3785	-15003	13858		0.7
45	22.55	23.0	1238	-2029	5362-	- 1875	-3491	-6263	-3458	-8423	=8358=	-10779	-11696	-13485	1,181-	13862	-14901	-14359	-14148		€
30	1.01	29.95	-3281	1915		8:3-	-1873	-5376	-2343	2:82-	-8453	-9693	-12638	-11465	-12368	13751	-13213	-13545	13129		80
\$2	-739 38.5	-1170	-1938	-3233	-2621	-1133	-3958	-4753	-3835	-9844	1967-	-8569	-9601	-19634	-13158	52212-	-13383	13865	11881		\$
70	-1323	-1771	-2508	-2813	-2996	-3392	11847	-4411	-1102	2285-	-8828	=3348	-8617	-9419	-16136	-19753	-11579	80211-	-11998		0.2
15	-1963	-2455	-5893	7:25-	-1813	-3741	-3884	12.0	6635-	-\$108	-6143	-6925	-17.05	-8437	-9368-	2666-	-10518	-19854	-14381		15
0.1	-8839	2918-	-3428	-3945	-\$33\$	-4523	8824-	-4410	-4868	1385-	608 -	1.25-	26.87	-7500	800 48	-8621 -6-2	3-15-	6.8-	5 4 4 5 -		01
~	-3338	-5843	-6343	-4641	-4765	-4753	-4973	37.5	6268-	2-84-	-1703	-5638	-6123	-6613	-7085	-7333	6562-	-8359	-9823		. `
0	-4313	-4643	-5058	1059	-5367	-\$\$68	-\$9.28	-4883	7.994-	8015-	8075-	-5145	-5443	-5775	607-	6. 74-	4777	-2328	2°6-		3
E. LONG	3	٠,	-10	-15	-20	->}	-30	Sh-	01-	\$4-	05-	-55	09-	-45	04-	-75	0 K -	-85	06-	[4]	1. 10MG

09	5.9	6.2	7.5	€	88	Úđ	66	100	105	110	115	£ . LONG
												141
•	2287-	105-	-3365	4505-	-2627	\$ * -	-1324 -1324	-634	-11-6	7.81-	4191-	a
, ,	-1865	-4121	117-	-1833	-3312	-2836	-1746	3.3-	=183	190}	-1{5}	\$,
, ,	-13.8	1:11:	-5323	\$285-	2515-	188-	64.2-	-1369	-493	~ ~,	-6.33	04-
٠,	-6178	-4373	-6265 -10.R	-5855	-5156	-4218	-3132	-2019	-998	144	\$33	-15
, ,	-7503	-7662	-7508	-7043	-6281	-5267	-4086	-2855	-1693	7.0	160	02
• •	-8883	-9003	1088-	-8298	8662-	-6425	-\$17	-3844	-2555	1589	-380	-25
۳,	13887-	-19342	-10113	-9574	-8738	13.5	2789-	-4944	-3549	-{243	-1867	0 .
Ξ,	-11570	-11631	-11382	-10827	15.8	1870	1353	-6111	-4635	- 5207	-1878	-35
7'	-1473	-12830	-12576	-12022	-11181	-10080	-8764	-7302	-5772	-4248	-2784	0 >-
ī	-13857	-13910	-13665	-13128	-12310	-11234	3566-	-8478	0269-	-5329	-3758	54-
-14443 -1	-14786	-14849	32671-	-14118	-13333	-12898	38 611-	6086-	-8049	-6413	125-	- 50
-15224 -1	15557	-15928	-15439	-14958 3.6	-14223	-13233	-12924	-10629	-9093 -9.8	-7465	-5793	-55
-15846	-14359	-16435	-16054	-15618	-14929	-14002 -0.8	-12857	-11523	-19943	29953	-6797	09-
7'	-16581	-16643	-16475	-14879	-15432	-14871	-13503	-12254	-10852	-9333 -15.8	-7731	59-
-16583 -1	-16816	-14958	-14883	-16505	-15715	-14923	-13942	14391	-11493	-16678	-8563	- 70
7	-16874	-16876	-16696	-16332	-15785	-15060	-14168	-13123	-11943	-10644	-4253 -10.2	-15
-	-16778	-16738	-16541	-16185	-15672	-15007	-14197	-13252	-12184	-11908	-9738	0 8 -
7'	-10579	-199RZ	-16267	-15911	-15420	-14799	-14054	-13190	-12217	-11144 -9.8	-9981	28-
7,	-16289	-14268	-15655	-15563	-15978	-14586	-13773	-14848	15858-	-11846	356-	06-
												A A
	\$ \$	2	22	8 U	8.5	U6	66	100	105	110	115	9N01 - 1

170	125	1 50	155	14.0	*	120	<u>^</u>	00	601	0 / 1	6/1	
												1 4 1
	1021	-1354	1824	2412	3077	15.3	10.6	5159	5737	6159	45.5	J
	1364	1760	23.64	7863	35.25	4210	4084	55.4 6.4 8.4	\$3.5	6494	940	S-
	1552	2018	23.85	3178	3849	4559	10.0	\$ 9 5 5	9377	8239	6669	01-
	foèt	2138	3212	4376	4058	4752	5433	6068	6617	6.62	1384	-15
	1503	2133	2792	3487	4204	4923	5256	8,5,	4-4	7265	7554	0 < -
	1271	2018	2766	3558	4295	2953	5774	64 38	7015	5.9	7806	\$ ~-
	813	1802	2 669	1503	6724	4143	86 K S	65.85	7362	7669	8035	- 30
	640	1487	24.75	3454	4334 5.84	2104	5 9 8 9 5 5 9 8 9 5	£029	7321	7833	82 30 9. 8	\$ z -
	-123	1978	10.3	1961	10.5	5186	\$209 6058	92.6	7423	7958 8.8	10 M 80 4 M60 20	07-
	-813	5.49	1303	2892	1258	\$988	\$88\$	8238	1963	88 39	8491	59-
40	-1597	-313	1284	3583	\$778	41	\$883 883	8888	{ \$1\$	12.21	8535	05-
~	1:45-	1000	\$ 0 0	\$508	1331	1968	3818	8878	1859	33.58	8503	\$5-
-5105	-3429	-1295	-228	12.4	3623	£. €. €. €.	\$0.05	\$058 \$054	9821	8081	8378	09-
~4	-4423	-2783	-1190	45.0	1368	3303	3:44	55.45	15.6	7349	6153	ς γ-
~	-5368	8.78-	-2316	6.8-	MB 6-6 8-6	{193	3505	1723	5851	1581	1838	-76
-	4835-	4.1.	-3213	-1692	-308	1245	26.0 20.0 20.0	3935	\$183	\$ \$\$\$	1454	-75
~-	-6987	-5519	7.00	-2583	-1308	358	1785	3174	4515	5800	11.0	·) & -
~	8:87-	£280-	8967-	8:21-	-1789	3.8	1108	25.82	3839	2.85	45.8	S& -
-0=	9957-	-6479	-4944	135.3	1212-	-755	195	2085	3486	\$0 8 7	08 4 X X X X X X X X X X X X X X X X X X	06-
												1 * 1
	125	1.50	135	140	145	150	155	160	165	170	175	1.1046

f. 10N6	L A 1	0	~	-10	-15	20	->\$	-30	- 35	07-	-45	05-	- > >	-60	-45	- 70	-75	0 K -	-85	00-	1 4 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
215		1987	\$ 83 ?	}	\$	\$5.18	205	7875	12.5	9513	10406	11320	12222	13889	15861	14839	15,703	15551	15899	14352	235
250		6-07 7264	\$368	\$563	3005	\$8.3	26.8	7946	8.00	9429	10245	11998	11966	12816	11819	14313	14900	15358	15691	35.5\$1	230
\$22		4008	33.3	32.99	\$008	\$183	7388	8018	8658	9341	10975	10.85.8	11676	12499	13288	14901	14600	15258	15168	15534	\$22
220		\$069 19.2	\$371	\$\$û\$	63.35 22.35	6906 18.8	13.89	8968	1654	9264	7166	10823	11375	12153	12916	13813	14308	14653	14236	15044	022
215		\$125	8585	\$80\$	17.4	11.8	1879	8124	8664	9209	9826	20901	11988	11794	12503	82881	13735	1,11,8	14,485	14440	<u> </u>
210		\$177 -12.3	\$3.8	5892	6533	7097	78.58	8186 2.5	8688	21.8	9680	19313	19805	11433	12023	12873	13186	13549	1:1:1	14724	210
205		-25.8	-1824	-1998	6635	7197	8:52	8258	8726	9165	-3397	19243	145.6	11871	11618	12238	12567	12859	12975	20881	502
200		5406 -34.5	-27.4	45.8	6773	7317	7845	4333	8766	9155	-1023	-13.89	10283	10701	11343	11352	11883	12083	12322	11298	200
125		-3936	-\$303	-\$\$\$8	24.85	2457	7949	7.58	8789	9128	826-	9119 F-161-	19916	10327	10438	10921	11339	11324	11176	19381	195
190		-35.58	-\$ 275	499	£\$\$2	7594	8933	8 4 30	8772 6-0	9089	9303	9519	977.5	8285	10101	10248	10313	19283	10346	9883	190
185		-28.3	-\$635	-11-6	2505	7687	8063	8398 10.0	86.87 78.83	8925	9118	9508	9385	£256	9516	9.04	10.0	9278	99.39	47.22	185
180		-17.6	41.06	6:82	7362	7688	4.6	10.1	4818	8705 6.9	3849	3.5	8983 3.0	1904	4873	8,08	10.6	\$185	7846	74847	180
f. 10NG	141	0	?	-10	-15	-20	->5	-30	-35	0+-	-45	-50	-55	04-	-65	-70	-75	04-	-#\$	06-	LAT E. 10NG

1. 10NG	240	3		•	5	,							
141													-
၁	5.87 5.87	1667	10.5	7.6-	5054 -100	3988	4175	-89.0	-8663	-928	5865	23862	_
₹	5037	5029	\$85 \$38	-10.9	4743	-\$2.3	1964-	2508	-8163	5040-	-2115	-3847	Ĩ
-10	5358	5311	\$279	5208	53.5	-5126	4958	-58.7	1689	149	-1549 -83.5	-3291	-1
-15	2085 2085	\$715 18.2	29.48	5555-	-53.4	5014	4406	3482	22.82	-81.1	-918 -78.4	-2452	\$ -
-20	6368	93.51	6153	-15.2	×846 -31.0	5497	-5816	-6943	-3868	-14:3	1.52.	-1834	17-
-25	1928	6818	8089	-9674	-26.63	-\$303	-\$833	-\$\$88	3543	-2133	1:59-	-1963	\$ ~-
01-	13.5	22.8	7413	24.05 20.05	15.31	-6.00 -300 -300 -300	4528	\$408	-55.0	2896 -5896	1326	-5139	- 30
-35	4953	4819	28 5 4 5 4 6 6 8 6	8 185	-4328	\$028-	-3878	\$0.28-	-1873	-3404	-3158	-45:3	*
-40	9575	4595	12.2	9385	2992	-40.6	-2863	3858-	\$908	4547	3025	1425	07-
-45	10533	19596	10568	6038.	8.601	9586	9871	7931	6772	5428	3929	2472	\$4-
-50	11498	13283	13559	11589	116.58	10508	9759 -2.8	8799	8-02-	-8314	-\$858	-3363	0 \$ -
-55	12414	12509	12477	12289	11919	11357	10593	9636	13.87	7215	5832	-23.5	-55
-40	13265	13343	13289	13278	12835	12309	11550	10415	9324	8108	-16.1	16.6	04-
-65	14019	15265	13974	15737	13330	12759	12023	11153	10109	8878	2002	-10.1	\$4-
0	14665	14809	14547	14084	13875	13318	12620	28711	108 39	9.193	8675	2403	07-
-75	15105	15171	15024	14550	14345	13812	14155	12382	11535	10538	90 70	396	- 75
-R0	15238	13861	15438	18307	147.8	14863	13848	61.621	15863	11383	36701	4 55	78~
2 K-	15989	15961	15815	15552	15174	14684	14884	13382	175 Rg	11695	10721	6994	\$ 4 -
06-	15285	16583	80751	1828	14363	15978	14589	13774	35056	12849	118.5	2059	(16-
(4)													14.1
DNO.	076	<i>y</i> ?	0.50	255	240	376	2.70	175	0.00	786	900	300	

E. LONG	300	\$0\$	110	315	07.	325	430	335	340	345	150	355	t. 10NG
0	-5930	-7354	-8511	-9330	5.3	-9785 21.0	-9432 35.4	3218-	6682-	-6418	5925	-4975	0
- 5	1.465	-6962	23169	-188:1	9.46-	-9389	5211	-8751	-7998	-7148	8-59-	-5436	S-
-10	-8358	184.3	-{\$\$}	-8530	606-	15.6	30.1	7758- 4758-	-7930	1:25-	£0,99-	1.18-	-10
-15	-4320 -61.8	-5805	-7219	-7905	-8432	-8624 15.0	-8521	-8193	-7713	-7152	62.8	-5941	-15
->0	-3596	-5078	-51.0	-1382	-7747	15.9	-7965	-7739	50.1	-6935	-6448	15927	-20
5	\$385°	9-04-	-5511	-6427	-7072	-7318	-7364	-7220	-6948	57.0	-8103	-5751	-25
-30	-1967	-3447	-4687	-5633	-4279	21.5	4.78	\$583-	-8553	-6171	-5834 58.8	-5472	- 30
-35	-1085	-2561	-3815	1029-	-5477	-5884 -25.5	47.9	6.045	-5911	-5699	-5444	-5366	-35
0 -	-3358	13812	-4878	-3884	-4619	-5085	-5328	\$583-	-\$363	-\$853	-\$269	-1803	04-
-45	-3033	-2801	11856	-2886	-366	-1808	-1343	£:27-	-\$3.7\$	-\$373	1:25-	47.40	-45
0 >-	-28.5	15.4	137	8671-	-2933	-3568	\$208	-4908	-4515	-4371	9:33	-4685	05-
-\$\$	-2888	1958	£24-	5.41	-1535	-2361	-2819	-3299	-3681	-4923	-4363	\$226-	-55
-40	4122	2833	1632-2.4	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	14.5	-1250	-1973	20\$ -	-3181	-3724	-4267	-4834	09-
-65	5246 -8.7	4008 -5-3	2823	1808	11.6	3251	-1142	-1954	-2723	-3470	-4216	-4980	-65
-70	6308 -3.6	5115	3936	2791	1687	11.0	14.8	-1379	-2326	-3566	1304	-5348	-70
-75	2.55 .5	6087	4406	3724	2549	1386	23.8	-847 0.07	9-85-	-3132	-4238	-5340	-75
0 .	8021 3.4	ဂိ ုန်စ္	5662	45.55	3195	1938	3.5	82 S T	-1848	tols-	-4344	-5570	0 u -
-85	#\$. \$	1504	6.137	4.96.4 2.64	1552	2216	864	265-	-1858	-3319	-4548	-5854	- 9 \$
06-	\$628	857,	4379	\$387	8258	12.12	-453	100=	-2082	-3486	8987-	-6198	06-
LA1 E. 10%6	100	305	310	315	320	325	330	335	440	345	051	355	LA1 k - 10NE

1 . LONG	C	•	U .	2	2	,	3			•			
141													LAI
0.	29401	1018-	25401	28401	16485	29401	29401	58401	28401	59401	25401	29401	36
8	54294	55518 -12.5	55356	55407	55471	55546	55632	55728	55813	55944	56060	50160	ž.
0 W	5.3989	54921	54,088	54190	54326	54696	54692	84918	55167	55437	55725	56018	8
75	52607	52631	52712	52825	53048	\$3299 6.5	53603	\$3956	54354	54.790	\$\$2\$\$	55750	75
20	51182	51192	51278	51442	51680	51992	52375	52828 12.0	53345	53921	\$4549 7.8	55217	02 .
65	49661	19668	49764	49944	50212	50562	50994	\$1507	\$2100	52770	5 15 06	54307	\$9
09	4 79 10	47956	4,6078	48267	48581	48956	49434	49955	50581	51292	52086	52953	94
4 \$	45845	45919	7.76	49349	8.55.	42083	47557	7018,	3.25,	16.9	\$9546	51121	\$\$
0.5	41878	43519	43658	43982	8.85	49913	6188,	43808	18864	417.8	41346	8228,)5
45	40096	40321	40650	41053 29.8	41507	41999	42528	43097	43713	44379	45095	42854 F - 3	\$ 7
07	\$6222	16527	36438	311.2	37933	38474	39039	39633	40257	40907	41574	42251	0,
35	\$15.70	31936	32410	32944	33503	34078	34675	35301	35952	16608	37246	37846	\$\$
40	8.85.	30402	26898	3386	29113	58882	28318	29880	39678	1363	2.818	32243	30
25	19783	\$7802	50868	51803	3388	25355	23855	23828	29804	7114	2\$803	1:802	\$2
20	12813	13138	13574	14055	14553	15095	15720	19455	17365	18067	12757	14259	90
15	5453	5661	5990	22.59	6793	12.1	7907	15.4	15.8	10389	11106	11592	2.
10	-1853	-1823	-1865	-1919	toti-	-903	11.58	\$7.54	1823	\$\$6\$	32.15	8668	0.
^	-8608 -54.9	-8816 -38.4	-8870 -23.8	-8807	-8613	-8243	14.8	20.05	-5977	-5121	13.1	-4112 35.8	~
0	-18303	-14832	-13148	1.981-	62821-	-14328	1.881-	-13618	8.72.	-11893	-11168	5:311-	<u> </u>
1 4 1													1 4 1
E . 10NG	=	٠	10	1.5	0.7	3,5	5	2	0.7	\$ 7	0.5	<i>y</i>	1

(units: nT)

VERTICAL COMPONENT (Z) WMM-90

	t. tone	Ç	\$\$	u/	\$	80	8.5	06	\$6	100	105	010	115	9N01 - 1
	141													LAI
	06	29401	28431	29402	28401	25401	28401	10455	28401	29401	29401	29401	73485	70
	ŝ	56502	56423	54543	5665	\$6669	56872	56967	\$2055	57127	57191	57243	572HS	«
- 1914 -	0 14	24520	56620	50.914	\$7196 -15.8	57459	57699	57910 -20-5	58089	SR232	58339	59407 -25.8	58437	3.6
	7.5	\$6255	56763	57262	57741	58186	58586	5 # 9 # 0 - 15 .4	59209	59415	59544	\$9595 -23.U	59564	22
111	0.0	55913	\$6 9 23	82\$78	5800 %	58635	\$5501	29685	85809	61319	29452	69858	82465	92
1834 1834	6 5	55150	\$6019	\$6890 7.8	57739	58534 4.8	59247	59847	80308	6.06.03	60.228	60661	9.8-	\$9
- 2562	09	5 18 79	54845	55825	56786	57694	58510	59 194 8 • 6	59711	60028	60121	59975	59588	04
6.9872 5.9813 5.8823	\$ \$	2.885	5 1958	54968	35458	54813	54878	57598	27185	2:645	66545	59565	£\$285	\$
4.9434 4.9424 4.9204 51835 51836	9.0	\$2867	50814	51582	\$2545	53868	54295	24390	\$\$\$n\$	8-245	5\$784	5 \$ \$ 2 8	5484°	0 \$
4-2934 4-3925 4-2219 4-2034	\$ \$	2.5	47493	48349	\$0264	\$ 0020	50863	51383	51835	52060	\$2029	51676	51006	\$\$
\$1903 39443 40410 40842 41204 41604 41605 4222 2722 4777 41134 \$7903 3256 3463 3463 34635 34635 34635 34636 34755 34816 3522 2772 34635 34636 34635 34636 34635 34635 34635 34635 34635 34636	0,	42934	43625	44320	45316	45673	62397	7.597	3-71-	7061,	4333	49879	46187	0,
2.42.3 3.42.4 3.42.4 3.42.5	3.5	38405	38932	39441	39936	40410	40842	41204	41460	41568	41477	41134	40495	35
26473 20403 27408 27235 27235 27235 27235 27235 27235 27235 27235 27235 27235 27235 27235 27235 27235 19426 <td< td=""><td>30</td><td>\$2991</td><td>33359</td><td>33678</td><td>33971</td><td>34244</td><td>34493</td><td>34704</td><td>34,85 0-55</td><td>34916</td><td>34835</td><td>34555</td><td>34010</td><td>30</td></td<>	30	\$2991	33359	33678	33971	34244	34493	34704	34,85 0-55	34916	34835	34555	34010	30
19625	52	22047	26907	27055	27153	27235	27307	27.875	23438	27469	30.8	27247	26849 38.0	\$2
13626 13635 13635 13635 13647 1991 13949 13149 <	20	19551	19666	19661	19593	19504	19422	19 \$70	19364	19398	19430	10380	19163	9 C
3803 3708 3413 2714 2814 2819 2179 4129 3214 3415 11.0 -4086 -4352 -4759 -5271 -5784 -6710 -6502 -6577 -6411 -6071 -5661 -11438 -11883 -12512 -13911 -14991 -14871 -14984 -14812 -14412 -13497 -15413 11.0 -11438 -11883 -12512 -13911 -14991 -14871 -14984 -14812 -14412 -13497 -15613 11.0	15	1,1828	13833	13998	13587	1354	11933	12888	1.181	18313	13958	123.8	11129	15
-4086 -4352 -4759 -5271 -5784 -6219 -6502 -6571 -6411 -6077 -5661 -6.5 -11438 -11883 -12512 -15527 -15911 -14491 -14871 -14984 -14812 -14412 -13997 -1413 -15540 -15910 -14491 -14491 -14984 -14812 -14412 -13999 -159.0 60 65 70 75 80 85 90 95 100 105 110	10	3808	3708	3533	1383	£1.53	2399	\$378	\$129	3234	8478	32.38	53.23	16
-11438 -11883 -12512 -15520 -15911 -14491 -14871 -14984 -14812 -14412 -15997 - 41.3 59.0 38.6 37.7 -15911 -14491 -14871 -14984 -14812 -1442 -15997 - 50.0 60 65 70 75 80 85 90 95 100 105 110	~	9407-	-4352	-4759	-5271	-5784	-6219	49.7	-6571 50.7	-6411 48.6	1.44	-5661	-5245	∽
60 65 70 75 80 85 40 95 100 105	0	-11438	-11883	-12512	-15220	-13911	-14491	14871-	-14984	-14812	-14412	-13897	-153462	÷
60 65 70 75 30 85 90 95 100 105	ואז													[•]
	1. 10NG	9	\$ 9	0.7	7.5	30	8.5	06	66	100	105	110	115	1 . 10NE

	29401	28401	 28401	28401 28401
	52323	53338	53344	33343 53344
	\$8007 -28.6	58129	\$8238 -29.8	58338 58238 -28.5 -29.8
5 57866	58183	58498 -26.2	58798 -26.6	59067 58798 -26.6 -26.6
	51808	58185	58745	
	26147	\$1875	51872	
	53778	54929	56780	57174 56780
	50584	51873	53378	54725 53378
	46703	48256	49864	
	42278	43904	45587	47229 45587
	37429	39028	40704	
	32241	33218	15883	36853 35883
	26769	28013	29384 22.8	30778 29384 26.7 22.8
	21948	21988	23975	24418 23077
	15996	15682	16839	17,570 16839
	8914	2136	9537	10949 9537
	2493	23.79	24.5	
	1176	=4568	=4383	-4879 -4383
•	-11072	-11659	-12088 -19.6	-12400 -12088 -13.9 -19.6
			,	
150	145	- 40	1.5	150

25104 27104 27104 27068 27068 27068 27068 27069 27068 27069 27068 27069 27068 27069 27068 27	256,04 256,05 256,03 256,05 257,03 256,05 257,	20	56401 56902 52400 57280 57380 51333 56915 55826 55826 55826 55826 55826 5778 63899	25 25 25 25 25 25 25 25 25 25 25 25 25 2	\$6401 \$6872 \$2335 \$2735 \$7739 \$1739 \$1739 \$1739	24 24 24 24 24 24 24 24 24 24 24 24 24 2	50 40 3 50 40 3 50 40 3 50 40 3 50 40 3 50 40 3 50 50 5 50 50 5 50 5 50 5 50 5 50 5	3
20, 20, 20, 20, 20, 20, 20, 20, 20, 20,		15	524.0 57.280 57.33 51.33 51.33 52.33 53.36 63.89 63.89 63.89 63.89 63.89 63.89 63.89 63.89 63.89 63.89 63.89 64.77 64.78	25	\$6872 -23.4 57355 -2715 -17.4 57808 -13.00	86.5 80.5 80.5 80.5 80.5 80.5 80.5 80.5 80	5250 2240 2340 2340 2340 2340 2340 2360 2360 2360 2360 2360 2360 2360 236	\$ 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
21 21 2 2 2 3 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2		15	577280 57333 56915 55827 55828 53828 5199 51199 61199	272 273 274 275 275 275 275 275 275 275 275 275 275	\$735 \$7739 -17.4 \$7808 -13.00	27, 28, 28, 28, 28, 28, 28, 28, 28, 28, 28	52405 54087 19.44 54085 5405 58625	80
01 N N 4 4 4 N N N N N N N N N N N N N N		54 4 5 5 5 5 4 5 5 5 5 5 5 5 5 5 5 5 5	57333 56915 57.9 55827 53828 53828 53828 5199 61199 61199 61199	25 25 25 25 25 25 25 25 25 25 25 25 25 2	57739 -17.4 57808 -13.0 57293	579.25 118.27 145.88 148.88 15.88 15.88 15.88 15.88 15.88	200 00 00 00 00 00 00 00 00 00 00 00 00	25 05 85
21		50 50 50 50 50 50 50 50 50 50 50 50 50 5	55.827 55.827 55.826 55.826 51.99 51.99 67.778	\$ 50 50 50 50 50 50 50 50 50 50 50 50 50	\$7808 -13.0 \$7293	5 5 5 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	58625 58625	70 65
20 44 44 25 20 20 20 20 20 20 20 20 20 20 20 20 20		55 50 50 50 50 50 50 50 50 50 50 50 50 5	55827 53226 51299 51299 47778	5 1 2 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4	\$7293	51888	58625	\$\$
40. V-4 - 000 V-		50 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	53226 51199 47778 43898	52453		\$ 6835	5:61-	
44 44 64 64 64 64 64 64 64 64 64 64 64 6		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	\$1199 \$7778 \$3898	52453	55868	-1/-	57843	09
3 90 30 8 7 8 9 2 8 9 2 8 9 2 8 9 2 8 9 2 8 9 2 8 9 2 8 9 2 8 9 8 9		4 6 6 2 3 4 5 6 6 2 5 6 5 5 6 6 5 5 6 6 5 5 6 6 5 6 6 5 6 6 6 5 6	43898		53706	54923	56871	\$\$
35.087 5.802 5.487		42503 38458 -527	43898	\$26-	59596	5198	53319	2.0
35987	,	38458		45}\$	£6833	48304	44738	57
		,	39805	41329	42675	44143	45596	0,
31331		34448	35669	36974	18332	32725	\$1813	35
22734	. • •	39828	33545	32695	33903	3\$363	36444	3.0
24162		26494	27,484	28328	16162	30476	31597	52
29417		24350	23966	23857	1:03-	25508	26543	20
16591	•	17903	18473	19106	19788	20504	21252	15
11615	•	13847	13823	14943	12893	13161	15755	10
6313		3.82	to59-	8675	9159	9644	10144	•
416	•	-58.63	2504	30.73	3575 -35.2	1.74.	18:3	0
•		,	;	9	2	č	*	141

\$6401
-21.4
256.36 564.0 266.36 564.0 266.36 564.0
4
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
1
56.64 25.69 27.00 57.00 58.50 5.50 5.50 5.50 5.50 5.50 5.50
245 345 272 368 272 368
-21.4 56602 -21.2
-2154 5 <u>6</u> 669
-21.4
•
56401

E. LONG	360	303	210	315	07.	325	130	335	440	345	150	\$ \$ \$	1. 1046
171													141
06	29401	25401	25401	19482	29401	28401	28471	10\$65	19492	28401	10185	50401	06
8 S	25879	\$\$788 -16.2	55702	55621	555.8	234 .3	55418	25367	5532F	55300	\$\$58.	55263	88
0 .	55775	53555	25418	5.8087	9.8-	54671	54491	54354	54203	10175	8.65.5	5.595.5	80
25	5 < 977	55558 -12.6	\$\$137 -16.5	54724	54331	53963	5 7 6 2 8 - 1 - 8	53133	53083	52882	52,35	52642	٤.
20	56242	55610	54977	54358	801-5	53218	82.125	52285	51916	51618 8.3	51395	51250	02.
65	2:265	\$385	5\$\$75	53244	53862	52243	51599	8,615	\$0.5ns	50501	49925	8728,	6 \$
09	55813	54744	53683	52661	53708	50843	28805	49432	48899	48 88 88 88	48188	44005	09
\$\$	54659	53393	52142	50952 -38.6	49856	4.88.Z	49933	62823	46756	46330	44041	45882	\$\$
20	52732	51297	49879	48545	47332	46268	45363	44623	44044	43626	43363	43249	\$6
\$	28953	7.62-	46909	45450	44138	53803	£3825	41887	49303	26207	40002	} 0807	4.5
07	1.16708	1.96-	43318	41739	46327	3202	38106	33308	\$55.01	36294	36083	36564	07
3.5	42831	-118.2	-1982	1752 -100.0	35988	34663	33561	32682	32821	31581	31363	31366	3.5
10	58557 -178.6	\$6684 -130.5	34770	32923	-38526	29734	28471 -82.3	3.69-	26863	26143	25878	25868 -18.U	30
\$\$	-12818	-35288	-32968	-18855	-38358	-41823	2,881-	21669 -88.	29698	28823	19665	185.6	\$ 2
32	-12883	-15839	-13512	-23924	20869	18843	17928	15485	14259	13383	12862	14892	02
15	24455	-162.2	20246	17914	15497	13155	-11801	-18133	3.871-	\$ \$ 00 B	5703	5466	15
10	-12574	-162.2	-170.3	15917	-18373	-16356	-150.8	2929	-170-7	-1012	-1113	-1654	10
~	-15892	-18873	-18963	-17359	-178.1	-167.1	-153.2	-14368	-15759	-110.1	5:42=	29378	⋄
0	1.551-	3041	\$759 -159.3	315:	353	-2482	-5101	-76.56	-9251	-11409	-18710	-13673	C
LA1 E. LONG	00 _k	305	310	315	320	32\$	130	\$15	340	345	350	355	1 1 1006

9N01 .	c	∽	<u>.</u>	15	90	\$ 2	30	.5	0 7	\$\$	٦٥	\$\$	1 . LON
7													•
0	-14363	-12832	-13248	11811-	62821-	-14828	27861-	318£1-	-18868	-11803	-114:8	-11379	
~	-14823	-19553	2009-	-20415	-20494	-20265	-19769 -19769	-18675	-1835	52271-	-17402	-17455	•
-10	-21915	-32827 -29.6	-21534	-23989	8:862-	-73989	-21841	-22977	-22410	-22043	-22019	-22398 38.9	7
-15	8.75-	-24538	\$ 0 \$.2-	-28903	-26,186	-76069	-25727	7-5305	-24979	-24933	-25282	1:882-	-15
-20	-24603	-25\$25	8:13-	2.682-	-26829	-76738	-26503	-28281	-26361	-26593	-22368	-28574	~
-23	24755	-25506	->6463	66282-	-28493	-26430	98 685-	-26356	-26670	\$082-	-2860\$	-39241	~
- 10	-24875	2.682-	full 2-	7:862-	-25679	52882-	-25253	\$946	10282-	-28813	-29403	-33813	ī
-45	-24032	-24392	-24634	-28774	-24869	-24288	-25261	-28,939	7.862-	-28234	-39125	-32410	Ī
0.	-23669	-23909 -23909	-36483	78549	-24818	61862-	£\$\$\$2-	-28945	-27273	-78939	-33926	-33479	7
\$	4,401-	-23843	-24918	1265-	-24593	-25076	-25874 59.68	-26847	-28269	-30063	-32235	-3473	7
-40	-24216 118.5	-34429	-34690	-25036	-25513	-26174	-27876	60382-	-28383	-31824	-33784	-34212	*
\$ \$	-25599	-25848	12885-	-2485	12822-	-28033	-29913	-30575	-31803	-33803	-35863	6768-	٢,
-60	-{790\$	-18182	-26823	-48864	22882-	-30558	-31586	-32828	28888-	19884-	1878-	-38818	1
-45	-31115	-19807	-31,785	-12301	-32958	1.968-	-34228	-35869	-35383	1288-	-46324	-48125	Ý
04-	-35008	85881-	-38723	\$6184-	-36388	80888-	-38355	- 30439	-49858	8:31,-	-43863	-49843	- 1
-75	-19642	-19864	-40172	-40570	-41061	7,88,-	-42330 -42330	-43109	-45961	-44942	-45987	-47106	- 7
04-	7-00	3.00	-44801	-43398	1:85-	-45971	-46455 FB.5	46.00	-47392	-48345	\$ 5 000 y -	1.387-	,
٠. د	-48423	-49516	-49643 89.9	10867-	-49995 P9.95	-59217	-50469 #8.9	-50748	-51855	-51383	-51133	tot8s-	4.
06-	40045-	-54894	-54094	-54094	-54094	-54094	-54894	8648-	-54094 88.9	-54094 88.9	-54094 88 - 9	-54094	0
7.													4,
3804	•	J	•	*			2	31			5	2	-

191													
													141
0	-11448	-11885	-12512	4555	-11911	16561	14871-	-14984	-14813	21881-	13807	-13192	O
?	-17875	-18585	-10476	-24439	-23353	-25039	52822-	P.612-	-22772	-7237R	-21824	-21243	? -
-10	-2*153	3.142-	2.88.7-	-26674	-27884	-28925	-296 #8	-3008-	-30114	-29613	-29 303	28419	- 10
-15	-27206	-28629	-3940\$	15815-	-33368	-18718	1.282	-39548	-34698	-34308	-16188	-456 78	-15
-20	-50147	-13979	-33926	-35903	\$321E-	-39588	-49872	-41855	-42400	-42538	-42365	-44801	02-
->5	-33858	12422-	-3886	-38858	2:815-	8.527-	9:65-	-49338	6:835-	-5383	8:51-	2:821-	->>
04-	-51139	-36365	-38878	-43568	-438ª1	p.532-	2086-	4.88-	-53859	-51853	6185-	-52399 -6-8	0.4
-15	- 54986	-37739	-40566	-43376	-489ng	8288-	-50882	-52794	-54300	-55384 -8-3	-56073	-56426	- 15
0 - 0	-36178	-38948	8-617-	41019	8-62-	-50438	-5387	-55203	-54756	-58114	8.005-	80665-	0 % -
45	-57447	-44325	-43278	9555-	-49113	-51857	-54394	-26658	-58893	19809-	-61368	\$1229-	-45
-50	-38852	-41639	-44505	-47387	825us-	-52943	-54898	-57813	-59843	-61361	-62936	-63969	- \$0
-55	2.6	-43824	-45713	1:467-	-5333	-53729	-56199	-58478	-60521	-62289	-63759	-64919	-55
-40	8-127-	80889-	7-70-	-49391	-51844	-54239	8-21-	-58670	-60621	-62349	22860-	-65843	09-
-65	8:85,-	-48873	46348	-59392	-58828	1:835-	->6333	-58438	60809-	\$2869-	8-159-	2.430-	54-
0	5:18,-	8;27,-	4853	-53162	-52823	-55833	20285-	\$255-	8.18	1.204-	-61873	15679-	-70
-75	-4 2 2 8 8	48823	£6265-	-54984	1386s-	-55869	-55925 67.6	-57156	-58286	-59360	\$: \$8	1:580-	- 7 \$
0 % -	-58473	-53283	-52115	-52959	-51808	-54651	-55479 76.£	-56284 75.6	-57056	-57788	-> 99.78	-58104	04-
\$	-52485 P6.7	9.845-	-53485 85.8	-53695	-54107 P4.9	-54516	P588-	-58813	2888-	->6463	-56419	-56735 82.5	2 R-
06-	-54094 9.84	-54094 88-7	-54094 489	988.9	40045-	-54094 988	-54094 F8.9	-54094	-54094 9-8#	-54094 8A.9	46045 88.9	-54094	06-
111													141
1. 10NG	09	\$ 9	٤	\$ 2	S	8	0.6	٥٠	100	105	110	115	1 . 1 ON 6

WMM-90	
ONENT (Z)	
ERTICAL (

20 04 00 40 00 00 00 00 00 00 00 00 00 00	f. LONG	170	175	159	145	140	145	150	155	160	165	176	175	1. 1004
	141													[4]
	0	-12869	69871-	-13400	-12088 -19.6	-11659	-11072	-10311	1716-	-9246	\$0.8	-5524 40.0	-\$955	٥
	?	4.1-	-20272	-19855	-19397	-18826	-18118	17358	-16229	-15035	-14881	-12207	-10692	\$-
	-10	-24149	-2763p	0.21.2-	-29587	-25849	-2813	-24862	-23200	-21978	-20605	-19115	-17576	-10
	-15	25336	80871-	-34074	-13496 -7-0	-32829	-32041	31115	\$56bx-	-24819	-77446 -8-6	-> 545}	30372-	\$1-
1221	06-	-41549	-41062	-40546	-39973	-30308	-38521	16878-	-30826	-34408	-34849	-32463	-30918	-20
	-25	-47281	-46884	-46419	9285	72857-	3,8,,-	1.823-	-42459 -1-1-8	-41346	8086x-	-38438	-36907	->\$
	01-	82825-	80825-	-51918	tills-	->9588	49318	-49803	2,217	8-894-	-45513	-43283	\$2\\$27-	01 -
1940 1971	2¥-	-56513	-56393		¥\$855-	85645-	-54308	-53403	-52352	\$08ts-	82367-	4284-	8268-	- 15
11	0*-	6050-	-40048		-59506	-58854	-58231	1575-	54323	23168-	4:28:4	-52878	-53188	0 7 -
	S 9 -	-62732 -2.6	7.8-		-62648	-62179	-61503	-60669	-59692	-58596 25.8	-57407	-56149	-54844	-45
1986 1987 1987 1988	0 >-	9.6-9-9-	-65063	-65323	8-85-	-64671	-64102	-63361	-62476	-61476	-60388	-59238	1:88-	05-
\$185. \$185.	-55	99259-	-66320	-66591	-66604	-66385	29659-	-65366	-64625	-63771	-62830	-61876 38.2	-60782	- 5 \$
\$285- \$285-	09-	-65975	10600-	88629-	0.87v-	1829-	-64383	12660-	15660-	-63373	-64829	-63803	-02335	09-
\$\frac{1}{2}\frac{1}{2	-65	97860-	-69893	7.854-	19869-	8,850-	-67963	-6987]	-66546	90750-	-65547	-64968	8.579-	-65
-5962 - 65623 - 65624 - 65624 - 65625	04-	82619-	8768v-	62850-	4.98.6	£2689-	95869-	2-130-	8-689-	4.839-	16839-	80189-	82659-	- 70
9942 - 5448 - 5484 - 5484 - 54848 - 54848 - 54848 - 54848 - 54824 - 54848 - 54848 - 54848 - 54848 - 54848 - 54848 - 54848 - 54824 - 54	-75	* *8}*-	-62698	6359-	-63712	25059-	-64883	-64418	-68449	-64392	1-64251	-64032 62.7	-63739	- 75
-54943 -58309 -58304 -58304 -58304 -58304 -58304 -58304 -58304 -58304 -58304 -58004 -5	0 .	-53973	-44883	869-	-61304	-61818	1966-	81249-	-61218	-61853	\$2869-	-61133	besto-	0 4 -
->4p4 ->4p94 ->4	2 H -	£645-	-58309	-5735}	-57767	-57949 R2-1	5.000 5.000 5.000	-5£316	-58395	-54348	-58355	-58335	22885-	- A S
120 125 130 115 140 145 150 155 160 165 170 175 E. E	0.6-	->4ps4	-54894	-54094 48.94	40045-	-54874	\$ 688 5 - 280 5 - 280	\$ 855-	-54004	-54094	-54094 8 P. 9	14004 88.4	-54094 9.94	06-
120 125 150 185 140 145 150 155 160 165 170	141													1 4 1
	f. 10NG	170	125	150	135	140	145	150	155	160	165	170	175	1 . 10N6

- 14600 - 1	1. 1046	180	185	149	195	700	205	210	11	u22	577	082	215	1 . 10MC
4813 1824 <th< td=""><td>141</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>141</td></th<>	141													141
1421 1222 1422 1222	0	-2644	-1400	8.21	619-	-38.8	-1567	- 89.7	\$308-	-3873	-\$273	424-	10.7	c
	~	25.55	-7925 -7925	10.0	-5916	25965=	11812	2.6.4-	\$555	-2648	-3859	-14R2	-035 28.2	₹.
1.00 1.00	-10	-16078	-14699	9.0	-12669	-11545	-10717	-0925	-9141	-8365	-7616	2.22	-6740	-10
1987 1987 1988	-15	27422-	-21429	10202-	-16924	-17851	-16849	-15679	-14021	-13975	-13958	-12189	-13869	-15
1947 1948 1948 1948 1949	-20	69567-	4.4 4.4	75492-	1:8152-	-21903	25252-	-21616	20862-	-19414	-18348	17355	-16354	-20
-4913 -4113 - 4113 - 4114 - 41	->>	8** 8**	- 15810	1:83:	2:86:-	22881	tof 62-	-23865	-23853	-24859	-23448	5:432-	82882-	-75
-4113 -4114	01-	5: 91	19199	-37892	-36236	-34841	-33502 32.8	-32305	13688-	-29684	-29438	86182-	75882-	-30
-44[4] -4	-35	45854-	-44823	-43838	43983	26886-	-39366	-35841	13868-	-39488	13808	-33895	\$*\$6 _k -	\$ k -
- 5413 - 5417 - 5423 - 6427 - 6494 -	04-	folt.	82867-	60287-	\$: { {}	80840-	-42854	-43872	-49314	-39840	62828-	2.895-	708-6-	04-
-2215 -5614 -5614 -5414 -5414 -5414 -5416 -5664 -6647 -6617 -5616 -5618	-45	-5 1813	2:85-	-59851	-49549	9.28-	-4833	1085	44504	-43208	41269	££ 20 >-	10068-	\$ 7 -
-62015 -62016 -62016 -53114 -53114 -53114 -54114 -5	05-	-56836	-55629	-54613	-53216	-52835	-20863	f 4604	52,987-	80827-	-45852	-44389	-42801	-\$0
-62912 -62102 -62813 -52818 -52824 -52825 -54829 -53245 -54828 -54829 -54824 -54829 -5	-55	-59715	-58636	13888-	1268-	-53543	-5488	b:11:5-	7.5	\$0105-	-49353	-478R2	-46284 4.8.4	-55
-64993 -64803 -64813 -64813 -64814 -54829 -54849 -54814 -54818 -5	-40	8689-	20279-	9:830-	-59188	\$6125-	-52864	-56985	-54941	-53714	-543ng	-59853	3038-	-60
-64903 -64603 -64813 -64814 -69548 -59599 -58901 -54914 -54139 -5	- 45	-61577	-62411	\$0879-	4:119-	1.580-	-58355	-54329	23558-	\$6085-	-54845	-53508	-52079	-65
-61372 -625.5 -625.5 -61912 -61919 -696.5 -591.2 -591.6 -583.5 -561.8 -5	0	-64893	-63597	-65843	-63134	12880-	8,569-	-59659	-58699	1:655-	8588°-	-55398	-52158	-20
-61372 -61372 -61373 -69367 -59541 -58935 -58581 -54599 -57263 -56604 -55916 -58189 -58269 -57316 -57294 -57294 -57294 -56750 -56445 -59122 -55782 -55405 -58494 -54094 -5	-75	3:830-	9.99	-62465	-61917	-67310	-69645	-59921	-58348	-58303	1:225-	8:96 -	-5\$488	- 23
-58189 -58267 -58218 -58257 -57294 -57294 -56750 -56445 -56122 -55782 -55427 -56445 -56124 -56127 -55427 -55427 -554294 -54094 -	0 .	-61372 0.07	-6310A	16269-	8786y-	£1869-	-59541	-58938	-58581	86885-	-57263	-56604 85.5	-55916 86.5	0 % -
-54094 -5	S #-	-58189 P4.3	-58069	-57818	833	12818-	26885-	-57934	-56750	-56445 98.0	-56123	-55782 88.9	-55427	-85
14G 18S 190 19S 20N 20S 21S 270 22S 230 2*S t. t	06-	\$6055-	-54094	-54U94 88.9	-54094 88.0	-54094 88.9	988.9	-54094 A3.9	154094 88.0	-54094 #8.9	-54094 88-9	\$.845-	-54044	06-
14G 18S 190 19S 200 20S 210 21S 220 22S 230 2*S t.t	141													[]
	1. 1046	180	185	190	195	700	502	210	215	072	522	230	547	1 . 10NG

9801 -1	740	545	υς. <i>?</i>	\$\$?	760	597	270	175	780	285	79 U	\$67	4 . 10Nb
													1 4 1
	\$6.5	3.18	93.3	6.82	\$8.3	\$028	18913	13438	12323	12685	13158	-13883	0
	53.0	1.31	1853	1978	3862	53.8	2168	\$5.58	7360	1:83-	18.83	188-	\$ -
	-2584	9.48	8084-	-4173	-8099	81.8	5859	36.7	7233	\$685-	-2973	-\$113	-10
	20851-	0068-	-850	-8005	-6923	-5779	14488	-3415	-2350	-1733	1873	-1848	-15
	-15426	-14518	-13563	-12534	-11595	-10149		8885-	9.56	1285-	-\$878	-5534	-20
	-28139	-19869	-17859	-19787	15851-	1,5362	-12564	-1344	-19175	1.56-	-8207	7.88-	-25
-30	8:23-	-23458	25852-	-29893	-19346	42839	-162#3	-14779	-13626	-12340	11828	-11368	0
	-24945	-27698	-26173	-24584	1:832-	-21828	-18813	29.651-	-19385	15861	-14293	-11840	- 35
	-53365	-1234	-30014	-28215	9: \$8 2-	-24878	-22815	-20847	-19251	-17913	-16910	20591-	04-
-45	-37348	-35579	5.22. -	8.28x-	-29744	-27732	-25768	-23915	-22243	-20823	-19715	-19861	-45
	-4 1983	3:88:-	33888-	-35458	-33383	1218-	-28823	-28845	-23549	-28985	-22808	-22632	-50
-55	-44557	4.25	5.26,-	\$028x-	38838	£1286-	-32,64	-19933	-29265	\$0\$\$2-	-265R9	-2\$831	->\$
	1;11,-	2883	-4\$155	4-999-	-40863	-34583	-38969	15681-	12888-	418673	£986x-	25162-	-60
	-56563	-48973	-47376	-45645	4.4958	-42593	-4 p6 79	1:18:-	-34323	22385-	-35276	94278	-65
	-52852	20865-	2:265-	48707	6637-	9028-	858#v-	8.88	-42033	-40899	-38863	-38835	-70
	-5445	-53393	-58312	-51820	-56328	9008	-47993	-46973	-45998	-45048	44228	45434	-75
	-55504	-54475	-53743	-52985	8.085-	-53495	-58769	85085-	8218>-	4:18	2.68.	-47513	-R0
	-55061	-54684 90.1	-54305	-53920	-53535	-53155	-58775	-52405	-52047	-51703	-51171	-51060	S & -
	\$6855-	-54094	-54894	-54394 88.9	-54094	-54094 88.9	-54094 P8=9	-54094	-54094 88.9	-54094 8A.0	-54094 9.88	- 58095	() 0 -
1 7 1													1 4 1
OMG	74.0	745	750	255	260	765	7,0	176	080	285	29.0	500	9401

E. 1046	200	₹ 0₹	-	313	0.7.	` `		`			•		
141													1 A 1
c	125.1	8041	159.1	3153	169.0	-2482	1-5191	-11834	-18833	-11509	8:79:	-11673	3
٠	5301	3547	-11569	-1385%	-1381	-19338		-11523	-13592	-15328	-16759	806/1-	~
-10	-3818	11579	-13178	-12879	-7233	-9824	13839	-15424	34846	-16099	-18854	-2882	-10
-15	-2842 -32.9	-4219	-5985	-12929	19803	=12504	-15529	18103	-13500	-19892	-21526	-22614	-15
-20	-6503	£\$\$\$=	800	18297	=18989	-18333	-16547	1.00-	-19559	-21803	-22325	-25528	-20
->>	1.88.7	1.00-	-11109	-188.9	-14312	-15959	-17858	-186.5	-29518	62682-	-25819	-23846	-25
-40	-11861	-12199	1399	-16131	-15808	-13829	-12842	13960	-23919	2562-	-22878	68782-	01-
-35	-13829	-14233	-14972 -39.8	-15981	-1793	-18303	-13453	2°\$0 ->0 20 20 20 20	-21448	-72266	-25967	-23555	-45
-40	16090	-19379	2882	-17524	-18414	-19356	-20271	-21106	-21833	-25445	-22948	-23352	0 7 -
-45	-14573	-18533	-18788	-1926#	-1988	-29268	-23534	1843	-23365	56882-	7,842-	7:495-	-45
-50	-21479	-21225 28.8	-23229	-71631	-21879	-23174	-22589	-22975 58.2	-23309	-23588	100.8	-24922	- 50
-55	2.6832-	8:632-	-24259	-24501	9,5,7-	-24408	-24584	19262-	-24936	-25093	-\$524	-{}40}	-55
-40	79687-	-28361	27975	-27655	1-65	-27405	-27377 89.8	88222-	-28823	1572-	\$1575-	-107708	09-
-65	1:34:1	85281-	-32173	1:91:	butte-	13415	-39878	- 10854 - 18454	\$918s-	-48743	-38918	-38428	5 V -
-70	-38118	86188-	-34789	-16274	-35847	-35502	-35232	-35035	-34800	-16836	-34948	-36228	- 70
-75	-42710 RB-1	-45064	4149	06604-	8,56,-	P028-	-38813	18688	-38839	- 39452	4.06	-39562	-75
0 4-	4.697-	-46467 -4665	-48834	43438	86857-	6689-	-44758 89.7	-44577	9-64-6-	-44379	4333	-44399	0 .
-85	8418c-	2018-	-58453	-50936	-40844	-49681	0-10	-49446 90.09	-49375 90.8	-49337	-48332	7988-	- R S
00-	-54094	-54094	-54894	46045-	-54094	88.94	90 8 K-	\$6885-	\$08¥5-	-54894	40045-	-54094 8R.9	00-
141													1 4 1
F. LONG	100	707	,										

													IAI
	-13.6	-1174	-13.0	2874	-13.6	-33.8	-13.6	4715-	-13.6	-13.6	-11.6	4114	06
£ '	4636	4652	-17.3	4632	1363	-1544	-18.1	4349	4287	4179	-18:4	1861	€
04	-47.7	-18.3	6932 -18.8	-19.	-19.8	-20-2	-20-6	6555-	6393	6202	5981	5731	90
	1948	6993	-1903	8997 -18.0	8957 -18.6	-19.3	-19.84	-3645	-9177	-21.8	-22.1	1742	2.2
70	10927	10970	19389	19262	1,953	10900	19820	19709	10565	19382	10156	9863	7.0
1 59	\$585	12983	12999	12980	13858	14918	12869	14794	14698	12573	13811	14308	\$ 9
1 09	15133	15131	15116	15092	1:063	15032	14009	14963	14919	14861	14783	14677	09
\$\$ 1	1748	17462	12424	12381	17349	17307	17,884	17271	17871	17275 6.8-	17280	17379	\$\$
? 0s	2,0002	10972	19922	19869	19821	19883	19951	19779	608-1	19948	1991	\$18ñ2	\$ 0
S	22643	22619	22580	22536	75.452	8.9.2	22462	82872	22815	22591	22710	22875	\$
7 09	25313	25329	25,822	12852	41.452	818-2	25329	25152	25401	25488	25835	25843	0 7
35 2	27906	27986	28049	28106	28160	28211	28255	28298	24352	28441	28592	28827	\$
30	\$5365	12623	39579	39707	30836	10948	31939	31108	31374	31369	31923	31868	30
25	33148	80.658	3 \$ 8 4 8	32828	33988	33863	33.403	20868	33598	13708	33872	3,13,8	\$2
20	35.108	3 \$ 9 6 }	24903	34828	34608	34859	35944	45196	35328	35878	3385	31883	9.0
15 3	33498	33943	34377	34789	35137	35438	35685	35894	36893	24313	348.9	36973 -1842	15
10	32583	33093	33601	44973	344.98	34849	32348	3510	35703	36030	36429-18-0	36917	10
∽	50599	31158	31660	32928	32428	33011	33368	33726	34119	34578	35125	35763	ş
0	-23.25	28247	28748	P. 552-	29671	30080	30488	39934	31453	32068	32788	33601	0
141													1 4 1
f. 10NG	0	\$	ů.	15	90	\$2	30	35	0 \$	\$	0.5	\$\$	9 10 1 . 1

112

	06 8215 825-		ŕ	•	•					14	10	10 10 10 10 10 10 10 10 10 10 10 10 10 1								
																		· · · · · · · · · · · · · · · · · · ·		
								,												-42225 -42246 -42262 -42222 -4
					·	,	•		•	,										40 MU 00 MA MU 40 MU MU MU MU MU MU MU A0 MU
·					•	•	•	•									•			1
27.52	2798	•	-3768	5285		-3.5	19192	19192	121.5 121.5 13.5 13.5 13.5 14.5 15.5 15.5 15.5 15.5 15.5 15.5 15	20 1 1 1 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2	7, 01 th th 02 41 42 42 42 42 42 42 42 42 42 42 42 42 42	2, 24, 24, 24, 27, 27, 27, 27, 27, 27, 27, 27, 27, 27	2	7. 51 11 51 01 5 5 11 11 11 11 11 11 11 11 11 11 11 1	1	2	1	1	1	1
-\$174		2996-11-9	-53.6	5725	4 6	-24.8	10563	10000 1000 1000 1000 1000 1000 1000 10	1000	200 000 000 000 000 000 000 000 000 000	20	25 20 21 22 22 25 25 25 25 25 25 25 25 25 25 25	21 22 21 22 22 22 22 22 22 22 22 22 22 2	21 21 21 22 22 22 22 22 22 22 22 22 22 2	21	21 22 22 22 22 22 22 22 22 22 22 22 22 2	20	20	20	25 25 25 25 25 25 25 25 25 25 25 25 25 2
¥215-	•	-3193	-22-1	6172	8138		10948	1000 1000 1000 1000 1000 1000 1000 100	14 20 0 4 5 1 1 20 0 4 5 1 1 1 20 0 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	84 NG 85 NG	00 00 00 00 00 00 00 00 00 00 00 00 00	11 100 01 11 100 01 11 100 01 11 100 01 11 1	11 12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20 00 00 00 00 00 00 00 00 00 00 00 00 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00 00 00 00 00 00 00 00 00 00 00 00 00	\$ 500 MG NA NO OF OF ON 1:0 40 NA 500 OK \$ 4: 0: 5: N: 0: 6: 4: 4: A: 6: 4: N: \$ 500 MG GG AA NF FO 46 4: 0F OF MK 46 \$ 500 MF NI NI NI MI	\$ \$4 \times \$6 \	1 804 VG NA NA DE 6F ON 110 40 NA 58 08 NY MY 1 41 01 61 71 01 61 41 91 M1 61 41 N1 M1 M1 2 60 04 08 44 M1 M1 M1 M1 M1 M1 M1 M1 M1 M1 2 61 F1 F1 N N N N M1 M1 M1 M1 M1 M1 M1
-33.3		1379	4824 -22.1	-24.0	8781 -22.8		11828	14358	14528 14348 12328	11828 14148 12323 12334	1434 1434 1237 2033 2237 2237 2337 2337 2337 2337	143.68 143.68 123.73 20.53.6 20.53.6 20.53.6 20.53.6 20.53.6	11414 14144 12174 20334 20334 20822 20822 20822 20822 20822	11414 14144 12174 2033 21377 2082 2032 2034 2034 2034 2034 2034 2034 203	20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	14446 17474 17474 20534	20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	20 24 24 25 26 27 27 27 27 27 27 27 27 27 27 27 27 27	20 24 24 25 25 25 25 25 25 25 25 25 25 25 25 25	20 24 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
-1378		3560	5349	-{4:}	-2398		148.9	14363	145.5 175.5 175.3 175.3 175.3	128.5 178.5 178.3 208.2 208.2	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20	20	20	20	20	10
2174	-13.6	-133	-22.0	7388	-2363	11958	-16.9	14534	14559	2 17 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2007 2007 2007 2007 2007 2007 2007 2007	14559 17505	2007 2007 2007 2007 2007 2007 2007 2007	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	20 5 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	20	12	2	1 11 1 2 2 2 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1 11 1 2 2 2 3 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5

-19.6 - 13.6 - 1	9 10 1 . 3	120	125	130	135	140	145	150	155	160	165	170	175	1. 1086
11.5	LA1													LAI
1811	04	-31%	-1376	-\$376	-{17.5	-43.2	-43.6	-2174	-4478	-4378	-4378	-41%	-1174	06
\$318,	Š	-1848	-1369	-12.3	1199	1559	-1303	-1526	1557	1583	-1603	-1612	-1803	8 × 5
\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$. \$\$\$\$\$\$	0	-7873	-4853	3982-	3334	1592	3840	4966	4267	4422	4542	-1618	-1852	0
\$\$\$\$\$ 1355	2	4838	5241-	5696	-9153	6593	4999	7357	-1858	7895	8067	8170 -21.5	8205	7.5
\$\$\$\$\$ 1360\$ \$\$\$\$\$ \$\$\$\$\$ \$\$\$\$\$ \$\$\$\$\$ \$\$\$\$\$ \$\$\$\$\$ \$\$\$\$	70	-286}	-8327	-8826	-2523	-3383	19589	15828	11274	13544	13528	11827	1387	٥،
\$\$\frac{1}{2}\$\fra	\$	19865	13802	1387	12933	13538	14969	1551	14856	15104	15258	13328	13309	88
\$\frac{2}{2}\frac{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac{2}{2}\frac	90	15569	15209	15868	19851	13863	13343	12818	19183	18369	198.5	18443	18374	9
\$888 \$2885	\$\$	18297	18860	19427	13853	29403	\$5282	29393	21138	21373	218.5	21952	20912	\$\$
2413 2613	\$0	23828	22418	25829	23184	23453	23617	23674	23653	23514	7.52.5	23123	22893	\$0
\$\frac{1}{2} \frac{1}{2} \frac	\$\$	45547	25785	25993	24333	24978	12802	25863	5218	8:452	\$2052	24722	24383	45
\$415	07	ZR869	28900	2889 28.9	28285	88572	28291	27907	27457	26967	26463	25973	25518	7 0
\$\frac{1}{1}\$ \$\frac{1}{1}\$<	£	5.16.89 9.89	8:31.	31565	31128	3000	30178	12862	28836	24279	tibiz	2872	20405	3.5
\$\frac{2}{10}\$\fra	10	1:375	3416}	33318	33168	32526	20618	82928	4505	28159	\$0\$\$5	29008	28385	0,
\$452 3720 3745 4551 3512 35405 35405 3525 35605 30405 3110 31245 35405 3	\$	\$671\$	\$6893	18888	34878	34888	33828	32340	31453	39599	13282	\$5855	\$9405	\$
39462 38822 38936 15.6 16.5 3693 34931 35.24 20.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5 1	20	38378	37,268	34454	14353	35378	34458	33828	12617	31838	39858	392 58	80482	0 ~
\$9974 \$9568 \$8872 \$1215 \$7215 \$9313 35532 34797 \$14.6 \$9514 \$59014 \$10.6	15	39462 10-6	38822	38086	17268	36392	35493	34601	33742	32949	32228	31565	39984	15
39916 14.5 38413 38179 37508 3685 36234 35609 36509 36	10	39974	39368	34673	3,23,	3:118	36313	35532	34797	34128	33208	32951	1343	10
39292 38918 38474 37992 37592 37826 39383 49185 3	\$	39914	14.03	38818	62145	37508	36855	36234	35669	35338	8-6-1	£1.5×6	35827	•
131 U30 571 U71 511 U21 561 U11	0	39292	38918	38474	1.6618	37493	37828	34848	\$914.	35824	\$\$\$08	1:163	2 4 5 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5	C
110 U10 170 U10 110 U10 U10 U10	141				,	,	,				,			1 4 1
	E. 1046	1.20	125	- 30 -	115	140	145	150	155	160	165	1 70	17.5	9 NO 1 . 1

141													
0.	-1176	-1176	-13.6	-{};;	-33.8	-1176	-33%	-1176	-4478	4178	-\$172	-1174	76
£	1591	1558	1508	-1643	-1325	-1478	-1179	1105	962	-13.3	815	4°61-	\$ a.
90	46.3	-1279	-1278	-1226	4134	3901	1628	3318	12.51	2597	-1153	1808	360
2	-2321	-\$2.2	-2505	-2469	-3473	-8818	6000	-9127	\$968-	5029	4412	1257	2,2
70	11878	13838	13818	13313	18131	1928	-3369	-3163	-9823	1869	4845	1551-	0.2
65	15508	13938	142 Rg	14449	14039	13547	12272	12314	11873	19768	- 1889	3988	6.5
09	1381	18046	46511	17568	1787	14906	16953	13218	14893	11988	13013	17071	09
\$\$	\$207	\$2\$02	20283	9-8-1	8-6-61	19273	11800	18265	17639	16031	16146	15293	\$\$
50	8.827	\$2420	22188	21052	80212	21416	21083	20688	62802	\$2661	19049	18349	0 \$
\$\$	2.962	23792 R.7	23559	23363	23.28	82652	27838	11822	22328	21976	21548	21877	*
0+	25218	24.740	24845	8.8.2	24266	24201	24150	24084	23978	23817	23589	23285	07
.	25.988	25608	25337	25178	25117	£ 2 2 2 3 3	25,185	25248	3-1-2	25.55	25858	2813	3.5
30	26855-	264.55	26344	25986	65652	20802	1:102	32502	\$2,92	26543	26625	20655	30
\$	£3825	53813	31939	3\$8\$2	\$1892	89892	27,728	8172	20\$15	324.5	2,895	3.8852	~
0.2	80682	28633	28322	29143	\$ 28 \$2	Sete	26.248	61802	28603	808ē2	8.085	23383	20
15	37489	30804	29842	29535	24825	29,803	854-2	255.62	30602	29848	30019	34184	15
10	\$3603	33606	33378	\$1815	39833	39213	30656	10648	39689	39743	30828	39921	01
\$	534.28	33005	32716	12401	32427	31899	31717	31576	33472	13401	31357	32334	~
0	34557	34208	33844	13477	33323	42793	32489	33318	31474	31758	31570	31473	ü
[1]													141
1. 10NG	100	185	190	195	200	502	210	213	220	522	280	215	1. 10M6

£- 10MG	194/	C * 2		(2)	•	3					•		
LAI													1 4 1
0	-13.2	-3176	-3376	43.6	2174	-13.6	-13.6	-1176	2174 -13.6	-1174	-13.6	3715-	06
£ .	848 -13.3	-12.2	-19-2	1272	1471	1684	1904	23.28	-4858	-10.3	-10.01	3008	8
80	1320	864	430	1306	707-	1188	1666	2352	2619	3976	3515 -6.0	5933	A ₀
75	1873	5987	1964	1911	23.0	20.02	1668	5338	3069	3747	752	\$008	75
7.0	5295	4425	10 10 10 10 10 10 10 10 10 10 10 10 10 1	2835 11.0	\$318 52.1	28.18	\$\$78	3231	9619	1983	26.23	11.2	70
65	7999	7035	6311	3897	9991	\$308	\$3.16	4977	31.4	28.6	7358	8505	9
90	11108	82701	9280	4823	2253	1828	33.3	3506	9859	\$228	32.15	19565	0+
\$\$	14389	13461	12546	11203	2.861	19313	19318	19435	13661	13872	12632	13857	\$\$
0,	17584	16773	15946	15150	145.4	138.3	13813	13597	13860	14361	15925	15773	0.5
4 \$	25802	19808	19314	18411	17753	17202	16846	16728	16850	17217	17764	72437	\$
40	22900	22435	21901	21323	9702	20224	19830	19622	19635	19879	202 04	20846	0 >
35	24923	24641	24273	23832	23349	22874	82425	22198	25903	222.3	22513	22955	3.5
40	2:32-	53852	29878	23959	4-46-	25135	24724	24397	24211	24,209	54379	5.86.8	3.0
\$2	24973	2806B -3965	27960	23738	\$2103	27804	28583	29399	25852	86252	25848	29863	25
0 2	29320	29381	29338	29173	26975	28689	58838	27598	27238	27012	5692	27062	20
15	30319	39392	38429	38528	29849	29555	29984	28599	24168	27853	7.917	9:872	15
10	3180}	33843	31005	30.80 40.80 40.80	39598	39818	29733	29215	62.232	53353	\$0882	24935	10
•	31718	33833	3,182,1	3,2873	3882	30658	8282	23862	288245	28499	29182	\$2882	~
0	315R\$	31373	33954	30805	5003	30327	29885	29366	28824 -50.8	28328 -45.5	27938	24883	0
LAT													1 4 1
F. 1086	240	542	750	255	260	344	,		000	300	20.0		, , , , ,

. 10M6	100	\$0\$	310	315	02k	325	430	315	67.	345	150	\$55	1 . 1 ONC
-													1 4 1
06	-3174	4114	-43.6	-13.24	-33.8	-13.6	-33.6	-3176	-4378	-1378	-33.6	-1174	06
~	3412	3406	3500	3761	3.81-	-1903	-11.3	45.54	4405	4488	4554	4603	8.5
0	4.3.2 B	4.8±	5030	-\$353	56.38	-12.9	-9323	-14:3	-15-1	1831-	-16.5	1:68-	0
2	5572	6095	9.4.5		7379	7713	8.00-	47.51	8460	8631	8769	4873	2.5
0,	0.00	77.85	8 213	83 2 y	92.0	9.62	998-	10352	10440	10623	35201	19857	0.4
•	18.9	9236	10358	10913	11385	11779	12303	12359	12561	12716	12829	70871	\$ 9
90	11290	12041	12703		13743	14329	14432	14669	14840	14874	15959	15109	0 €
55	13859	34.8	15253	15807	19263	19828	16913	173.59	17288	17396	17461	17485	\$\$
20	12328	1883	13962	19294	18832	12763	19459	13879	45841	16633	143.5	29814	\$ 0
\$	20721	9275	28378	7.98.Z	23329	23828	53863	23.98	23389	23313	22596	35 35 5	\$ \$
0	21858	28833	222.8	1363	3185	₹06€2	24348	22882	24863	25,046	253.9	28263	9 *
~	2,12.3	8:872	8.332	45182	25425	2.832	26438	35682	2333	\$3,552	5,852	\$6282	3.5
40	43.49	55872	28393	28458	27489	\$1812	29319	28782	28182	2824.3	28435	39868	3.0
~	7:047	20874	2.95	27967 36.8	83485	23158	129121	39267	30754	33389	31548	33808	\$2
0,	88832	82182	82828	28789	29387	39895	39898	33459	33968	32133	32858	32838	0.4
~	2 7899	28229	28670	29184	29734	30285	30,814	8091	29218	12801	32828	13057	15
10	6: 1=7	28379	287785	¥ 6 6 2	20554	25862	fitus	30448	30963	\$1296 2.5	31679	15/03	10
~	29031	28363	28378	82662	28843	29011	29125	29212	29315	79484	1:11:	30328	~
3	27574	27568	27614	27651	27629	27528	27562	27177	2,882	23003	27116	27.180	C
-													
1. 10MG	100	505	3.10	315	320	3.25	01.1	414	0 7 2	345	15.0	7	7407

9N01 • 3	د ,	~	ا ن	15	٥2	52	30	\$2	C	? ?	5.1	55	, C O N
AT.													٧.
0	5385	1,585	29 849	9285	22833	38282	39888	39834	3353	14842	328.8	\$3803	
•	24469	24803 -3803	25,183	\$285	25854	28353	70807	8,282	23893	82782	296RQ	\$7905	ı
-10	\$18.8	21217	23603	21838	21913	23823	24025	23382	24170	25118	56200	27.04	-10
-15	17898	1787	17833	17381	18046	18365	18869	19873	80802	21586 8.36	2 8 18	20882	ī
-20	15406	13871	14834	14729	14803	15096	15833	10418	17639	18649	19973	21328	- 20
52	13429	12958	15919	13643	12595	299821	13399	14264	15565	16635	62681	19893	-
-40	18973	11895	11869	13127	11237	11824	12394	13323	15368	15831	1:681	19108	- 30
35	11383	10989	18758	16734	19363	11651	26721	13363	19383	13172	14628	17634	Ĩ
0.	13563	11101	7:677	11133	11983	12053	12834	13780	14822	15871	16837	17644	7
4.5	11886	11860	13908	12138	12556	13354	1 1905	14764	15665	16536	1,7303	17905	7-
-\$0	13152	13,30	1325	13533	13955	14508	15363	4554	18809	17,872	17817	18846	٢-
-55	15983	20241	14448	15105	15269	15818	16829	16962	12881	17858	97851	14568	٢-
09-	14313	16339	16448	16237	16896	17207	17852	17903	18333	18509	\$0\$\$1	18783	04-
-65	1777	\$7.71	17825	17827	18973	18545	14929	18905	85281	18864	18903	18851	9-
-70	18822	18787	18388	18503	1884.	18892	81841	18974	18483	18851	17869	18713	- 7
-75	10283	19224	82861	10133	8.061	1905}	19903	18958	14832	18718	18848	18835	2-
-40	19043	18982	1891	18837	18855	18963	1855	18436	7.981	18135	17948	17734	ec í
-85	18953	14901	1784\$	17876	17809	17218	17671	17518	17401	17373	177.8	8.291	ec.
06-	14502	16302	16502	16302	16502	16302	16302	16302	16302	16 40 2	16302	16302	06-
141													-
, 10 M.C	•	,	•	1,	20	3,6	2	<u>۲</u>	4.0	4.5	20	~	NO T

1. 10NG	141	3	~	-10	-15	02-	-25	-30	-35	07-	-45	-50	-55	09-	-65	-70	-75	-80	-85	06-	LAT	6. 10N6
115		\$9568 20 <u>.</u> 9	38223	36318	3 5 8 7 8	81800	27,88	24378	20869	1481	14003	10907	8451	1338	1762	8353	11195	15012	14.700	18303		115
110		33858	38212	36114	33514	10801	27213	23798	20393	17113	14878	11466	-10.3	8978	9340	19358	12028	13487	14892	14503		110
105		\$\$\$\$\$	18068	35858	13031	80862	76587	21333	29803	12812	13308	12284	10920 - R-8	10467	19853	25581	12853	13963	15892	\$5\$\$4		105
100		38838	37794	35355	32455	28463	25960	\$\$\$\$\$	19745	17905	19818	13280	12297	11999	22881	12893	13654	155.6	15296	16302		100
\$6		\$3.88	37.98	34816	33814	36862	25374	24339	19637	1333	13808	14355	13646	1342}	1358\$	13958	14417	12313	15503	16303		95
06		38999 30.0	36886	84198	\$211s	23832	24837	55835	19648	8.757	16348	13818	14899	21251	‡92, 1	14928	15139	13364	15709	1\$303		06
8.5		38477	39568	33480	30369	65252	24324	213.12	13208	18153	13978	16385	16908	15844	15809	1\$29\$	15786	15798	15913	18303		88
8		37832	348.3	32678	29585	\$2862	23785	66812	133.48	18598	17688	17205	16839	16792	16683	16853	16378	16394	14112	16302		80
2.5		17083	34684	4827	26692	38182	23169	51138	19676	18719	18149	17839	13871	17551	17410	betz1	16902	16566	19505	16302		7.5
٧,		36254	33755	39785	6.832	24852	22433	20848	19462	18368	18418	18266	18197	18324	17983	17338	17358	16906	15491	16302		۲,
6.5		35374 R.3	12757	29585	26598	48282	235.5	19890	19964	2:561	18472	18475	18515	19213	18406	18759	17747	17214	16668	14303		65
0.4		34476	31718	2,855	25,384	2.852	1:462	12348	18459	18364	18303	18466	18632	\$25\$	18691	14483	19073	174.00	16835	34303		09
E. LONG	141	0	٠	-10	-15	-20	->2	-30	-35	0 %-	-45	-50	-55	09-	\$ \$ -	-70	-75	0K-	-85	06-	141	f. 10N6

t. 10N6	0	~	-10	-15	-20	-25	-30	-35	07-	57-	-50	-55	09-	-65	-70	-75	-80	-85	06-	LAT	t. 10N6
175	3484	35407	35253	34389	32888	39883	2 8852	26925	23395 -19.8	29898	1791R -9.8	15919	12959	9346	10.0	3585	13813	18835	14303		175
170	35195	35625	15378	34424	32829	39329	28282	25845	22899	29983	17178	14353	11969	8228	6913 14.8	2867	10861	137.78	14802		170
165	35500	35816	15460	34411	32328	34827	28285	23238	22374	19432	16392	13324	2997	13:59	19.90	31.8	1996	137.57	19302		165
160	35b 24 15.9	35997	35529	34377	32595	2088E	27667	25815	21833	18757	15568	\$5571	\$6. \$0.5 \$0.5 \$0.5	\$28	5114	7338	10599	13153	14302		160
155	16182	36204	32605	94344	32,906	30005	23358	24389	21566	18879	14721	11,323	8.82	3587	31.8	3,48	19507	13143	16.203		155
150	36582	36449	35701	34324	32345	24872	27938	21878	8,2 <u>0</u> 2	17382	1 1868	£3801	6443	3863	36.65	7102	19522	13583	16302		150
145	47074	\$6.709	35820	34317	32233	28868	\$6.242	24863	20213	16708	13935	-1389	-16.39	1822	36.73 50.73	7380 38.8	19859	13851	19303		145
140	37409	\$240\$	35957	34319	32123	2425	26432	53fēz	19695	16062	13255	-9578	-23.73	1339	\$808	£83}	bibli	13846	16302		140
135	15051	32328	36104	14322	32803	28238	5-6317	65222	3575	15951	11579	7549 -22.8	-3514	1868	4728	85.3	135.4	15269	19303		115
137	38474	37629	36243	34309	31861	24881	82150	355.25	18695	14.823	11035	-2334	-35%	2878	\$720 33.0	35.25	1325	19198	19303		1 30
125	18918	\$0022	36347	44258	31665	8.85	22452	21864	18215	14478	14711	-2159	-18:3	1504	6862 53.5	38.25	13129	15343	19303		125
120	\$9292	34113	36381	34119	51386	218-7	24905	21374	17765	14158	10655	-19.8	\$755	\$778	8079 28.6	19376	1385}	15518	16302		120
E. 10N6	0	٢-	-10	-15	-20	-25	-10	-45	07-	-45	-40	55-	04-	-45	-70	-75	0#-	-85	06-	LAT	1. 1046

t. 10NG	0	\$	-10	-15	-20	->5	-30	\$ k	J 7-	-45	-50	-55	-60	-65	-70	-75	-80	-85 -	06-	[7]	1 . 10N6
235	31413	37503	34378	39202	29519	8:182	1:812	26778	35836	30\$72	531.5	21853	25482	19173	85871	16749	14853	15918	14303		215
710	31574	31482	31145	30611	29925	\$6062	24114	26976	801\$2	24324	22884	21411	19824	18503	82621	16103	15598	15702	19303		230
522	31758	11796	31537	33059	10314	29418	\$3.8	27,110	61852	8-1-2	23892	2985	19303	13729	\$0¥01	15433	18831	15485	14303		\$25
072	8278	32133	31944	31412	39643	29303	32802	27188	25688	24036	243.89	20482	128.73	19878	22851	14741	1425	15271	16302		220
215	8138	32488	32358	31453	33838	22958	28679	27721	\$0952	23940	21868	20003	18038	19813	24823	14054	2784.	15060	16303		71 2
210	32489	32863	32779	32261	31878	30195	24399	27219	25485	23609	106tz	19511	17397	1543	11952	1 4 5 1 6 . 2	3.21	14857	16305		210
275	3863	33751	33207	32669	33863	30418	28892	8.8.7.2	£\$\$\$\$	23342	£1828	18999	16743	15956	13323	12598	78881	14663	14303		\$02
700	33123	3385	39 19	33873	\$3433	\$2,535	29864	27729	25832	23433	25808	15458	16069	13858	88521	11881	8-64	15481	14333		200
195	33477	34965	3\$468	3.5458 -24.8	38833	39308	29901	27013	24892	23673	24334	12873	13365	13937	11622	11172	12358	19313	14303		195
4.0	33844	34463	34554	33804	3258	30817	28989	26855	24808	23361	19814	17249	14619	19128	10559	19478	1355	1516}	16302		190
1.45	\$029×	34824	80275	34084	32774	1981	28914	26639	\$355	21793	19838	16566	13825	11833	7000	9807	11597	12933	19303		185
*	34557	35145	35862	62525	32878	\$9262	30057	26369	28.80	41873	18606	15823	17879	10348	8663	21.73	11279	13922	15303		180
2 K C 3 K S	0	~	-40	-15	-20	->>	01-	-45	0 %-	-45	05-	-55	09-	59-	-70	-75	0 £	-A5	06-	[4]	E. 10N6

9401 .	740	\$42 .	U\$.	58 2	7 6 0	597	270	512	240	285	<u>د</u> ک	£	7N01 - 1
141													141
	318.3	1117	31858	3885	39863	30327	29885	39162	2382	28328 -45.5	5.82.7	2.88.2	5
-\$	30803	1985	39878	\$2892	32832	85872	22248	283.9	22381	28835	53125	23804	\$-
-10	\$9865	19161	45852	23894	2985	13133	26825	29514	7.627	27039	28582	28929	-10
-15	29814	29462	29143	28852	21559	28202	27773	27248	26641	25996	25368	24809	-15
- 20	8010.	28705	28 52 0 2.5	27949	27576	27168	25508	26142	23308	24918	24128	23478	- 20
-25	2 # 3 2 9 40 * 8	25872	27475	\$ 29.2	26.60	29159	\$2657	23936	22374	23957	28929	28829	52-
- 50	27566	55652	45.34	Sef 92	62852	25524	24683	24079	23802	28489	85 88 2	28882	-30
-45	29813	28397	25829	25423	24984	20842	23880	23390	25733	25813	2382	2882	-35
-40	25500	25311	1.50.55	6.275	24425	24825	23559	23025	25415	21737	21017	20278	0 4 -
-45	24445	24430	85572	1222	24828	23743	23385	22940 -41.8	23419	5 3803	233.8	29429	-45
-50	23371	23551	23672	23727	23691	23568	23847	23025 -38.0	22604	22095	21810	20865	-50
-55	29852	22636	22944	23875	23314	23353	23588	23998	22872	58425	232.1	23401	-5\$
-60	21899	21623	22825	\$5\$2	35357	24833	23805	22962	22814	22566	25256	22808	0 9-
-65	9.84.	20802	2.1923	10512	21879	24189	82352	23456	25443	28338	\$\$\$\$\$	23873	59-
->0	18551	16161	13 61	70263	\$1502	20012	21338	81812	21813	21639	21588	23474	- 70
-75	17359	17928	18451	18922	19336	19695	10987	20250	20394	29513	29574	20559	-75
-80	3.841	10803	17398	17855	17984	18279	18549	18765	18956	19313	3585	1:321	98 -
-85	16131	16340	16541	16735	16919	17091	17252	17908	17535	17657	17764	17859 5.8	5 9 -
06-	16502	16302	16302	19303	14303	16302	16302	16302	16302	16302	16502	16302	06-
. 41													LAJ
	070		030	3 3 6	1	* ; ;	•	,	•		6		

1. 10NG	. J	₹	-10	-15	->0	->\$	-10	-15	01-	-45	98-	-55	09-	-65	0.4-	-75	-80	-85	06-	141	1. 10N6
355	84.82	26.229	21962	18209	1582	-13867	-1695\$	11908	1176	123 53	15313 148.4	13678	14385	17842	18893	19352	Loter	18093	16302		355
0 5 2	61882	24135	22278	18526	16318	-165.3	13308	-103.6	1628	17852	13904	1498	1,181	14873	3 8 9 9 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	19439	10166	18126	16502		150
345	\$3403	5-65-	23443	18966	16900	-18859	-18828	-13212	12904	18368	14012	12304	18861	19303	19343	10535	19223	18151	50891.		345
340	8887	24445	22862	18530	17565	-15984	-16678	-13956	13592	13779	14523	15728	13328	18418	19324	10647	19378	19841	16302		078
3.45	81113	24812	22408	28195	18290	-16753	-18858	-16625	14131	18858	15120	16224 15A22	17528	19323	19536	52281	19328	18172	16302		335
130	£48₹27	25843	23022	20917	89681	17537	-181:1	-15503	15897	18881	13783	16801	12999	1908	18379	19901	10374	18822	16 302		130
325	25528	55687	23634	23638	18432	16308	18113	18879	15868	15839	19899	17433	18523	13431	25862	28837	19418	18161	\$9584		\$2\$
320	27629	24052	24186	22307	\$3857	19938	17953	12855	16628	16703	1333	19101	18641	10897	£0\$67	293.73	19449	18139	50841		120
315	27651	26284	25645	22894	21803	\$1767	18833	17733	17369	18404	17981	18387	19658	58882	29883	7.36.2	19456	18107	14303		315
110	27614	26463	22975	24399	21388	28859	19186	16418	189.3	15618	15751	18\$79	29336	28.28	29848	20802	19456	18963	16 302		110
303	27568	26603	25326	23851	28335	503.	19829	19100	19913	18001	19462	58185	29298	21879	23993	24509	15856	18008	16302		305
400	24827	99247	2564-	24303	28885	23862	28292	10798	19269	19708	285.48	5825	23828	21848	23805	29863	19391	17940	15.2		100
5 10 10 10 10 10 10 10 10 10 10 10 10 10	0	~	-10	-15	->0	->>	- 10	-15	0-	-45	-50	-55	-40	-65	-70	-75	04-	-#S	06-	141	t. LONG

• LON6	င	•	=	•	;)		•	;	÷	-	4. 1086
													1 A J
06	56443	56443	56443	5044 2	56443	56443	56443	56443	59463	59463	56443	56443	06
\$ H	55488	55513	55551	55600	55863	8:215	55812	55901	55997	\$6099 -16.8	56206	56315	\$ a
0.	54428	2445	54531	84629	54758	54915	\$ 5 0 9 9 - 6 • 5	55308	55537	55783	56043	56311	80
7.5	5 1365	53393	53476	53612	51799	\$4035 3.2	54318	54645	55011	55410	55836	56282	7.5
20	52435	54359	53443	19493	83458	54128	78825	53905	54383	54912	55486	\$6095	20
6 \$	51353	51833	51433	\$1808	51857	54389	32595	8.38.5	53825	54843	84858	80655	99
9 0	59261	54287	50398 19-6	59593	50863	81818	51848	5:51:3	52338	53565	2+1+3	54949	90
55	49067	49127	49273	\$ 34.08	\$505	50165	50805	51115	51706	52380	53134	53962	\$\$
\$0	47673	47789	47990	48262	48595	48986	40434	17.6	50526	51183	51915	52722 R.7	\$0
4 .5	46047	46233 22.8	46501	46832	47213	47632	4.88.	46603	4937	49798	50489	51243	45
0.	44190	64449	1283,	45179	42,603	46957	46536	47048	47601	48198	48841	49528	0 🕈
15	43738	42463	42863	43304	41766	8-42-8	44729	45243	45786	46358	35394	\$2523	35
30	30952	49335	6278	41250	41728	45203	\$385,	43503	43735	44285	44946	45408	J.
52	12218	347.2	38849	38323	39595	49061	49530	41017	41527	42054	425 R4	43106	2.5
02	55687	36136	39613	37088 17.1	37544	37979	37408	18855 5.5	39321	39813	2,80+	40818 -8-8	20
15	31939	34612	34895	35358	3.88	36189	36 \$ 51	30098	37329	37769	38246	38747	15
10	32938	33344	33665	34103	34508	34845	35142	2842	35348	36316	34578	34898	10
~	31787	\$23528	32885	33355	34738	34925	34,236	35418	358.8	35855	35408	35999	₹
0	31566	31000	16428	32981	323.4	3888-	33308	33799	33946	34239	34736	35643	0
LAT													LA3
9,01	c	~	10	15	20	25	5	3.5	0.4	45	5 0	<i>y y</i>	F. TONG

nT (units: nT)

<u> </u>	ć	ξ	C	00	\$ \$	5	ŝ	60	ŝ	C	<u> </u>	1 - 1 ONE
6,46	59463	59443	59447	56443	56443	56443	56441	56443	56443	56445	59443	06
98.	56536	56644	\$674R	56848 -21.6	56941	57976	\$3103	53172	57227	57275	57311	8 5
8 8 3 5 8 3	50854	57116	11815	57805	52825	58977	58125	58302	58399	58463 -26.5	58494	0 %
97	57194	\$2675	58070	58467	58824	59132	59383	59572	59694	59748	59735	75
	57363	57994	58599	59163	59667	60097	60438	82842	41465	\$ 8 8 5 2	8502-	70
~°	57219	8008	2.588	82 765	21109	25609	61278	61361	61495	£2510	\$6\$15	65
808	56694 894	57599	58408	18865	60923	60649	61128	61438	61561	61583	61319	09
15.8	55783	56727	92828	58540	59334 8.5	400 v 4	60517	60839	60830	8-709	604 30 8 . f	\$\$
-53	24507	55465	80378	82528	58861	8£ 8 ys	83843	50543	59612	59426	58978 10.2	20
52055	\$2909	8.3.5.5	54665	55503	\$6263	26905	57377	57648	57680	57448	56249	45
-040 V: 1	51913	51405	\$2590	53344	54029	54602	55023	52525	5\$348	54981	54438	07
4 2 1 5 -4 -8	48875	49551	\$0226	\$0877 -7.1	51467	51959	52313	82491	52455	52172	51622	35
20.	-10.8	£1112	41484	48232	48728	49136	49427	49554	49493	49209	48676	30
517	77857	44624	45119	45599	7.65,	46351	46583	0.694	6356,	46328	45824 18828	\$\$
2. 5.	41798	44578	42747	44136	43578	43873	44969	44137	44054	43797	43346	20
798	39282	40308	40814	412R3	41683	41992	42186	42246	42362	1351,	41516	15
37683	38303 -11.1	38944	19547	40119	16507	40956	41167	41256	41179	4.99.	8.5.	10
36704	17482	38287	39074	39799	40418	04U 80 0 80 0 80 0	41184	41294	41228	41011	40671	\$
24	37316	36.35	39368	49309	41115	41738	45141	42316	42283	42086	41773	0
												LAI
0.9	65	70	75	08.0	88 2	0.6	95	100	105	110	115	1 . LONG

25		\$1 \$1 \$1 \$1 \$1 \$1 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0	\$50 \$50 \$40 \$50 \$50 \$50 \$50 \$50 \$50 \$50 \$50 \$50 \$50 \$50 \$50	28463 97343	59443	59463	59463	56463	58443	56443	90
201 221 221 221 221 221 221 221 221 221		me me my on ey oo no vo nr	24.55 27.35 27.35 27.35 27.35 27.35	29443 57343	29443	29443	59443	28443	584.3	26543	06
22338 28482 29658 206638 20766 207663 207663 207763 20		mc my on cy oo no vo nm	27.15	13825						4.17-	
2		my on cy oo no vo nm		3013-	57323	57298	57373	51242	57211	52780	8 €
29658 27560 27560 27573 27573 27575		on cu oo no vo nr	25	58931	\$\$8\$₹	\$3805	538.8	2,685	23883	57516	er C
29569 29671 27673 27673 59875 59875 59875 59875 59875 59860 5788 5788 5788 5788 5788 5788 5788 578		cur oo no vo nr	2869	30665	58335	58978	57827	57612	57434	57296 -20.k	7.5
\$ 98.75 \$ 98.85 \$ 98.85 \$ 98.85 \$ 98.85 \$ 90.86 \$ 10.11 \$ 10.11 \$ 10.12 \$ 10.1		00 10 10 1	23.0	58556	3083	57632	22825	56883	56612	50424	2.0
\$ 98.75 \$ 98.75 \$ 10.11 \$ 61.60 \$ 14.60 \$ 14.6		No vo nr	3600	57883	57.5%	56539	55953	52855	55114	54882	65
2		vo Nr	2518	26565	65855	4.1.5	54058	53454	53918	\$2744	9
\$6160 \$4160 \$4160 \$1618		~	5838	82675	\$ 1 \$ 6 3	52548	51673	\$0969	59469	sayea	\$\$
5 19.00 5 18.18 5 1			54654	52335	51079	0-6	48969	48394	47649	47319	0
5 18.18 5 18.18 5 18.00 5 18.0	15.2	52546	1117	49696	48353	4734.3	46323	45316	8,2,,	825,,	4.5
47888 47888 47888 50.2 50.2 45101 45101 45159	51269	49854	16.373	46918	45549	44328	41302	42502	41946	41640	07
47888 46863 20.2 60.8 45101 44159	48457	47057	16.7	44157	42819	41635	40651	39896	39389	39122	3.5
19.9 44.159	45648	7.81	-2926 -15.8	41373	11607	39214	38307	\$7625	37183	36973	0 t
	19.5	£261,	£9\$65	19334	34198	37206	36397	35799 -10.8	35475	35269	52
16, 2081, 2085, 00	9449	39804	\$ 3.5	31818	36629	35748	35938	34514	34198	34808	9.0
15 41948 49527 39	9387	38.44.64.64.64.88	12.8	36595	8:835	34868	34338	13861	33555	33403	15
10 47623 39470 38	15.1	1601	12.8	10398	35845	34960	34371	13899	33555	33429	10
\$c \$0.76 8.34 5	39319	38468	12.5	37928	36412	35,79	35185	34873	34349	33868	~
41381 44929 40	0423	11.1	11.11	38644	30088	37.578	36761	36173	35624	35119	J
LAT											LAI
E. LONG 120 175 1	130	135	140	145	150	155	16.0	165	170	175	1. 10NG

1 8 6 0 F													
0 6 6													1.47
% 0 €	56443	50443	5\$443	29443	55443	56443	56443	56447	56443	56443	56443	56443	76
0	55143	0.97-	57088 -25.8	57058	5.85-	5,2808	56973	56942	55911	56878	59845	59806	8 e
	27549	57366	57363	57345	57338	53346	57357	\$7575	\$7396	57414	\$2428	52429) 6
2	57204	54158	57158	57198	57276	57384	57515	57669	57810	57957	5,6003	58503	25
70	56325	5630A -8-6	56377	56524	56738	57006	57314	57643	54393	58328	58944	58927	02
99	54783	54813	54980 3.0	55259	82635	\$6095	36918	\$2169	57737	58296	58825	59306	\$\$
99	\$5825	8\$\$\$5	52898	23805	53845	54589	55313	\$865.	8.695	85825	59403	88385	٧0
\$\$	\$ 49.74	80545	50527	51038	\$1208	52508	53404	54359	55339	56318	57247	58119	\$\$
20	47538	47385	47756	48330	48983	9880	50987 8.8	\$2965	23878	54286	53364	59383	36
*	\$ 5 5 7 7	\$05**	26877	45488	20200	80524	48258	985-	50552	51733	52892	54006	\$ 7
0*	41579	41750	42137	12127	0-111	44386	45412	46524	5.885	48672	54849	28175	07
\$	39091	39275	39649	49194	866 0 ,	5287	29624	43701	44796	45924	63827	48184	3.5
30	36980	57173	37523	38006	38609	39326	40147	41057	42037	43061	44105	45151	0 \$
25	35308	3885	35298	36198	36889	37253	37929	34878	38503	49385	71898	483.18	\$2
20	35498	34267	3452	19162	33113	35524	36017	36595	37247	33053	38603	32648	2.0
15	3 3 8 3	33453	33576	33730	33918	34158	34466	34851	35305	35.3	3835	36915	15
5	33205	33146	33123	33326	33348	4320g	33313	33898	33743	34039	34354	34703	10
~	33614	33386	3418	33508	35855	38728	32650	72624	32646	32709	32807	32935	\$
o	34658	14237	37846	3480	37139	12829	32555	32319	32122	3:07-	3.1838	37275	C
191													LAI
1. 10NC	180	185	140	195	200	202	210	215	022	225	730	517	F. 10N6

9 NO 7 .	740	745	250	555	092	597	2 7 n	275	280	582	000	^ •	I. LONG
11													1 4 1
0.6	25443	59463	55453	59453	\$\$\$\$\$	56443	55463	56443	56443	58443	56443	58443	06
y.	5,265	56729	56670	56616	56557	56494	56427	56356	54281	59204	56126	59047	an ac
0	57420	57396	57355	\$7294 -21.0	57214	57114	56993	56854	54696	56524	56338 -16.5	56144	0 &
۲۶	58297	58352	58369	58344	58274 -21.8	58152	57995	\$7789	57543	57260	56946	56608	22
0,	59163	59343	53458	23202	53863	59357	59167	58901	58564	58164	57709	\$7.513	0.4
45	59721	25007	-28.4	5,662	\$2000	60390	2-139	59878 -30.9	59459	58645	58350	5.885	. 9
09	59694	\$0565	69809	4085 P	8605	69953	80865	£3685	38885	59340	5 8 6 1 8	53808	09
\$\$	58905	59584 -38.8	4014-	60536	60772	60826 -24.8	60689	60359	59844	59159	58332	57395	\$5
٠ 0	57321	58153	58854 -48.8	59399	59761	59918	59853	5955F	59039	58314	53818	56379	\$0
23	55050	\$6401	56879	57505	57987	58253	58573	58935	57541	56807 -60.0	55868	54770	4.5
0,	57294	53315	5885	25825	55583	55943	56048	55876	55426	54713	53765	55639	97
35	49276	50310	51256	52074	52719	53146	54317	53208	52811	52135	51311	59992	3.5
1 0	46181	43373	58092 -58.8	4.8904	40563	58916	58528	59179	49627	49203	48326 -83.6	41245	30
25	4,1432	4,892,8	46868	45857	46343	46696 59.98	46924	48800	\$0.865	46943	45231	44517	\$
0.0	40213	40007	41685	42345	42903	43313	43533	43527	43276	\$2585	44843	43117	20
5	37491	38978	32244	38389	32843	32896	49194	48185	39966	39524	38873	380.6	1 5
10	£287£	35463	35873	38862	328.3	36889	37921	35608	38193	19401	35825	35105	10
~	3.88.5	33292	33818	33847	33869	34118	32178	37808	33888	33513	37893	32358	•
0	3.6912	31689 -37.8	31773 -35.8	31779	31830	31841	31781	31622	31348	30957	30464	29898	0
A T													נאו

E. LONG	.)Ω ,	£0\$	110	315	ú?	\$2\$	U\$,	\$ 23	C 7 ×	545	ς .	(,,	1
141													
06	56443	50443	55443	59443	56443	56443	56443	56443	56443	56443	56443	56443	36
\$	5.468	55892	55818	55748 -16.F	5.684	55624	55576	55535	55503	58485	53878	53474	à.
0	55943	25845	25249	55345	55955	54.988 2.0±0	5.83. -83.	00275	54590	9°5- -5°6	54450	54423	<u>a</u>
2.5	56254	55891	5:152	\$5171	54830	54512	54222	53967	54753	53582	53459	53785	5.2
0.0	54987	56349	55692	25863	89875	54045	53655	22888	82828	\$5825	\$5 <mark>8</mark> 08	52467	7.0
65	\$6695	58469	55546	54841	54178	5355	\$5825	\$2515	\$23.09	81,286	515.5	51393	\$9
0.	56944	5,885	55365	5430R	53503	52769	52119	51562	51303	20245	594.85	59328	99
\$\$	56389	55353	54328	53348	25561	51828	50.921	\$0450s	65864	49488	49240	49102	\$\$
96	\$\$\$\$\$	1:435	52388	51813	5984	29982	76361	48766	48301	43624	1381,	8:8},	3 {
45	\$385	55344	24143	52213	43817	48158	5.43.5	72894 12894	46459	46.159	\$5.45	45884	5.7
0,	21403	50124	48881	47739	46732	45891	45218	44892	44329	44097	608++	44834	0,5
45	48847	47557	46396	45163	44179	43378	£3855	42303	41997	41834	41806	41919	\$
30	46029	44763	43845	42813	41479	40717	49156	39771	39540	39449	30492	39664	30
\$	79697	4. 6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.	48478	13818	38823	38828	33835	33323	31973	32028	37178	37408	\$2
20	2.5007	*8939 -92.3	37848	36861	36043	35425	35015	34792	34731	34807	35001	35 100 5.8	20
15	60125	36998	38123	34368	33530	33218	32719	32613	32862	32850	33139	33508	1.
40	34874	13404	32568	11831	31268	10894	39743	30789	379R4	31296	31693	32144	10
~	37650	34925	39246	29680	28385	28102	29328	29342	29698 5.8	30150	30665	31217	~
o	5.045	28717	28808 288.3	32835	27632	27640	27856	92285 9. A	28732	29315	29947	30604	G
141													1 4 1
F. LONG	400	305	110	315	120	325	Û € ≥	318	140	345	350	355	ONC 1

5 t 10NG	0 E5	5- 56	·	24- 36	9520	·	359 -30	196 -35		57- 99	0550	55- 25	18 60	50- 35	113 -70	27- 640	·	\$805 -85	06- 26	
\$	56.9 3564	<i>~</i> 1	•					36896									35.54 8.87.	5 1	97 5649	
\$	m i		3618 34224					197 34405									51543 523	V 11	197 564	
07	3946 3453	F 1	PO I					15x \$2508										3938 545	40.7 5649	
\$ *	mı	3336 33	mı														59481 59°	~ i	84.27 548	
30	- 1	34304 3						28952								46393 4		\$3457 280-2	54497 5	
\$2	13580 -3880	33346	\$2737	31888	39703					28318 -69.6						45799	45814	53251	56497	
90	37347	33969	32807	31802	30943	29290	28922	27,12	26983	27613	29080	31313	34193	32583	41333	45284	48261 48663	53069	56497	
15	32981 -1590	82755	12301	11556	30468	29176	28824	28301	-103.2	-32136	-48159	30615	33494	38844	40789	44856	4 8 9 9 9 9 9	52914	56497	
C.	16421	37515	31809	31122	30134	28956	27,788	-10481	-112.2	26826	-14323	-18822	32960	36444	40359	44514	48721	52786	56497	
~	31009	31582	31164	19863	29647	28609	28579	-101-9	-26361	-122.4	-12031	-19739	32576	38978	6.082	44257	48537	88432	56497	
င	31266	30873	30418	29808	29032	29156	56847	26593	-14555	26507	-122.6	-1921	-18328	35835	3982	44083	48408 -82.2	28918	56497	
E. LONG		٠	04-	-15	-20	-25	04-	-35	0.9-	-45	05-	-45	09-	-65	-70	-75	0 % -	-85	06-	

9ن	4.5	U/	7.5	C 80	ec ec	06	95	100	105	11 0		10NC1 . 1
												LAT
29324	32318	38358	19369	40303	41115	41738	42343	42316	42283	4.5086	4123	0
8065	17662 8.5	3,97,1	40256	41449	42483	47296	43847	44124	44359	\$065,	43729	S -
36758	14.1	39916	41491	42958	44245	45883	46018	46442	46584	46509	46294	-10
37209	38978	49883	45866	44591	46340	47419	48373	48984	49279	19324	49209	-15
10.0	39847	42039	44174	46189	47981	\$0267	50691	51516	\$2909	\$2563	\$2203	->0
38183	49918	43047	45511	8,62,	,186,	51413	52822	53872	54571	54959	55108	-25
38393	43819	44929	6\$64,	45834	53355	53665	51218	55878	56 88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	23828	57789	-30
38258	48583	9-24	47630	59138	52462	54544	56128	57778	58885	\$9965	60168	54-
40518	8552,	44894	48663	21515	\$3808	82.78	82828	12865	60553	61519	£2829	3-
4 16 79	44355	4 1835	\$9600	\$2303	54595	56798	58766	69463	611.8	62963	63771	-45
4 1013	45554	48108	50633	54085	55421	57595	23563	53965	64775	63973	64892	-50
44505	46839	49202	51554 -26.0	57855	54063	58140	60049	61757	63239	64478	65466 9.8-	-55
44333	49852	80485	53413	54496	56506	58414	69387	\$3055	63821	65643	1:545	09-
47852	49616	53616	5335	55813	19285	58429	58836	82615	3:355	63878	64844	-65
828	51893	53853	58901	55855	56873	58243	59543	55275	61868	75825	63736	-70
51858	\$2\$606	53677	54760	55839	56903	57936	58927	59863	35785	63534	\$5\$55	-75
53416	54095	54788	55499	56193	56887	27867	\$2585	5385	59455	60008	60520	-80
7.7	55445	55778	59118	59858	1.585	57323	57447	57759	58059	58343	58609	S &-
5885	5885	5693	56497	26493	56497	56407 -R0.7	56497	56497	58493	28485	58465	06-
												LAT
09	65	7.0	7.5	8.0	85	06	95	100	105	110	115	E. 10N6

TOTAL INTENSITY (F) WMM-90

E. 10N6	0	-\$	-10	-15	06-	-25	-30	-35	07-	-45	-50	-55	09-	-65	-70	-75	-80	-85	00-	1.41	f. ton6
175	32113	36986	16261	42172	45139	48127	21818	53743	\$2.38	5385	60750	62610	82675	\$2879	65103	64315	25435	59897	56497		17.5
170	35624	17655	46711	43314	62797	49212	\$31153	55841	54348	59632	61678	63425	7:285	62829	65466	64538 -58.6	62625	59936	56497		170
165	36173	18334	41012	44016	8,72,	50237	53173	55893	58373	-3200	53523	64206	65389	45965	\$77.3	64704	95139	23852	76497 -80.7		165
160	36761	39011	412.0	44858 2.8	48959	51183	27173	59862	58335	63525	23418	64936	65869	66373	62213	64809	62754	538.5	56497		100
155	37576 12.0	39675	42497 8-9-8	45651	₹98ē,	52038	5\$843	\$385\$	30265	62367	29825	65593	69173	68707	28182	64848	62723	59893	56497		155
150	34007	40319	44165	46329	49596 -5-8	7.525	54793	58536	68885	63119	64863	66156	64889 24889	66951	8-88-5	64818	62636	52824	56497		150
145	38644	40937	43780	46950	\$0528 \$0.505	53436	24458	28185	61838	63732	65414	66599	4118	67983	<u>6</u> 6258	20255	62498	12182	58485		145
140	39270	625617	44538	47492	59764	53873	54986	25737	£\$8\$5	64211	65822	60899 80899	25855	67903	87155	81875	62305	59604	56835		140
135	19867	42358	44834	4795R	\$1207	54397	3.33	<u>6</u> 0126	£2\$29	6452R	66061	67030	65\$29	56975	65916	£7875	62957	59454	56495		135
1 50	49423	42546	45271	48354	51567	\$2255	51899	82409	\$2\$ 29	9.079	90 v9	12599	82129	96845	63369	64880	\$3875	59278	54497		130
125	25642	42985	45656	48690	51853	54955	23825	60483	62759	26579	65944 1.8	1.1.	66806 4.84	25285	659.83	63427	61495	59078	7.08-		125
120	41381	43381	4 59 09	8.844	\$2073	\$ 5005 \$	57908	82509	82\$29	90579	0.55.0	20299	64436	\$\$ 36	235.8	64884 640.2	6888	58854	56497		126
E. LONG	0	ş-	140	-15	->0	-25	- 10	\$	-40	-45	-\$0	-45	09-	-65	-70	-75	0 <u>k</u> -	-85	06-	141	E. LONG

E . LONG	180	195	190	195	200	502	710	215	026	525	n & C	3 k 2	1. 10NG
LAI													LAT
0	345.8	18672	23849	13489	32138	32829	32555	32319	35135	37825	319 10	3,27	0
~	36338	15719	35131	14576	34053	33556	33000	32652	32242	31468	3.13.6	21315	Age, 5
-10	39572	47771	37,001	36265	35564	34894	34348	33625	34923	32444	31900	71403	-10
-15	41213	40260	39335	48449	37583	3675R -35.7	35957	35175	34409	33664	32948	32271	-15
-20	44979	43914	41969	46648	39967	39919	3 0 0 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	37196	34308	35.63.5 38.35	345 78	3,287	02-
-25	27405	45873	44745	4384 8	42579	4348	40549	39570	39603	37638	36676	35715	-25
04-	23873	18303	47550	46613	45308	44239	43205	42185	43834	-2155	34318	38958	J _F 1
-45	20925	51454	50374	49173	48072	4340\$	1,885	8705-	43813	42865	41771	40619	-45
04-	54181	54071	52965	51815	50815	49383	48767	47757	46729	45658	445.72	43304	07-
-45	52888	58545	53518	54498	53489	52506	51529	\$0543	40518	48433	22324	46903	-45
-50	59804	58853	57900	56968	56039	55113	54178	53215	2022s	51118	49941	48658	-50
-55	61373	660331	£2825	58534	54378	52313	56618	55683	54689	53616	53453	51183	-55
-40	62375	55555	61308	61159	60372	59566	58722	57826	56867	55835	558.13	23803	19-
-65	64413	63818	63193	£\$\$35	61840	\$1108	62324	\$2898	58403	57639	56604	\$5494	-65
-70	046.8	44829	63858	2382	58285	<u>6</u> 1953	61266	60529	59737	58890	57949	52025	-70
-75	64039	63712	63,538	62917	62451	61939	61383	60782 -68.9	69137	59449	38858	53953	-75
0 K -	0.64-	42199	61956	61674	61353	69895	90565	29173	59718	59228	58713	\$8174 -80.3	-80
-#5	5.0831	59749	59675	59486	59324	533.9	58937	58714	58475 -90.6	58219 -81.0	57949 -81.5	\$7668 -81.9	-85
00-	\$ \$4.03	58493	26495	56497	56497	56497	56497	56497	56495	20795 180.7	58403	58485	06-
LA1 E. 10NC	140	185	190	195	700	205	210	215	220	\$25	230	235	LA7 E. LONG

t - 10N6	o	. 5	-10	-15	-20	-25	-30	54-	07-	-45	05-	5 5 -	-60	59-	-70	-75	0 & -	S & -	06-	1 4 1	1 . 10NG
\$67	29898	36822	26106 -48.5	24876	3373	23843	54845	3,285	26015	27872	10744	35391	36895	79867	44464	48063	51295 -86.A	54093	50497		562
J 62	38\$58	28318	26621	25417	62883	24524	25835	25628	26976	28903	31420	34477	37952	53838	45334	48772	51799	\$\$\$\$5	56497 -80.7		U 6 C
285	39852	28823	27773	26054	55463	25398	22829	28734	28163	39148	32684 -81.5	38528	39134	48738	5.685	49525	52330	58633	56497		2.85
780	33344	222.3	2222	26744	82832	28812	26984	2,482	29545	31574	34111	38103	40429	43895	48584	50317 286.8	52884	5#8?1	56497		780
275	32825	23846	28248	27448	33852	30512	28253	28435	31058	33138	35671	38904	41819	1,187	48313	51149	53458	55219	56497		2.5
316	337.3	24845	\$2 7 52	28133	22125	52832	29578	39916	32657	34797	37326	76865	43283	46424	20205	51588	54045 -85.5	55523	56497 280.7		270
592	33341	38165	29146	78778	23903	29733	30898	32449	34 50 50 50 50 50 50	36508	39039	41837	26245	\$5825	58509	5885	54643	55833	56497		592
761	र्वे के देवे	39333	29529	29378	29837	3,803	35389	34909	35935	38232	40772	43505	£8335	49306	51835	53328	55246 -84.5	58345	5.885		260
552	13828	30469	29963 -36.0	29941	39633	11831	33632	15365 -28.5	37546	38836	42491	45164	43864	50456	3.252	54604	55849	56457	56497		552
750	8:318	30604	30200	30490	33409	32824	35828	38778	391n5 -19.0	41585	44163	46784	49347	£1283	53878	55473	56448	56768 - 63.1	56497		250
572	11988	39862	39557	31049	33366	35795	35829	34118	44592	43150	45769	48340	50812	\$ 5878	54964	56323	\$ 5835	57075	1.08-		597
240	36818	\$286\$	50953	31638	\$3843	34756	36852	\$2\$03	41994	44637	47263	49813	52801	54318	56018	\$7358	57615 -81.2	\$2825	56497 -80.7		240
E. LONG	0	-\$	-10	-15	-20	-25	0,-	-15	0 -	-45	05-	-55	-40	-65	-70	-75	0	2 8 -	06-	147	f. 10%6

	E. LUNG	400	305	01.	315	420	325	130	515	071	345	45.0	355	1 . 10NG
	LAI													141
1862 1862	0	29299	58213	28808	05 877	27632	27640	27850	28229	28732	29315	20047	10005	င
	-\$	2 78 8 2	26439	26499	2630 A	60817	26485	2+845 4-8	27357	2,863	28651	\$23.5	30124	\$
1411 23599 23613 24619 24649	-10	25005	25333	23342	23321	12873	28282	26465	65445	27321	78053	2882	2962	-10
11 11 12 12 12 12 12 12	-15	24468	23323	53783	2425# 8.88±	24529	24943	25467	260.65	15192	27485	28249	29034	-15
1442 1444 1444 1444 1446	-20	11285	23308	23513	\$0\$\{\bar{0}}\}	87672	60872	\$2953	25659	26289	26852	27655	28354	-20
1862 1864 1867	->>	23395	23193	62882	23845	23818	24542	24813	25,708	25931	\$6\$65	5.68.5	58835	-25
101 1 1 1 1 1 1 1 1	01-	2352	23581	23582	23188	27879	25278	2,56.2	25826	25689	28 325	28851	28843	- 30
2827 28814 28824 28820 28903 28928 28928 28929 2	-15	55135	23829	23742	23871	24143	24496	24876	25242	25583	25821	28169	26394	-35
2917 2807 2807 2818 2818 2818 2818 2818 2818 2818 281	97-	25312	24872	24673	24672	24811	25925	25275	25512	25718	25890	-26939	26149 -110.6	-40
29471 28797 28797 27753 27750	-45	2,2825	26818	26269	\$06\$2	25972	26019	26304	26192	26267	-105.0	26375	-126.38	-45
25673 17716 3100 30637 29896 29872 29607 29677 -49393 -49393 -49359 -49393 25673 18609 18609 29700 17960 17960 17960 -17050 -17050 -17050 25708 18609 <t< td=""><td>05-</td><td>29471</td><td>28797</td><td>28309 -67.5</td><td>27977</td><td>27766</td><td>27637</td><td>27558</td><td>27504</td><td>5863</td><td>-48439</td><td>-\$7431</td><td>-121.0</td><td>-50</td></t<>	05-	29471	28797	28309 -67.5	27977	27766	27637	27558	27504	5863	-48439	-\$7431	-121.0	-50
582.1 158.6	-55	32473	31714	31109	39637	39578	29898	28773	29607	29477	-104.5	29357	29791	-55
2927.9 282.0 387.2 387.2 387.3 387.5 387.5 387.5 387.5 387.5 387.5 387.5 387.5 387.5 387.5 387.5 387.5 387.5 387.6 387.5 387.6 387.5 487.6 487.6 487.6 487.5 487.5 487.5 487.5 487.5 487.5 487.5 487.6 <t< td=""><td>09-</td><td>35967 -8367</td><td>15169</td><td>3466</td><td>33929</td><td>33462</td><td>33077</td><td>32764</td><td>32515</td><td>32327</td><td>32205 -97.0</td><td>32155</td><td>32190</td><td>-40</td></t<>	09-	35967 -8367	15169	3466	33929	33462	33077	32764	32515	32327	32205 -97.0	32155	32190	-40
4864 4825 4820 4820 4811 3969 3865 3861 4820 4820 4815 4815 4816 4820 4815 4816 4816 4816 4816 4820 4820 4816 4816 4816 4816 4816 4816 4816 4816 5820 4820 4816 4816 4816 4816 4816 4816 4816 4816 5820 4816 4816 4816 4816 4816 4816 4816 4816 5820 4816 4816 4816 4816 4816 4816 4816 4816 5820 5816 4817 4816 5816 4816 5816 4816 5816 5820 5816 5816 5816 5816 5816 5816 5816 5816 560 5816 5816 5816 5816 5816 5816 5816 5816 560 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816 5816	-45	30776	18987	38294	38698	37178	38743	36381	36891	35478	38633	35673	18704	59-
-47607 -48703 -48918 -48509 -48918 -48509 -48918 -48509 -48918 -48509 -48918 -48919 -48919 -48919 -48910 -48109 <td>04-</td> <td>4364</td> <td>18887</td> <td>42585</td> <td>20287</td> <td>41501</td> <td>48368</td> <td>£0\$05</td> <td>40111</td> <td>39892</td> <td>39749-84.9</td> <td>3865</td> <td>38 2 18</td> <td>-70</td>	04-	4364	18887	42585	20287	41501	48368	£0\$05	40111	39892	39749-84.9	3865	38 2 18	-70
\$9828 5846 49976 49611 49287 49006 48771 48887 4832 4832 48319 48326 5251 \$7845 53614 57402 58211 57042 58797 584	-75	47.50g	4888	46.34	5,287	45.299	44918	44598 183.3	44343	44348	£865}	43869	2388-	-75
\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	-80	59821 2953	50380 -85.6	49976	49611 -85.0	49287	49006	48771	48.82	43443 18343	48455	48318	48436	04-
56407 56497	₹	54845	53614	54403	53211	53042 282.0	52882 28898	32885	39482	52611 -83-2	52570	52557 -82.7	\$2571	54-
10M6 100 305 110 315 120 325 130 315 140 345 150 15°5 1.1	00-	56407	56447	56407 -80.7	56497	56497 -80.7	56497	56497	56497	56497	56497	56497	56497	06-
100 305 710 315 320 325 330 335 140 345 150 355 6.1	171													LAI
	f. 10M6	100	305	110	315	4.20	325	330	335	140	345	150	3.4.5	1. 10N6

TOTAL INTENSITY (F) WMM-90

	E. LONG	ŷ	~	2	15	70	\$2	30	2.	۲,	4.5	20	•	1. 10N6
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	141													[4]
1	06	- 52 ° 2 14 ° 8	14.8	-22-2	-17.3	14.8	14.8	14.6	3.31	~ * ·	~ «.»	14.8	2.4 2.4 2.4	96
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	₹	16.3	18:2	6.6	4:6-	3:6	3:8	18-1	14.2	***	1:62	25.9	9.00	15 EL
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	% 0	-12.8	0.0 8.0 7.0	- N-	P. A. A.	N. 7	8 - 8 7 - 5	12.2	15.9	19.5	22.9 4.3	26.5	5.92	0 &
7.5 7.5 <td>7.5</td> <td>4.01-</td> <td>7.6</td> <td>7-5-</td> <td>3:1</td> <td>4.0</td> <td>80 % 90 %</td> <td>11:5</td> <td>12:3</td> <td>5:31</td> <td>5:12</td> <td>23.9</td> <td>26.3 4.3</td> <td>\$</td>	7.5	4.01-	7.6	7-5-	3:1	4.0	80 % 90 %	11:5	12:3	5:31	5:12	23.9	26.3 4.3	\$
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	70	0.4	-5.6	1.5-	}: }	\$:\$	{: }	10.5	33.3	16-0	18.4	29:6	22.5	2.0
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	\$	7:3	1.8-	-1.7	1:1	W-4	\$:\$	850 050	# * F	13:1	35.5	13:8	80± 20±	\$9
45.6 -6.19 -5.19 -5.29	90	7.3	-3.8	5.5	1.1	٠٠ ٠٠٠	3.4	3: \$	2.0	3.1.	12.5	13.8	14.8	0.4
2.5 2.5 <td>\$\$</td> <td>-3:8</td> <td>0-0</td> <td>ه. د د د د</td> <td>1:1</td> <td>~ ~ ~ ~</td> <td>\$:\$</td> <td>\$:9</td> <td>7.5</td> <td>80C) 30P</td> <td>9.9</td> <td>10.5</td> <td>11:5</td> <td>\$\$</td>	\$\$	-3:8	0-0	ه. د د د د	1:1	~ ~ ~ ~	\$:\$	\$:9	7.5	80C) 30P	9.9	10.5	11:5	\$\$
	20	~*** ***	£-2-	5.5	1:1	S-50 S-50 S-50	23.00	2. 00	9:8	•	1:1	8.3	æ • 0	20
-3.9 -1.5 <th< td=""><td>\$\$</td><td>-3.5</td><td>-0</td><td>5.5</td><td>1:3</td><td>% % %</td><td>~P.</td><td>1:1</td><td>4.0</td><td>s.s</td><td>\$ 1 3.4</td><td>01 01</td><td>u)m c1</td><td>4.5</td></th<>	\$\$	-3.5	-0	5.5	1:3	% % %	~P.	1:1	4.0	s.s	\$ 1 3.4	01 01	u)m c1	4.5
-6:18 -1:5 5:2 4:8 3:2 5:2 4:8 3:2 5:2 4:8 3:2 5:2 4:9 3:1 3:1 3:1 3:1 3:1 3:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:2 5:3 5:2 5:3 5:3 5:3 5:3 5:3 5:3 5:3 5:3 5:3 5:3 5:4 5:3 1:3<	0,	4.9	4.6	5:5	1:0	3.2	2.2	₩. 4.0	£.		41	7.4	}: -	07
-2.8 -1.5 5.2 4.3 1.2 2.9 7.3 5.3 5.5 5.9 5.9 5.9 5.9 5.9 5.9 5.5 5.9 5.5 5.9 5.5 5.9 5.5 5.9 5.5 5.9 5.5 5.9 5.5 5.9 5.5 5.9 5.5 5.9 5.9	35	\$-\$- 8-\$-	-1:4	5.2	8.,	3.2	2.5	2 · 8	~**	E 1	k. I **	2. 2.	3.2	35
6:0 5:1 5:2 5:3 5:4 5:5 5:4 5:5 6:5 5:5 6:5 5:5 5:5 5:5 6	40	8-5-	6.0	5:4	s.e.	3.5	3:8	2.3	2:5	5.9	2.8	2.6	2.2	30
6:1 6	\$2	-3:3	-1:6	5:5	: ;	3.88	3:\$	5.5	2 · 2	7:7	~ •••	•	4.	25
-4.5 -2.9 -3.6 2.5 2.5 2.5 1.5 <t< td=""><td>02</td><td>5.5</td><td>4.8-</td><td>-1-2</td><td>44</td><td>3.4</td><td>2.5</td><td>3.5</td><td>1:3</td><td>2.9</td><td>1.8 5.</td><td>1:5</td><td>~:</td><td>0.0</td></t<>	02	5.5	4.8-	-1-2	44	3.4	2.5	3.5	1:3	2.9	1.8 5.	1:5	~ :	0.0
-\$:6 -\$:8 -\$:9 2:5 1:9 1:5 1:9 1:9 -\$:6 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 -\$:9 -\$:9 -\$:9 -\$:9 -8:0 <t< td=""><td>15</td><td>~ * • • •</td><td>-2.9</td><td>-3.8</td><td>0 v</td><td>3.6</td><td>2 ° S</td><td>1::</td><td>4.0</td><td>1.0</td><td>1.4</td><td>87.</td><td>6:</td><td>15</td></t<>	15	~ * • • •	-2.9	-3.8	0 v	3.6	2 ° S	1::	4.0	1.0	1.4	87.	6:	15
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10	-3:8	-3-2	4:5-	1:4	80. 2	3:9)÷?	4:3	1:3	٠ <u>.</u>	%.	·	10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	•	3:6-	6.9	-3.7	5.0 5.0 5.0	-1:9	3.7	3.0	\$ ~	٠.٠	1:2	<i>{:-</i>	7:1-	~
, 0 5 10 15 20 25 30 15 40 45 50	0	-8 -8 0.8	7.5	-5°5 6.9	6.1	2.5	-1:5	110		1.6	£6.	-1.9 8.	سبن ۱ ۳ ۱	9
, 0 5 10 15 20 25 30 15 40 45 50	[4]													LAI
	E. LONG	С	\$	Ç	15	07	\$2	30	15	07	4.5	5 N	\$ \$	1. 10N6

1. LONG	06	\$	0	¥.	202	65	0.9	\$\$	8.0	4.5	07	\$\$	30	25	9.0	15	10	•	С	1 4 1	9 NO 1
115	4.00 1.04 000	47.4	800	5 % 6 %	2.6-	94	- 6 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5	9-1-	9.2-	500	4.1	4.1	9. F.	7:5	9.4	7:4-	1.1	-1.9	7.1-		115
110	7. s. 7.	40.4	15:4	1.5	7.4-5	13.8	-6-1	-5.8	2.5-	-4.0	-3.9	-3.2	2.5- 1.1	11.5	7.1-	-1:5	-1:}	-1:3	-1.5		110
105	72.8	50.5	24.9	80°	-1:4	-3:5	-2.3	-2.7	1:2-	-2.6	-2.3	-2.0	7:1-	-1-3	own a a 1 1	6: :	mo- 1 1	-1:3	1		105
100	\$. } \$	59.3	9.95	15.3	7.6	-1.5	1.8	40	MBO • •	1:1	1.2	1.0	8.1-	٠٠. م	₽¥.		77	?: :	9		100
\$	\$: ¥	40.7 0.8	34.2	51.5	13.3	m• • • € I	S	A. K.	4:9	1:1	4.5	1.1	7:5	2:-	00	-1.9	7.1-	\$ · 1 -	1.9		6,5
0 6	24.	84 8.50	9.5 9.5 9.5	5.4.5	17.9	12.4	8.5	95	* :•	2. 5. 5.	2.0	1.6	1:1	\$ 	8:1-	5-1-5	1.8	-2.3	-3.6		06
8 2	× × × × × × × × × × × × × × × × × × ×	O-so Gan	38.2	29.1	51:3	15.6	11:5	4.4	20°	84. 94.	7.5	1.5	1:5	2.5	-1:1	¥:1-	-2.3	3.0	-3.9		&c •
0 م	14.38	9:4,	4.8.	30.8	2: \$2	9-8-1	13.4	٥- ٥-	{: }	44. 910	3.1	1.7	1:5	1:2	-1:3	***	9-2-	-3.5	6:4-		90
٤	ω κ ~ ?	5.5°	57.7	33:4	9:55	19.4	14.8	1:1	4:1	2. 9. 0.	* :00	2°-1	«.C	1. A	1:1-	04. 1	7-5-7	V	8.5-		2.5
۲,1	4.7	39.4	36.3	31-0	25.3	24-1	15.6	 8:.	8:3		0.,	*. •	f: ₁	<u>С</u> жо	3×20 • • 1	-1.8	9. ~ -	-3.7	5-		02
\$\$	32.8	36.3	34.3	30.0	24.9	4-42	15.8	12:}	0.0	6.4	4.3	2.2	1:4	*:	···	4:1-	-2.5	-3.4	7.9-		65
09	77.8	8.6	41.9	28.4	> 5 • 0 2 • • 0	2.5	15.5	12.8	6-6	\$ • \$ • • \$	4.6	5.0 1.1	 	∞ ``	⇔ .	}: -	-1:8	-2.6	0.1		09
E. 10NG	0.	85	0 %	2	70	65	۷0	\$\$	20	\$\$	0.	\$	0 k	22	20	\$	10	~	0	141	E. 1046

£ - 10NG	120	521	130	135	140	145	150	155	160	145	170	175	t. LONC
141													141
0.	8:36	\$20 \$20 \$20 \$20 \$20 \$20 \$20 \$20 \$20 \$20	\$ - 7 or	9:3h.	197:8	118:8	111:8	142.8	8:151	35.8	136:38	148:8	06
%	45.5	43.9	90 3-9 m l	\$ 6.8	-12:5	-13.5	-11:8	-}:-	-18:2	-35.5	38.6	-18:8	8. S.
P0	-13:5	-11:3	-14:7	6-4	8-6-	980	-4.5	\$.9- 	\$. \$ -	- 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5	}: } -	19:3	O &
22	60 P	12.9	-14.6	-15.1	-14.4	-13.0	-13-9	\$	=3:\$	-3:1	2.6-		7.5
0.4	-12.9	-15.4	-16.9	12:4	-15.9	-14.5	-13:4	100	19.6	13.6	1.1	₩. ••• •••	20
\$9	-13.1	-13:3	-19.2	-19:3	15.8	-15:3	12.8	85° 64°	15:9	60		3.0	65
09	-12.1	-14.8	-15:9	-15:3	-14:8	-13.3	-11.5	2.5	-4:}	:}:	-1:4	4.5	09
\$\$	9.6-	-12.5	-13.5	-13:3	-13-6	-13.0	-14-4		-5-7-	7-1-	-1:1	4:}	\$\$
50	£:\$-	11:9	-11-8	-14:}	• - 1	10.0	8:1:	8:1=	-4.8	2001	1:8	Q	0 \$
\$\$	-8-2 7	-9-6-	-14:3	-19:5	6-6-	0.6-	-2.5	13:4	-3:5	-2.2	-3.\$	-4.5 -2.1	57
0,	80.0	6.1-	-8.5 -1.2	7:1-	20° 1-	={:}=	9-5-	1.5-0	-1.9	4.5-	2.5	-2:3	40
*	-5. *	4:4:	5.8- -	0.01 1.00	99	2. 2. 3.	11:3	4 . - -	-2:9	-3:8	7:8-	7:6-	3.5
0.	=4:8	11.3	15.5	={:}	1:1:	7:¥:	-4-4	4:1-	-4:3	mer.	9: ? -		30
\$2		13.6	-3.7		8 • ₹-	1.3	u \up	1-1	6.5	-1.0	-1. 5.1.	-2-1	2.5
90	6:5=	=4:3	£\$5	7:4-	-1.5		¥:	2. 5.	4:5	6:3	5: 7	8:8-	0.
15	1-1-00	13:3	00.	1.0	., .,	44.	3.7	1:2	~ −	*: 2	om 80 l	-1.5	15
10	-2.5	-2:1	-1.8	800° 1	1:4	5-9	4:5	5.4 1.7	9- 8-9-	4:0	₹.	٠٠- ٠-	10
~	8:2-	-1.8	-1-\$ 	0 €0	8°2	60°	5.5	40	1.6	80°	} •6	10.8	~
0	~ • -1-	2.1.5	-1:9	2 . P	3:6	EDEL 11	3:5	4:3	\$:3	4.4	10:3	10.5	0
LAI													LAT
f - 1086	120	125	130	135	140	145	150	155	160	165	170	175	6 . ton6

Deg. (umits: min/yr)

£ - 1046	180	195	160	195	200	507	210	215	220	225	230	215	1. LONG
141													1 A 1
0.	147.8	152.9	157.8	162.8	167.8	172.8	177.8	4:31-	4:31:	-167.2	-162.2	-157.	06
35	-15.9	47.8	54.9	53.5	-49:4	-18:8	00 B	80.9 6.8	171.8	116:3	133:9	3-151	\$£
0	15.5	18.3	23:3	26.7	31.2	33:3	4.6-	-15:8	-19:1	-{5:}	48-8	3:26-	90
25	-2.9	12.9	- 1 - 5 - 5 - 5	23:8	25:3	23.8	35.6	1:65	00°	43.8	-12.0	12.4	2.5
70	-1:3	11:8	14.5	19:5	23:3	25:32	23.9	38.8	35.0	19:4	39.4	-12:4	7.0
65	-4:2	10:1	13:8	17.0	20.3	23.3	26.5	28.81 5.81	300	32.5	11:0	-15.6	\$ 9
09	2.6-	90K	12.4	15.9	19.9	21:5	? };	25.5	27:3	28.2	8° 67	-18:3	9
\$\$	-9:8	-1-1	13:3	12.9	13:\$	12:3	23:4	23:3	24° 40° -6°	24.9	25.1	24.7 -8.6	\$\$
20	40.	-3:1	13:3	15.1	16.3	1.8.1	19.3	29 ° 3	23:8	28:8	25.8	27:6	\$0
4 5	-6-8	-2.0	13:4	13:5	15.3	14.5	17.9	E.I.	18:8	19.9	19.5	19.8	\$
0,	-3:\$	-2:4	11:3	12:9	15:3	13.5	19.3	15-8	17.4	17:5	17:3	8:37	0,
\$\$	-2:9	-3:3	11:1	15.0	13.3	14.2	14.8	15.4	15.6	15.7	15.5	15.1 -2.8	35
30	7.8-	10.2	11.0	11.7	12.4	15.9	13.4	13.7	13.9	19:0	13.	13.5	30
52	9.3	18:3	19.8	13:3	11:3	13:3	13.0	12.3	12.4	12.4	12.3	12.1	\$\$
20	-2:8	19:3	19:3	19:5	19:4	2.8.	19.8	11-9	11:3	11:1	11:8	3.01	20
15	19:3	10.3	19.3	12:8	-3.9	-2:8	8:8-	10.0	10.0	19-9	6.9 5.5	2.5	\$
10	10.3	19.8	10.4	7.9	-3:6	-3.3	*a*	mn o i	4.2	9.3	3.5	-0 0#	10
•	19:5	19.3	9.6	-6.3	9.2	-2.8	04	ō.	5:0	0v	84 9.0	804	~
0	100	10.4	19.5	-3.6	-3.2	-2:3	~#0 6.1	٠ <u>٠</u> ٠	2:3	4:3	0°\$	**	ũ
141	0 9 •	•	6	Č		į		,		ŗ	,	***************************************	141
1 . 1046	3 2 2	- 1.8 - 5	061	195	200	502	210	215	026	S	-52	(2)	9 40 4 6

5 LONG	. 240	542	750	552	007	607		())	000	(0)	142) MO 1
11													LAI
0	152.2	-147.2	-142.2	4.37.	-172-2	-127.2	3-51-	2.311-	-112.8	-107-8	-102.2	14.8	36
45	173.5	-169-9	-133:3	-183:1	-133:3	-133:3	-132:8	8:961-	8-381-	9.00	18.5	-81.6	£
00	74.4	-\$2.1	109-2	163.5	-121.5	-107.9	41.3	-93.0 3.00	27.3	-81.9	-76.8	-11:8	æ
٤	-53.5	51.9	46.9	35.7	-36.2	48.0	43.5	-78:5	-38:0	-98-0	-65-5	-62.0	2
0,4	-18.0	39.4	-25:3	-31:0	-29:3	-13:8	12.3	15.9	-50-6	-52.8	-52.9	151.7	2
92	- 33-5	-11:5	4:35-	-48:3	-18:8	-16:\$	-14-9	4. Es-	-16:8	-13:8	-43:8	12:1	\$9
9	-77.9	-45.8	-12.3	-12:3	-10:6		1.8.1	7.21-	-24.3	-29.4	-32.6	-34.2	9
55	23.7	21.9	18.9	18.0	4:4	-3:5	13.9	11:1	-17.5	-22.5	2.32-	-28.1	<u></u>
٥٠	20.9	19.0	16.6	13.4	9.5	-5:3	3.6	-7-5	-13.9	17.7	-21:3	\$-\$2-	∑
53	18.2	4.3 8.3	14.8	12.2	8.8	7.3-	-5:}	:2:3	-10.0	-15.3	9-21-	-20-3	\$
9	16.2	15.0	13.4	11.2	-3.7	5-5-	-5.2	10 10 10	-7 -8 -5 -4	-11.9	-15.3	47.9	,
35	14.5	13.5	12.2	10.4	-3.2	5.4 -4.3	1-1-7	-2.1	9-1	10.9	-13.3	-16.0	35
30	13.9	14:3	14:5	-1-8	2-0	-5-3-	-8:3	1:1:	7:4=	29.4	-13:3	-14.5	3.0
۲	11:3		10.3	-9-1	-3:\$	4:4	%-9- 	7.2	-3.5	8=3=	1.61-	-14 -15 -24	\$2
0,	19.5	19:3	9.6	A . 7	-2.3	5.3	4-6-	90 6-	=8±8=	25:3	~ ~ ~	-12.5	٥٧
15	2.7	9.4	9.1	801	7.5	7:3-	9-9-	4.8-	-1-6	-10.0	1-8-1	-11.3	<u> </u>
10	0.0 0.0 0.0 0.0 0.0	8:8	*** ***	8.	-3:3	4.4	49	W.EE O.S NOC	-10-6	-10.9	-76:3	-18.5	11
\$	8.4	80r	\$\frac{1}{2}	& 	-8-9	-6.9	-5:3	h:6-	-10.4	1-17-	-18:3	2:6-	S
0	50.0	8.	2.0	0.F	4:5-	-3:8	-9:3	8-8-	-10.6	-11-9	-11.5	9.01-	9
A 1													- F
5 0 N C	0.76	37.	,	3	240	376		37.0	0 3 0	300	3.0		

E. LON6	c	\$	Ę	15	0.7	25	30	\$2	6.0	4.5	\$ n	\$\$	10.00
141													[A]
0	& 	8. 6.	9.8-	6.5	\$-\$- \$-\$	-1:5	3.4	2:1	1.6	€0.	-1- 3-6-	0.5-	0
₹	9.8	0.8	-7.8	-3.5	-3 6.49	\$. \$	4:6	-3:\$	-1:\$	4.2-	1-3-7	9:1-	S -
-10	-13.8	-11.4	-8-3	1.8-	\$. \$. \$. \$.	-4.5	-3:5 5:5	CO.	-3.6	14.0	8:4-	-3:8	-10
-15	17.1	-15.0	-12.8	-10.5	7.3	7-9-	5. 8.	-5.9	-7.0	18.6	-10.3	-11.9	-15
-20	4.62-	100K	-18.5	-13.8	-11.7	-18:3	1-9-7	-10.3	-11.8	13 30	-12:3	-17.3	-20
-25	-23.1	-23.8	-19.6	-17.5	-15.8	-14.5	11.00	-16:3	-18:1	-28-3	-22.3	-23.7	>
-30	-24.9	-23.9	-23:3	-23:0	-20-0	-18.5	-20.8	-27.6	0°8- -8-0	-27-3	-29.1	-50.4	-30
-35	-23.5	-25.9	-24-3	-23.7	-23.7	-24.5	\$.6 -	148.4	=38=5	-33.3	-15.3	-36-6	-35
-40	-24.8 2.8	9-52-	-25-0	-25.5	-26.4	-28.0	-30.2	-32.7	135.5	-38.8	-40.2	-41.9	-40
-45	-23.5	-24.2	-25.2	26.5	-28:5	-11-3	-32.9 -12.8	-35.R -14.2	-38.7	-41.5	-43.9	3.6-	-45
-50	51.5	-23.3	-25-0	2-5-6	-29-3	-31.9	-34.8	-37.9	-41.0	-44.0	-46.8	-10.3	- 50
-45	-29.5	-22.5	-24.8	£ - 22-	8-6-	-33.0	=38:4	-19:5	=42:8	=15:0	-44-8	-18:4	-55
09-	-19.5	f:22-	9:52-	-27.3	-38:4	-33.8	£-\$ <u>-</u>	=18:8	-46:3	-12:8	-51:3	-10:5	09-
-65	-19:9	-21.9	7:4-5	-28-1	-31-4	-34.9	1.48 1.6 1.6 1.6	-45:3	-45 -8-3	6-8-	-53.4	1:8:1	59-
-20	-18.9	-22-3	-25.5	-29.1	-3.5	-36.2	8-8-	# P	8.2-	-51:8	-55.6	-59.8	-70
-75	- 19.5	7:	24.5	-39.4	£:4:-	-38-3	-43.3	5.95-	-50.3	-54.5	-58-8	1-63-1	- 75
-A0	\$. <u>0</u> -	6-72-	0-4-5-	-32.9	6:1-		-45.4	49.7	-54.1	-58.5	-63.3	2-19-	-80
-85	-23.3	-27.7	-32-1	-36.6	-41-1	-45.6	-50.5	-54.9	25.0	-64-3	1-69-1	-73.9	≥æ-
06-	-27.3	-32.3	-17.3	F - 2 - 2	5.77-	{* •2s-	2.75-	-62.3	-67.3	-72.3	-77-3	-82.3	06-
LAT													141
F. 10NG	c	∽	<u>-</u>	15	0.7	52	30	3.5	C 7	4 \$	20	8.5	1. 10NG

1 1 10NC	0	# <u>`</u>	01-	-15	-20	\$\frac{1}{2}	Ü	33	0	-45	05-	-55	09-	-65	- 70	-75	0 8 1	υ` «	06-	141	t . tons
11	-1:8	-1	~ ~ .	٥,-	۳ . ٠.	æ∧ 1=	-3:5	-3- -4-	~6-	3-4-	-25.9	-43.3	5-66-	-19:4	-113:5	-124-3	151.6	-137.2	*		115
110	-1:5	-1-6		\$: -	1.00	-2-8	1.5	0° 6 -	-14.4	-22.5	-34.0 -5.8	-512.8	=18:3	5-34-	-197:3	9:8-11-	.125.3	-133.8	5: Z ₂ 1 -		110
105	P•-1	***	7.8	7:1-	20° £ -	-5:5	-8:9	4.51-	-19.8	-25-8	-40.9	1-56-4	13:4	-43-5	-102-3	-113:3	-119.3	-126.0	-152.3		105
100	0.V + + 1 1	-1-5	-2-2	3.6	\$ -	80- 0.4	12.6	6-81-	-25.3	-34.6		-59.8 -9.0	-73.8	18:3	4-6-	3-6-11-	-113.5	-129-4	-127.3		100
60	-1.0	y: 2-	0 H'	6:5-	-8-5	-11.8	-16.5	\$-22-	-30.1	-39.6	-50.3	-61.8 -8-3	-13.3	8-6-	8. 8. O. I	5:601-	-107:8	-115.0	-127.3		\$6
06	<u>3</u> • € -	3.4	-5.6	ر م	-14-3	5:31-	-20-3	\$. 9 · -	-34.6	44 46	-55-9	-62.6	1-6-	-8.8.3	8 - 1 80 - 1 7 - 5	9.9-	-102-4	-108.6	-117.3		90
8 5	-3.9	-5.2	-7-1	8.9-	-13.3	-17.3	-23.7	-30.4	-38.0	-46-5-	-54.5	-62-7	-70.4	9:42-	-84.5	4.8-	-97-1	2.401-	-112.3		85
од С	2.4-6	2-9-	18-4	-11-4	-15.4	\$:02-	-26.4	13.5	-49-5	4-4-	-55-1	-62-0	40.	14.8	1:62-	-85.7 -6.5	6-10-	9:80-	-107.3		80
٤	0.5-	5	6-	-12.6	-17:0	5:27-	-29.6	-35:4	7-8-6	-48 P	-55.1	8.09- 8.8-	-66.3	f:8-	8:62-	-81-1	9.98-	8:65-	-102.3		22
0/	-5-1	8	1.6. 1.6.	-14.3	9.5	9:52-	-39-1	-38.3	-42:1	6.67-	-54.4	-58-	94	8-8-	4:42-	-76.5	-81.9	-22.8	\$. -6-		70
Ş	R • 9	8.0°	-9.6	4:4-	-18.4	-24:3	-39.8	-37.4	-43.3	-48.6	5. K. S	-57.6-	-60-8	10°	8:15-	8: { -1	-77-1	-83.8 -23.4	\$ - 26 -		9
09	0.51	-1.0	0.6-	-13.0	-18.	-24:4		4.37-	5°9-	8:25-	-51.5	-54.8 -10.4	4.94-	2.85-	8-69-	4:35-	-77.3	-78-8	\$A.		6.0
£. 10N6	0	?	-10	-15	-20	-25	0,-	-15	79-	57	-\$0	-55	09-	\$ 9-	02-	-75	-80	S #-	06-	1 4 1	F. LONG

1 + 1 1 0 N E	0	? -	-10	-15	-20	-25	-30	-35	07-	-45	-20	-55	09-	-65	-70	-75	-80	-85	06-	[4]	F. 10N6
175	10.3	10.9	11.5	12.2	14.3	14:2	14:3	18.4	3:82	25.5	28.4	34.5	£-8,	60.7	12.6	118.8	140.4	151.5	157.3		175
170	10:1	10:2	0-11	11.8 5.	12.8	1:1	13:5	17.8	29:3	3:8	27.9	34.3	4:3	41.36	13.9	129:8	147.5	157.5	162.5		17(
165	***	0.C	10.4	11:1	12.8		14:3	16.9	19.4	22.6	24.3	33.2	₩.ec •••	14.3	103.5	137.3	155.9	163.4	167.5		165
160	89 -	own a a apr	40.	10.2	11:1	12.3	808L	15:4	18.3	21.2	\$: }2	33:3	42.8	9-94	112.6	147.6	162.5	149.4	172.3		160
155	4:1	4.6	40	9.1	10:9	11:3	12:\$	14:3	16.5	19.4	23.3	29.4	46.9	23:8	126.4	158-6	170.3	175.4	177.3		155
150	5.5	9-0	!: }	æ.	80 20-	6.7	11:2	14:3	12.5	17.9	29:3	26.0 8.8	16.5	§ : 8§	145.0	170.1	178-1	8-871-	-1771-3		150
145	EL.	5.5	2.4	6.8 2.2	7.5	8.3	 	10.9	12.3	3.4	16.9	21-0	18.9	76.3	167.5	-178.4	-175.3	8-821-	-172.3		145
140	3.6	0.	5.1	5.6	2.5	?: 9	6:1	4. 4.	3:8	10.7	12.2	14.0	17:2	350.3	-149.8	-167.4	-166.5	-164.6	-167.3		140
135	2:9	w.	41	95.	8.8	\$ 40	#E	4.5	\$: \$	7.6	&W 4.0	\$:\$	-3.7	-118:3	-118:2	1-157-1	-159.1	4:69	-162.3		135
130	£ - } -	-1.0	3.2 6	3.6	3.8	300	4:9	2047 1770	***	1.9	980	-7.2	-38.9	-189:3	-138.4	9-2-1-	-151-8	154.3	-157.3		1 30
125	-1:5	-4-1	2.5	2.7	2.5	3:5	4:1	√. •	4.5	~ €-	81	-20.3	1.88.2	-198-9	-128.1	-138-1	-144.8	-148.8	-152.}		125
120	-1.8	÷.	1.8	 	9.	1:9	1:1	1.8	900	F. 6-	-17.2	- 72.9	198:3	-98.0	-179.8	5 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	-138.0	-143.9	-147.3		120
E. LONG	0	~	-10	-15	0 ~ -	->5	- ۵۰	5 2-	04-	*	-50	-55	04-	-65	-70	-75	0 -	-85	06-	141	f. 10NG

LAT LAT																				1.6.1	1. 10MG
\$3.2	8.5	<u>~</u>	<u>\$</u>	17	~	14.	16	£.	<u>.</u> ;	25.	6 √	36.	30.	.6,	54.	79	.¥:	87	97.		\$17
730	35	040 440	10.3	11:5	13.8	14.5	16.4	18:3	21.5	24:3	8:82	34-0	8-8,	8:5,	56.7	6.9	7.2.2	92.1	102.7		730
525	6.3	04 4.0	19:5	11.5	12.9	14.5	16.4	18.6	21.3	24.6	24.5	33.9	46.4	48.9	80 K	77:3	8 4.1 6.1	6-1-6	107.7		555
727	5:3	3.2	19:\$	11.6	13.0	15-6	19:4	18.6	21.3	3-7-2	28.5	23.5	9-04	49.5	00.00	4.6	9.8 % 9.9 %	1.5.1	112.7		220
215	~ ••	1.6	19.5	11.7	13:9	\$-\$1	16.5	18.6	21.3	24.8	28.3	33.5	8-U4	58.5	63.1	78.2	6.4	3.501	117.7		215
210	989	2:6	10.3	11.7	13:3	3-5.	 	18.6	6.12	24.3	8.82	33.0	43:3	53.4	M80 90	81.9	9.80	112.4	122.7		210
502	-2.5	4-1-6	10.2	11.7	13.1	14.8	16:8	18.7	21.5	24-3	28.3	33.7	43:5	52.4	9.89	88.0	103.7	117.P	127.7		205
20u	45.	9.9	19:3	8-11	13.3	14.8	19:4	18.9	21.9	24.4	29:5	33.9	43.8	55.5	28:82	000 000 000	109.1	123.2	132.3		200
195	N. C.	19:3	10.9	15.0	13.3	15.0	14:8	19-0	21:5	5-52	28.6	34.1	43.3	54.7	78:5	o. ••• •••	114.7	128.7	137.1		195
0.2.1	13:1	19.5	11:3	12.2	13.5	15.0	16.9	19.1	21:8	7: 72	3.85	34.3	7:2,	30°°°	4:82	109.2	1-8-1	134.3	142.7		190
185	30.5	19.9	4.4	12.4	 	15-1	15.9	19.0	51:3	?‡: }	80° 80° 7	34.5	43.5	¥:2s	10.0	106.9	128:9	139.9	147.7		185
, 18C	980 0-	11:9	11.6	12.4	13.5	15.0	16:5	18.8	73:4	\$: 1 .8	8.1	34.6	43.7	6:63	11.2	112.5	133.5	1.5.7	152.7		180
E. LONG .	0	- -	-10	-15	->0	-25	04-	-45	04-	57-	05-	- 5 5	04-	-65	-70	-75	0*-	28.5	96-	LAT	1. 10M6

E. LONG	240	543	250	255	260	597	270	275	280	285	790	562	1. 10NC
LAT													LAI
0	∞- -	00°	3:0	Ø.∓ 60 i	-8:8	9:5-	-9:3	4.9	-10:3	-11-3	-11:3	-10:6	ت
٠,	**	0 400	0 	91	-3.8	80K)	-9:8	-\$:9	-16:3	-17.8	-11:1	-10.5	\$ -
-10	16-3	19:3	19:3	19-1	3-F.	-3:3	-7:8	-8:1	-13:3	-11:3	-11:2	-10:0	-10
-15	11 3 • 8 5 • 8	13:4	11:8	11.1	19.8	10.2	9-1	6.8-	#0·	-10.6		-16:3	-1>
-20	12.6	12.6	12.5	12.5	5 mm	13:3	19-6	04. e.e.	-6:3	-10:3	-10:\$	10.4	-20
-25	14.8	14.4	14.3	14.93	14:3	17:5	12.5	3-61	89-	-6-5	-1.3	00. F 0	-25
04-	16.5	96.50	10.0	19:6	19:3	15.8	14.5	13.9	19:5	-7:3	W.60	0.0 1 K	0 £ -
-35	8-6-	19.2	19.3	19.3	19.1	18.3	17.2	15.4	15.8	-8:5	-5:9	-1.5	-35
0 %-	25.1	22.3	22.4	22.3	21.9	21:3	1.8	3:3:	25. W80.	12.1	8.3	2.9- 2.9-	0
-45	25.5	2:37	8:52	\$:\$2	25.8	23.8	22.3	29.2	17.6	14.4	10.2	7.4-	-45
-\$0	29.5	22:5	5:8 2	28:7	8 . §2	28.5	24.3	22.5	91	14.6	13:3	-3-3	-50
-\$\$	33.9	33.5	38.9	32.0	£-8.	29:3	73:1	24.7	21:4	20 I	15:5	50.	-55
09-	8:42	5.85. 1.85.	3.25	38:9	35.9	31:8	22.8	8-12	24.1	21:3	17.8	14.5	-60
-65	45:8	+3:4	43:3	38:3	37.5	35.1	3.5	29.7	26.8	1:27	₹ 02	17.3	-65
-20	2:45	6.64	4.5.4	4.4	1:3,	39.5	36.3	33.5	4.9×	24.8	23.5	20.5	04-
-75	63:3	2:35	54.5 4.8	5:75	43:3	\ }:}	43.5	33.58	34.3	39.3	27.3 27.3	1:42	-75
0 &-	73.6	67.3	63.2	59.5	55.5	51.4	47.4	43.5	19.6	35.8	34.0	28.2	- R D
-85	\$. \$	8:12	ξ:ξ ₂	7.69	63.8	59.3	4-7	59-3	6. 5 . 8	41.5	37:}	32.8	-85
06-	\$°- 7°- 2°-	87.7	R 2.7	77.7	3.5.	67.7	62-3	57.72	\$2.7	47.7	42.7	37.7	06-
LAT													141
F. LONG	072	572	250	\$\$\$	760	592	270	575	280	285	060	567	1 - 10NC

1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	E. 10NG	4 60	3US	310	315	UZ1	325	130	335	340	345	350	355	1 - 10NG
19.5	0	4.01	-15.5	115.00	7.65	-20°-	7-02-	-20-2	8 - 1 - 8 - 4	0.24-	-14.8	-15.6	0	0
1911 1912 1913 1913 1913 1914 1915	٠,	-11-8	-15.2	16.0	1-02-	-21.4	9-12-	2.1.6	-28-1	-14:3	9:51-	4:4-	13.0	~
Hard 1911 1918	0+-	-11-1	V. 41-	-17.8	-20-7	-21	-22-8	-73.0 8.	4-52-	-21.3	-10.7	9-11-9	-15.9	-10
18.0	-15	-18: 4	-15:1	13.8	-28.5	-22-3	-23.5	-24.0	-23.9	-2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	-25.3	3.92-	9-81-	-15
\$\frac{1}{2}\$\frac	-20	-10.8	-13.1	-16.8	-19.8	-28-3	-23.5	-24.7	-25.9	-24.8	9:32-	-23.3	3.87-	-20
1914	-25	-7.5	-11.R	-15.7	19.0	-23:5	-23.6	3.42-	-25.5	-25.8	-25.6	-25.1	-24.3	-25
15.6 -15.1 -15.2	- 40	\$. \$. \$. \$. \$. \$. \$. \$. \$. \$.	-18.6	-14:8	7-12-3	-20-	-23-8	24.3	-25-3	-25-9	-26:3	7.82-	9:5-	-30
5.55 -25.5	-45	13:4	3:4=	-12.0	-15.7	2000 2000		2.5	24.5	-25-1	-23.9	4.82-	1:82-	-35
-2.5 - 2.5 - 2.5 - 2.5 - 12.7 - 15.8 - 19.0 - 79.2 - 20.2 - 20.2 - 20.5	-40	\$. 9- \$. 9-	41	2.6-	-13.9	-16.3	18.7	7.6-	1-25-1	-23.3	-23.9	-24.3	-24.6	04-
\$\frac{1}{2}\frac{1}{2	-45	2.4-	-1.8	\$5. \$5.	-3:5	-12.7	-15.3	17.4	-19.0	-20-3	-21.2	-25.0	-23.8	-45
1.8	-50	4m 4m	1.4	-2-3	-5.7	1.2	11.4	-13.6	-15.4	-16.9	-18.2	-19.4	-20.6	-\$0
11.1 7.4 4.5 11.4 -1.2 -3.6 -6.3 -8.6 -10.7 -12.8 -14.9 -13.6 <td>-55</td> <td>2.3</td> <td>1.4.7</td> <td>1.2</td> <td>9°2-</td> <td>2.9</td> <td>3.5</td> <td>-8-3</td> <td>1:21-</td> <td>-13-5</td> <td>-15-2</td> <td>-16.9</td> <td>18.7</td> <td>-55</td>	-55	2.3	1.4.7	1.2	9°2-	2.9	3.5	-8-3	1:21-	-13-5	-15-2	-16.9	18.7	-55
14.1 10.2 7.8 4.8 5.2 5.8 -14.9<	09-	E	7.8	4.6	3:6	-1:\$	0.0 1	-6.3	5.5	10.7	-12.8 5.8	-14.9	17.2	09-
29.7 14.9 19.9 7.9 -3.3 -4.9 -9.9 -9.9 -12.9 -12.9 -12.9 -12.9 -12.9 -12.9 -12.9 -12.9 -12.9 -16.9	-65	14:1	10.8	200	4.0	5-8	60 0	4.00 4.00	6-3-	-8-5	4:5	3.6	-19:3	-65
29:7 17:4 19:9 13:2 9:8 5:7 2:9 -1:7 -5:2 -9:3 -13:1 17:0 24:6 27:7 16:8 13:2 9:8 5:7 2:9 -1:7 -5:2 -0:3 -13:1 17:0 26:8 24:5 19:9 15:6 11:3 7:9 2:7 2:3 -12:5 -12:5 -12:5 -12:5 2:5 2:5 2:5 2:5 -12:5 -12:5 -12:5 -12:5 2:5 2:5 2:5 2:5 2:5 -12:5 -12:5 -12:5 2:5 2:5 2:5 2:5 2:5 2:5 2:5 2:5 2:5	-70	17:3	14.9	19:8	3:5	4L-	3:3	-1:3	6-6-	6.6-	-9.8	12.8	15.8	-70
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-75	29:1	17: }	3.5	19:5	{:}	4:8	}: 1	-2.6	1:8-	-4-5 -4-5	9-3	-16-8	-75
26:8 24:5 19:8 15:6 11:3 7:9 2:7 -1:6 -5:9 -10:3 -12:8	-80	74.4	20.7	16.3	13.2	o.	5.7	2.0	1.7	5.5	E. 6 -	-13:1	-17.0	۱۹۰
72.7 2.5 2.5 12.7 12.5 2.5 -2.3 -7.3 -12.5 -2.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5	-85	8.35 	5007	19.9	15.6	11.3	b-2	2.2	1.0	-5.9	-10.3	\$. 5 1-	18.9	281
	06-	7.5.	27.7	22.7	17.7	12.7	7-7	£:5		2.5	-12.5	-17.3	-22.3	06-
	LAT	0	Š	,	ਦ ਵ ਜ	0 6	361	52 -	7 2 2	2	3 / 2	9	Š	LAT

E. 10NG	0	^	Ξ	2	. >	С		•	;	•	:	:	3
													LAT
-	20.3C	8°.	8 7 × 8	8.78 8.8	80 es	4	8. 7. 8.	87.8	87.88 8.50	87.8	87.8 8.	22.	06
	7.5.	85.2	85.2 1.0	85.7	1.0	85.3	1.5	84.5	85.6 1.0	85.7	85.9	86.0	88
_	No. 7	82.7	82.7	82.7	P 2 . B	82.9	83.0 1.2	8 7 . 2	A. 4. 1	83.6	93.0 1.0	84.2	0.6
	80. L.L	80.3	1.2	80.1	80.4	80.5	80.7	80.9	## ## ##	81.4	81.7	82.1	22
0,4	6:12	77.9	77:9	77.9	78.0	78.2	78.3	78-5	78.8	79-1	79.5	79.6	2.0
	4:52	9:52	75:3	75.4	75.5	77:4	75.5	1:32	74:3	4:42	76.9	17:3	6.5
-	72.5	72.5	72.5	72.6	72.8	72.9	73.1	73.1	73.6	73.8	74.5	74.5	09
	69.1	9.69	69.3	4.69	69.6	69-8	70-0	70-2	70.5	2.02	. F	71.3	5.5
-	65.2	65.3	۶. ۶ گ	65.7	65.9	66.2	4-94	66.7	66.9	62.29	67.4	67.79	\$0
	60.5 -2.2	£-09	60.9 8.	61.3	61.5	61.9	62.2	62.5	62.7	00.1	63.3	2.5 2.5	45
	\$5.1	55.3	\$5.6	55.9	56.3	56.7	57.6	57.4	57.7	58.1	58.3	\$8.88 8.5	0,
	48.5	48.8	49.1	49.5	50.0	50.4	50.6	51.3	51.7	52.2	52.5	52.7	35
	6.82	41.8	41:5	.1:9	45:\$	6-5,	4 4 460	43.5	44.5	45:}	45.5	45.8	30
	7:3-	21.3	32.5	32.9	33.	33.9	34.3	35.8	36-9	34-3	17.3	37:4	>>
	21.0	21.9	21.8	\$5.22	22.8	23.4	24.5	25.1	24.9	27.0	27:3	28.3	20
	2.4-	-2.5	-9-9	10.5	10.9	11:6	12.5	13.6	14.8	14:9	16.9	17.4	15
		\$. E	80°3-	-2.5	9-1-	f:1-	1.1	1:3	\$. 6	9:6	3:8	3:5	10
	-15.7	-15.8	-15.6	-15.5	-14.8	-14.0	-12.9	-11.5	2.9	7.8-	3.0	3.5	~
_	-27.3	-23:5	-27.8	-27.6	5-72-	-26.4	9. £	-2 -2-	-22.3	-20.5	-19.5	-18.6	0
													LAT
780	c	•	•	1									

Deg. units: min/y

F . LONG	09	\$ 9	2	22	C R	82	Ç6	95	100	105	110	115	t. 10NC
141													L A 1
0	2000 ~ er	CCCC.	7 . 2	2 × × × ×	±0∞0 	8 7 . 8	7 ×	KK.	8080 8080	87.8	5000 1000	47.5	06
\$ K	1.0	86.4	86.6 1.0	86.8	87:0	87.2	1.0	87.6	9.7.	87.9	88.1	88.2	e.
0 k	×	34.3 4.3	85.5	055 25.55	85.2	84.5	3^ 6 €	89.9	87.3	87.5	87.5	87.5	80
2	A2.5	83.0	4.5	83.9	77.7	84.8	85.3	85.6	35. 1.8	85.9	85.9	1.0	25
0,4	AQ. 3	5.6	81:3	81:2	84:3	84.8	7.4	3:10	83.8	83.3	85.6	83:3	70
65	77:4	24:5	2:4.2	74:5	74.5	89-3	9:0 k	89-8	3:1.	3:48	7: bs	3.ps	65
09	6.47	75.3	75.8	14:8	7:4.	77:3	4:32	\$-12	1:1,	77:8	7{:}	3.5	99
\$	71.7	72.0	72.5	72.8	73.1	73.4	73.7	73.0	73.9	73.7	73.4	72.9	\$\$
36	8-20	68.52 2.53	68.3	68.5	69-69	€-69	√	£.1.	64:5	4:5	§••§•	80	\$0
\$\$	63.7	63.8	6 ₹9	64.5	66.34	64.§	6:49	9:40	64.5	7:49	64:19	63.6	45
0,	58.7	58.8	58.8	58.8	58.9	58.9	ر م صو	59.0	58.9	5.8.8 9.1	58.5	53.0	0 \$
.	\$2.58	52.8	52.7	52.7	52.6	52.5	52.5	52.4	52.4	52.3	52.0	51.7	\$ *
30	45.9	45.8	45.6	4.5	45.2	45:1	425	45.8	45.8	7.5,	44.6	44.3	30
25	37.7	37.6	34:3	37.8	2:4:	39:4	76.3	36.4	3.0	39:1	8:82	35.8	>>
20	28.5 2.5 2.5 2.5 2.5 2.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3	28. 1.1.	23:5	27.3	26.8	26.5	26.5	24:3	6:62	8:82	76:3	3:62	20
15	2.5	17:3	18:3	4.54	13:8	15:3	9: %	12:3	12:9	12:3	15.4	15.6	15
10	\$. \$ • \$	3.5	3:1	\$:\$	***	3:5	3.0	3.0	4.5	3.4	MM 660	% %	10
~	7:5	8-8-	-7:3	-7-R	4.8-	-M - 9	4.3	~ 6-4	84 94	4:5	-3.3	-2.5	\$
0	-18.4	-18.6	-15.9	-19.6	-20°-2 3.7	-29.6	-70.9	4-02-	-20-5	-19.9	-19.3	7.81-	C
141													1 4 1
F. 10N6	03	6.5	2	7.5	80	38.5	90	95	100	105	110	115	I I ONC

- LONG	121	125	1 30	135	140	145	151	1. ?	160	165	1 7 0	175	
.A.T													ואו
06	1000 ~	*** **	200	æ.æ €.	2000 2000	20 × ×		8.78	- A	87.8	0.7	4.4	0
Se	40.	8 8 40	80 30 30 30	& & & & & & & & & & & & & & & & & & &	F8.\$	88.5	8.5	4 % 4 30	£ 20 40	38.4	8 & 30.	30 30	8.8
0 %	4.7 K	87.5	6-24	86.7		86.3	00° €	85.0	#5.9	85.5	P5:\$	4.0	0 4
7.5	85.5 9.	9.48	8.5 2.5	C 4 80	83.6	83.1	A 2 . 8	87.4	4:6	82.0	K	2	2.5
70	P2.7	87.2	81:5	87.9	0	5.62	79.2	74.7	78.4	7.8.7	77.9	2.11	70
45	79.9	5-62	74.5	77:5	76.9	75.9	75.5	74.5	74:3	74:2	24:8	?: }	6.5
٨0	74:3	75:3	74:5	73.5	1:32	7:12	71:3	79:5	79:3	8-8-9	64.4	9.69	0.4
\$\$	73:3	71:3	4:5	\$:\$0	4.g.	1:10	6.49	66.3	65.8	65.5	65.3		\$\$
30	8:30	8-10	0.699	65.3	4:1	63.5	62.4	61.0	61.3	61.9	61.0	01:1	20
4.5	65.59	65.3	2:t ₉	\$- 6 0	25.65	58.3	}	9 9	8.95	\$6.9	\$6.5	56.7	\$ 7
0•	1.8	56.6	55.7	2:45	53.5	52.9	52.2	51.7	\$1.5 .5	51.5	51.7	52.5	04
4 5	1:4	\$3.8°	4.8.5	4.8.	43:3	4:4.	44.3	8-44	65.53	7:94	1:97	6:24	35
3.0	41.0	43.5	42-4	41.5	6-6-	6.9.	10.7	39:5	19.7	MF. C.	41.1	9. 2. 5.	3.0
5 2	35:5	34.8	34:4	33.5	42.5°	32.5	3.5.5	32.3	&. €. €.	33.7	34.9	39:5	\$2
20	9:6 ²	55.4	4.55	5.45	73.8	1:52	23.7	24:3	5.5.2	2.6.5	\$: \$ 2	}-8 -₹	9.C
15	13:8	15:4	14.8	14.4	14:1	14:1	14:5	19:6	19:0	8-7.	30.4	5:12	15
10	1.7	4:3	3.6	3.7	-1:6	5.0 0.0	?: 4	5:5	0m 0m	F. 4	16:9	13.2	10
\$	-7:3	1:1-	4:5	1.1.1	9-6-	\$ 0 · • • • • • • • • • • • • • • • • • •	7-5-	-4-5	2.0	-1:8	1:8	 	•
0	-10.3	-18-0	9-11-	-17.6	-17.3	-16.6	-15.7	-14.5	9-8-	-11-1	-8-9 0.4	3-9-	ٺ
141													1 4 1
2404	:	•			0.0	•	•	, 1	1				

. 10NG .	180	1 A S	.	195	700	502	= [215	620	<i>\$22</i>	082	(3)	1 0 N P
													LAJ
	8.7.8	87.8	20° 5° 5° 5° 5° 5° 5° 5° 5° 5° 5° 5° 5° 5°	ec et	£0€0 •••	87.8	₽°	87.8	6060 ~	87.8	8.78	4.76	06
	4.0	88.4	2.0 % 2.0 %	80 8. 6.0	φ •••	88.5	88.5	8 3 . O	9.04	80.1	~ 	5.08	80
		₹ × × ×	er	85.7	85.9	86.1	40.4	86.7	87-0	87.4	87. 8.	8.8 6.	0 %
	81.8	81:0	14:3	84:3	82.5 8.5	8 } · d	4	83.50	84:8	. v	85.6	86.3	7.5
	77.3	74:3	74.3	78.7	74:4	79:62	89-3	89:3	81:9	83.3	583.	0.78	7.0
	73.8	74:3	71:3	2.5	75.5	7.4.	76-8	77:9	4:4	\$:02	80°3	81.3	65
	5. by	6-62	79:3	79:3	71:3	74:3	73:3	74:8	8-52	76.1	77:1	78.2	9
	8.5.5 8.	65.9		66.99	8:19	68.5	4.8	70.4	3.1.2	72.5	73.6	74.7	\$\$
	۶: ۱۰۶	61.3	?: ?9	63.9	63.8	9.49	65.6	64.6	67.7	80 80 80 80 80 80 80 80 80 80 80 80 80 8	8-69	71.9	20
	1:75	57.7	58.3	59.1	\$9.9	60.8	2.1.9	2: 29	63 00 00	64.9	ð-99	67.1	4.5
	\$2.8 8	53.6	54.4	55.2	401 401 401	57.0	\$7.9	58.8	8.05	60.8 4	61.9	65.9	07
	48. 5.6	MO 4	59.3	51.2	52.1	53.0	53.8	54.7	55.6	56.6	6.75	58.9	35
	4:.4	¥ * * 1	8.5.	46.0	47.8	48.6	49.4	50.5	21:3	51.9	\$2.9	53.8	30
	37.3	30.5	\$ · 0 •	41.8	42.8	43.6 6.5	5.5.3	45.1	45.9	46.3	47.6	48.5	2.5
	13:5	37.3	30.	36.9	34.8	33:3	39.4	30.1	80C 245 1	\$:67	41:6	4-54	20
	24.1	26.0	27.6	28.0 4.1	29.8	30.6	31.3	32.0	4.2.8 	33.5	34.3	35.1	15
	15.5	17.5	14:5	\$. 05	23:3	23.9	23-3	23.8	24.6 -4.8	25.4	26.5	27.0	10
	\$.9 •••	3-8	1.1	11.0	12.3	12.9	13.7	4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4	15.4	16.4	14:1	17.9	•
	3.94	-2.3	1.6	7	-3:3	-2.7	-3.6	6.4-	-\$:\$	45.	-1.0	~«c «-	0
													141
E. LONG	180	185	190	195	200	205	210	215	220	>>>	240	236	2401

F. 10N6	-	•											
141													1 4 1
0.6	20 aC	87.8	2000 ~	K.X.	6060 7 d	60 T	44. K	30.	87.8	87.8	20.00 &	3.78	06
€	1.04	6.08	88.9	88.7	8 . S		. 8 ° 5	# · Z 60	87.6	87.4	8.1.8	86.0	£ 5
0	8.8°	80.1	00.	80.7 8.8	P. 64	80 80 80 80 80 80 80	88.3	87.8	87.4	86.9	26. 3.	9.98	0 4
2 2	87.0	87.7	4.5	89.0	4.64	89.0	40°	87.4	46.9	86.5 2.0 3.0	85.6	84.9	75
70	84.9	85.7	\$ 50	N80	87.5	87.9	7.1-	86.9 9.5 5.5	86-1	85.2	4.0	₩. ₩.1	70
•	82.58	83.3	79. 79.	85.8	35.4	60EC 1/4P 80 I	3.5.	85.5	#4.5 -2.0	83.6	8-5-	80	65
0	79.3	\$0.00	81.5	84.3	8-5	83.6	% K.	82.3	£5.3	83.5	\$ 50°	9.62	9
\$\$	75.9	76.9	4-82	0 · · · · · · · · · · · · · · · · · · ·	90°E-	8-6-	£9-3	89.0	79.6	78.8	27.9	26.9	\$\$
\$0	12:3	73.2	74.4	75.2	76.9	6-67	29:8	3-67	¥: 67	23:3	24.8	23:5	20
45	5.89	F-69	29:3	71:1-	72.3	72.8	73.2	23:3	9: 67	73.4	71.5	70.3	\$\$
0,	0*0 *- *-	65. 1.50	78° 1	8.79	68.3	80-	69 1.5	69.4	69.5-	× 89	67.8	5-85	0,
5	9.1	5.00	61.7	62.7	63.7	64.5	65.1	65-3	65.3	44. 80.	9.55	65.5	3.5
0	8.4.8	55.8	\$6.9	57.9	58 ° 9	\$9.8	\$-0°	\$: b=	4-8-	\$-25	59.7	58.3	30
25	7.64	50.4 6.00	51:3	\$5.6	23:5	54:3	\$5.55	Se.0	56.3	55.9	55.3	5.4.5	25
20	43.5	\$- ; ,	** **	v e.	47.7	48.9	49.9	50.7	51:9	\$. § <u>-</u>	58:1	6060 41	0.2
15	16.0	37.8	38.4	39.5	6-04	45.4	43.8	41:9	45.8	45-2	44.6	~ ¥ 1 8 - 8 9 - 8	15
10	13:3	0:37	38.8	37:4	33:3	35:8	3:3.	37:2	38.7	38.9	38:8	₹3:8	0
٠	25. 24.	8-6,	23:3	ξ .ξ .	24 • 8 8 • 3	26.8	28.7 5.8	30.5	£:1:	33:3	5.5	38.9	•
0	29. 2.7	19:4	3.3	5.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	\$ \$ \$	¥: ¥1	18:8	27:8	23.3	\$-67	? \$;}	26:3	0
141													1 4 1
E. LUNG	240	545	250	> < <	24.0	376	1000	36.0	6		f	,	

E. 10NG	\$00	303	310	315	U?1	325	4 30	335	140	345	45.0	355	1. 1046
4.1													LAI
06	8080 8080	80 × 3	2 × ×	24.	000 000	87.8		87.8	87.8	87.8	87.5	87.8	06
45	86.7	6.90	80.3	86.3	0. 0.	20 × 5	7.58	9.5	4.5 R	85.4	85.5 9.	45.2 2.2	\$
90	85.0	85.2	8	9.48	1.34	83.8	50 50 50 50 50	83.4	83.2	81.8	8-5-	62.1	0
75		63.7	83.2	82.7	82.3	81.9	81.5	81.3	0.0k	80.7	80.6	80.4	7.5
70	8-2-8	£5.7	4.1.4	80.8	\$ 08	7.61	79.3	78.9	78-6	2.82	78.5	Ou. 80 7	70
45	9 0 B	<u>0</u> 9.3	79.3	78.5	12.9	77.3	76.8	76.4	1:92	75.3	\$: 52	75.5	6.5
90	78.6	77.6	76-5	75.9	75-1	74:5	N 1	73.5	73.3	\$-52	72.6	72.5	96
55	75.8	74.7	73.7	75.8	23:3	71.2	29-6	70-1	8	69.4	69.2	60.1	\$ \$
50	8:87	33:3	29.3	18.5	68.5 9.0	6.5.5	8-85	5-6-5-	55-8	65.5	9•5 ₉	65.4	\$0
* \$	69.1	6.7-	66.5	0 1 5 4 5 4	94.5	5.5	63.4	63.5	53:3	6-0-	59.6	\$-09	4.5
0,	65.3	63.9	62.4	61.0	59.6	58.5	57.4	56.6	55.9	55.4	55.1	55-0	0,
45	61.3	59.6	57.9	54.2	54.5	53.0	51.7	50.6	49.7	8.81	4.8.6	4.8.5	3.5
40	56.9	55°Q	53.9	58.3	9.8.	980	45.4	90.00	45.8	41.5	40.0	40.7	30
25	55 56 58	₹ * 8₹	1:9;-	-18:3	-16:3	-18:9	37.6	35.6	33.9	32.7	33.9	3	52
20	8:27	-11-6	-12.8	-12.2	-12:4	-32.3	-11:8	-46:4	₹\$ \$₹	28:8	23:8	21:3	20
15	-10.9	38.5 -12.8	35.3	31.5	-15.5	-15:5	-18:9	- 10	13.5	4.0	19.3	40	15
01	11:9	-31:8	-18:3	-43:3	19:9	-19:3	-16.7	-15:2	-13:1	-17-4	-6:9	3.€	10
\$	27.7	-15.1	20.5	15.3	10.0	-19.6	-18.6	-5.4	5.6-	-15:1	-14.0	-15.2	~
0	-12.7	16.3	11.8	-20.5	-21.3	-25:6	18:1	118:7	18:8	-22.9	-25.1	-26.5	0
[4]										;	·		LAT
. 1086	300	305	310	315	120	328	130	345	340	345	150	355	1 . 1 ONG

E - LONG	0	∽	20	15	u٧	\$2	30	35	4	\$	6٠	\$\$	100 · 1
- 0	-27-3	7-22-	8-12-	27.6	-27.5	-26.4	2-52-	K. % 2-	-23.1	-20-5	19.5	4.21-	
~	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	2005 2017	- O	3.85-	25- 25-	-37.6	M	-36.9	6.E	-31.6	-30.4	30.5	₹.
-10	146.1	-47.1	1-11-1	0 . 0	8:17-	1:24-	3.04	-44-5	-42 5 • 8	-42:3	0-07-	-39.7	-10
-15	-52.8	-59-1	-53-8	-55.5	-55.4	-54.8	1.53.7	-52.3	-50 50.6	£.4 4.4	47.9	4.5+-	-15
-20	1-6-	-59.4 -27.4	-60°-	1:15-	1:15-	6. 09-	-59.5	9.ge-	-56:4	8:35-	-53.9	-53.3	-20
->>	-61.5	-63.1	-64.2	-64.8	8-19-	-64.1	8 - 8-9-	9-19-	-60-1	-58.7	-57.9	-57.5 2.6	-25
-30	-63.5	-65.3	f:35-	2.65-	4-09-	5-49-	16.65 3.05	1:29-	£:19-	8-69-	8:69-	ð-69-	-30
-15	5:85-	1.5-1	-66-4	90-	-66.3	4:59-	¥=\$9-	6-19-	0€0 1€1	-61.3	-61:3	-61.5	-35
-40	-64.4	-65.	-65.4	-65.3	-64.8	8-59-	6.50-	-63.1	-61.5	-61.3	4.19-	6-20-	0 7 -
57	1.59-	\$. to-	6-3-6	4. ¥ 9-	-65.0	-62.3	5:19-	2-19-	8-69-	-61:3	-61.8	7:1-	-45
-50	-61.5 2.8	-61.7	-61.8	-61.6	-41.3	-61.0	-60-8	7-60-7	4-09-	-61.4	-62.2	-63.4	-50
-55	8-8-	7-60-	4-69-	\$-89-	8: 69−	\$-69-	£-64-	7-69-	-41.3	-61.9	-62.8	4-2-6	-55
09-	1.58-7	-59.0	-69.3	¥-69-	-40.4	9.09-	-60.9	-61.4	-62.0	-62.8	-63.7	40-	09-
-65	-62.3	6-89-	1.8	8:6-	-41.3	-61:5	-42.3	\$= \$9-	8-69-	8-69-	8-19-	-65.9	-65
-70	-63.8	8-39-	-62.3	-62.5	8:34-	MC 84	2.84-	-64.3	9-69-6	-65.6	-66.3	-67.5	-70
-75	1:69-	2:40-	-64:3	2-69-	-63:3	-65.5	-65.	£-69-	8:69-	8:29-	6:84-	7-64-	-75
04-	6.69-	6.50-	8.79-	4.29-	-67.6 8.5	8-29-	-68.2	-68 -6 7 -8	8-69-	4.89-	6.89-	4.62-	08-
-85	-69.9	6.62-	-79:3	-79.3	3:62-	8:62-	3.6.	8:12-	-71-8	-71.4	-73.6	-73.9	-8 -
0.6-	-73.2	-73.5	-73.5	-13:5	-73.3	-73.2	-73.2	-73.2	-73.2	-73.2	-73.2	-73.5	06-
LAT	,	,	,	•	,	;	,				,	,	LAT
F. 10NC	c	s.	Ę	5	07	\$	δΩ	Ş	0,7	45	0	\$	F • CONC

115 t. ton6	18.7 0		~~					-69.7 -35												141
110	-19.5	•	'																	
105	-19.9	-39:4	-39.8	4.7.4	-54.9	8°-19-	-65.9	-24-1	-73.7	-76.6	78.Z-	-80.1	-80.5	4-48-	-79.0 1.8	-77.8	->6:4-	5.61-	-73.5	
1 00	-20.5	1:3:1	4:4-5	-48.5	-55.4	61.8	3. \$-	8-62-	24.5 -73.5	-75.7	9-71-	-76.3	-78.8	-78.5	7.77-	-76.8	-75-8	5:61-	-73.3	
66	-20.8	-31.5	6-0-	-48.9	-55.7	₹ * † •̄	59-	9-6-6-	5-52-	74.6	1-16-1	7.91-	-77-1	-76.9	4.82-	-75.8	-75.5	-19-3	-73.2	
6	-20.4	-11-6	6-1-	9-64-	-55.7	-61:3	8-19-	-68-9	4:42-	-73.3	-74.5	-75.2	-75.4	-75-4	-75.3	-74.9	-74-5	-75.8	-73.2	
ec \$	-29.6	-31.4	9:6,-	8.84-	-55.4	€:\$=-	6-65-	-67.9	3:62-	-71.8	-72.8	-73.4	-73.7	-73.8 1.0	-73:9	-73.9	-73.9	-73.7	-73:3	
S	5.82-	0 - 1 - 0 0 - 1 - 0	63-5	4:4-	-54.9	6 • 6•−	6-65-	-66.8	-68- -3.00	5:62-	-73-1	1:1-	-72.1	-72.5	4:52-	-72.9	-73.3	-73.4	5.2 -5	
\$	-19-9	-30.5	3-6,-	0-84-	-54.4	P-65-	9-45-	-65.6	4:50-	8-8-	1-69-4	-1-3	4-61-	6.07-	4:12-	g. 51-	-72.6	-73.3	5:81-	
٤	-19-0	3.3	5-5-	4-1-	-53.8	-58-6	8-1-5-	-64-4	-65-	6.8-	7.25-	-68.5	5 ° F y-	6.69-	-74-3	-73:3	-75.0	8.2.2 9.2	-73.5	
\$ 9	4.5	7-67-	- 59.2	-47.3	-53.4	-54.9	-61:J	-63.5	4.65-	-65.4	1:65-	1-66-7	-67.4	-68-3	-69.5	-70.3	-73:\$	-72.5	-73.5	
0.0	-18.4	4.5°-	9.6	6.8,-	-53.3	5-1-5	6:04-	7-4-5	4.52-	-64-6	6.1.9-	-45.3	-46.0	47.9	-68.5	-69.5	8:6	-72.2	-73.5	
E. LONG	0	?	-10	-15	->0	-25	0 x	-15	04-	-45	-50	-55	0 4-	-65	-70	-75	- A0	×	0.0-	141

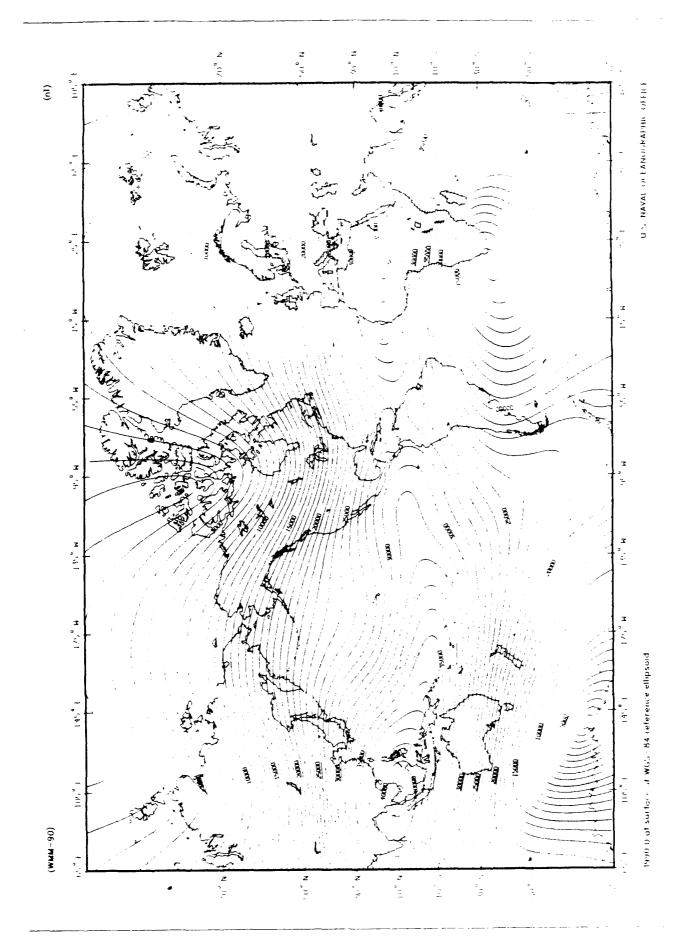
1. 1006	Ü	~	-10	-15	-20	-25	0 4 -	-35	J 7-	-45	- 50	- 5 5	09-	59-	-70	- 75	- 80	-R5	06-	141	9 NO 1 . 1
175	64 6w	9.6	-24.5	-35.4	-43.5	-59:1	-56.8	6-1-9	-65:1	6.09-	\$-22-	1:91-	-79.2	-81.}	-83.1	-62.3	-79.8	7.62-	-73.2		175
170	-8-9	-18:8	-28.4	-37.0	1:77-	1515-	-57:1	6. 29-	5. 99-	-70.3	-73.8	-77:3	5:08-	£:28-	9.58-	-82.8	-89:3	7: 62-	-73.2		170
165	-11.1	6.62-	-30.2	-38.6	8:57-	-53.6	-58.5	-63.2	\$- <u>7</u> 9-	-71.3	6-42-	-78:3	-81.5	-8 -	-84.8	-83.5	-89:3	4.84-	-73.2		165
160	-13.0	1:1-	-31.7	8.04-	-47.3	2.4.5	-54.3	1.64.1	5.8.	-72.3	-75-8	1-62-	-82.3	-84.9	-85.6	-83.5 2.2	1-88-	\$.64-	-73.2		160
155	-14.5	-24-1	-33.1	-41.2	4.4.	1:45-	2.09-	0.59-	£-09-	-73.2	y-92-	-80-1	-83.4	7-98-	-89-F	-83.A	-80.3-	£:62-	-73.7		155
150	-15.7	-25.3	3:1-	-42.2	0-1-	\$. 5.	-61.0	65.8	7.0.7	5-72-	2-7-	-81.3	24.5	-87.2	1.68-	-83.6	\$ - 86-€	1.8.	-73.2		150
145	-16.6	-26.3	-35.1	-43.0	-50.1	-56.}	-61.7	-66.5	4-02-	-74.8	-78.5	-82.1	-85 ° 5	-88-4	-86.8	1.68-	89.8	4:62-	->3-8		145
140	-17.3	27.0	-35.8	1.1.	-50.7	-56.8	45.24-	-67.5	-71:5	-75.5	-79-3	-R2.9	-4-4-	-89.7	-86.5 2.2	1:4-	2.5	-78:5	\$. \$-\$		140
135	-17.6	-27.5	-56.4	7.44- 1.40-1	-51.3	1:15-	6-29-	8 - 29 - 1 - 1	-12:3	1:51-	79.9	-83.5	9-18-	-88.9	-85.9	3:28-	-13.4	-79.3	-13.5		135
130	-12.9	9-5-	8.91-	41 41 41	-51.8	9.8.2.	-63.5	-68.3	-72:3	2.91-	4.08-	-83.9	-84:8	-87.5	8-1-	8-28-	-73:3	-79:3	-73.5		139
125	-18.0	1:47	-37.3	-45.3	-52.4	-58.5	6.49-	6.89-	1:12-	1:21-	7.92-	-63.9	-86.2	1-86-1	0.8×-	-81.3	9-81-	-75:3	2.52-		125
. 120	-18.3	1:82-	7.7	-45.8	4°-7's-	- 26°-3	5.79-	5.04-	-73.5	-77-5	0 · · · · · · · · · · · · · · · · · · ·	4.83.4	3:54-	4 8	- 8 - 8 1 - 8	-49.5		-75:3	-73.2		120
E. LONG	0	-5	-10	-15	-20	-25	0 * -	-35	0 -40	-45	05-	-55	09-	-65	-70	-75	0 % -	-85	00-	141	f. 10N6

i. 10N6	0	? -	-10	-15	-20	-25	01-	-35	-40	-45	J\$-	-55	-60	\$9-	-70	-75	0 K-	- 8 5	06-	1 4 1	f. 10NG
587	مع ه ه	~ 0	-11:5	-20-6	8-82-	-36.5	6-8-	8-67-	-53.7	6-88-	-61.6	-64.7	7-19-	-69.8 2.	9-11-	-73:3	8:82-	6-2-9	-73.2		512
730	-1.0	}:	-12.5	->3.5	-39-3	-37.5	9:5-	b. 8,-	0:1-	b. 65-	9:29-	-65.9	-68. -68.	-71.9	-72.8	7-12-	8: 8	-74.5	-73.2		230
\$25	-00-	23:3	-13.6	-22.8	-31.2	-38-6	-45-1	-5q.8	-55.7	6-09-	63.6	-67.0	6.69	1:21-	-73.9	-75-0	-73.5	-74.6	-73.2		525
220	5.5	9:3=	-15.8	6-5-0	-12 .3	£-61-	-46.1	-51.8	2.95-	-61.9	0° 4°-	9-1-	8-6-1	-73.2	-74.9	-75.8	-75.8	-74.9	-73.2		022
215	-5.7	7.5-	15.8	-25-1	-33.5 -3.5 3	80°C -	-47.2	-52.7	-57.6	-61.9	9: \$ -	9-6-	-71-8	4-5-	-75.9	-76.7	-76-4	-73:3	2.5		215
210	3.6	7-9-	-16.8	-26.2	6-72-	41.5	7-8-5	-53.7	-58:\$	1:29-	\$ - 9 - -	-64.8	-72-8	-75.5	-76-8	-77-5	-76.9	-75:3	-73.2		710
502	7-5-	7.2-	-13.8	-27.3	-35.7	-42.9	2-64-	-54.7	-59.5	9.59-	4-79-	1-4-1	7.4.7	1.91-	-17-8	-78.3	-77.5	-75.9	-73.2		205
20v	-1:8	-8-7	-18.9	-28.4	-36.7	0.44-	5: 05-	-55.7 6.	\$. 09-	4.99-	7.89-	-71.6	6	1.7.	2.87-	-79-0	-78:8	-75.9	-73.5		200
195	7	0 K	-20.1	5.67-	-37.9	-45.1	-51.3	-56.7	-61.3	4-69-	-69-1	4-51-	4.51-	9.81-	\$-02-	-79.8	-78.4	-16.1	-73.5		195
140	39 1 m	-11.3	-21.4	3.08-	[*- 6 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	-46.5	-52.4	1.22-	-62.3	1:99-	6-02-	-73.3	-76.3	-78.9	-80.5	- P 0 - 5	-78.9	-76.3	-73:5		199
185	*** **	-15.8	-22.9	-32.2	1004-	5-2	-53.6	-58.3	-63.3	-67.3	6.02-	-76.2	£:-12-	1.07-	-81.3	-81.1	-79.3	-76.4	-73.5		185
180	4.5	9.31-	-24.6	7.51-	41.8	-48.8	-54.8	04. 0. 0.	-64.4	-68.3	-71.9	-75.2	-78.5	0 K -	45.5	-41.8	-79.9	-76.5	-73.2		180
E. LONG	0	?	-10	-15	->0	->\$	04-	56-	0 %-	-45	05-	-د ۶	09-	-45	-70	-75	D & -	S & -	0.0-	141	E. 1046

INCLINATION (I) WMM-90

1 - 10N6	ũ	٢	-10	- 1 5	-20	-25	0 4-	-35) 7 -	-45	-50	- 5 5	09-	-65	-70	-75	-80	2 × -	06-	LAI	1 . 10NG
\$ 6 g	5.87	13.1	₹. 9.40-	0.0	**************************************	-23-3	-28.5	-34-0	3.851	24.8	9-95-	2.05-	8-85-	-54:}	-61:1	4.6	-67.9	-70.7	2.52		562
U 62	24:3	14:8	5.8 -5.5	-5-6 -5-6	-15:8	-58-8	2.52-	-33.6	-38 -8 -3 -4	43.9	-46	-50.5		2:15-	6:19-	8-19-	1.89-	-79.9	-73.6		u 62
587	23.8	15.8	5.7	-3.8	-13.8	-23-3	-28.5	-34.5	-39.5	-43.7	\$-27-	-51.1	-54.8	-58.5	-62.1	65.5	-68-6	-13:3	-73-2		285
2 5 10	23:3	14:5	3:-	1:9	-14:3	\$: ₂₅ -	829-6	35.0	5	-44.8	-48.5	-52:3	-55.6	5-65-	-63.8	-66.1	h= 2y-	-73:3	-73.2		280
275	5:12	12:5	2.3	6.9	-14:6	-24:5	-31.5	-37.4	2-24-	9:4-	4.04-	-53:8	7-95-	-69.3	4:69-	2:69-	-69-4	4.81.	-73.2		\$2.2
012	9:9	14:5	3:2	2-6-	-18-5	-24.8	-33.4	-39.1	-43.8	-4 { .8	-51-3	-52:8	-52.9	-63.5	4-84-	9:3,-	-49.9	-73-3	-75.5		270
597	18:8	\$:\$	10°	2.5	-29:\$	-28-5	-35-3	4.64-	2.5	#	-52.9 1.8	->4:4	59-5	-62.3	-65.	1.69-	- 29-5	-72-3	-73-8		597
560	4.8	18:8	12:3	4.6	-22.5	-30-3	-36.9	-42.5	-47.2	-51:3	-54.5	6:},-	9-1-9-	- (3.5	-46.3	6:6,-	-71-0	-72.5	-75.5		992
55?	1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	13:4	11:1	-15:5	-24.8	-31.8	-38.5	-44.0	7-89-7	2:55-	-56.1	-59.1	3-29-	104.8	4.10-	2:40-	-71-6	-72.A	-73.5		552
u\$?	11:8	18:9	10.4	-16:3	-28-9	-33:6	-39.8	-45.4	-59:3	54:3	-57.6	\$ 0 \$ ·	-63.4	64.9	-68-5	8:h	1:5,-	-73-1	-75.5		2.50
54.	19:4	Q.	~6·4 6·4	2 × × × × × × × × × × × × × × × × × × ×	8-67-	-34.3	0.5	-46.6	-51.4	-55.5	-50.0	1:29-	-64.8	6.20-	7:1-	4:1-	-73-8	-73.4	-73.5		545
946	6:5	8:5	-10.4	-19.5	2.3	4:51-	7-7-	2:5,-	1.6	-56.8	7-09-	-63.4	9:99-	- 48.6	-70-7	-72.3	-73:6	-73.7	-71.5		040
6. 10NG)	~ -	-10	-15	-20	-25	- 40	-45	04-	-45	-50	-55	04-	54-	-70	-75	04-	\$ €-	0	141	1 10NG

F. LONG	₹00	\$0\$	310	315	120	325	130	335	140	348	150	\$\$\$	t. LONG
141													LAT
0	19.8 -12.7	- 4	18:4	6:5	21.0	-5-5-	10.7	-15.7 -18.1	-19.8	-24.9	-75.1	6-87-	0
Š.	-13:6	1.91-	-18 -18	9-02-	-21.4	-24-3	-19.9	-24.9	-29-1	-32.3	14:8	-38-5	\$ -
-10	-12.3	-15-9	-5.9	-11-3	-16.9	-27.6	-28.0	132.8	-36.9	-48:3	-42.7	-44.7	-10
-15	-15.5	19:9	=15:3	=18:3	-58:4	\$-85-	14.6	-386-	-43:8	-48:8	-43.8	-51:3	-15
->0	-15.8	-18.5	-32.1	-18:6	-31:3	-18:9	-48:3	-49.3	148:1	=\$1:3	-43.8	- }\$:}	-20
-25	=34.8	-25.4		-33.8 -18.8	6-61-	=43:3	18:8	142.4	=51:3	-54.9	-57.5	-11:5	-25
36-	\$:87-	-31:8	-35.5	-11:8	:43:3	=45:3	18:3	-31-3	-13:9	=13:4	-59.5	7-24-	0 2 -
-45	400 400 400	118:4	-39:3	-48-8	-45.2	-13.5	-513.6	-54-3	-51:9	-10:3	-64:\$	\$ - 8 g -	-15
04-	\$ 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9° K-	4.5.8	-15.3	-47.9	-10-2	-53.3	-55-A	-58.1	-69-3	-61.8	-63.3	07-
-45	-43.3	-44.3	-45.9	-47.E	-58-5	-52.2	-54.4	-56.5	-58.6	6-75-	-63.3	1-62-4	-45
-40	46.8 -3.0	6.7-	48.4	5-85-	-51.8	-53-4	-55.1	-56.7	-58.1	-59.3	-60.3	-61-9	-50
-55	-59.2	\$:85-	-51.5	-55.8	-53.3	-54.5	-55.7	-56.8	-57.8	-58-6	-59.3	-50.8	-55
04-	-53.6	-53.7	6.7	-54.6	-55.2	-55.9	1-56-7	-57.4	-58-9	\$. §-	-58-6	-59.4	09-
-65	-57.5	-57:}	-57.5	-57.4	3:23-	6:85-	-58-4	2-85-	-59-1	-59.4	-59.8 3.6	4-80-	-65
-70	3-6,-	-60-6	£-64-8	-69.5	-69-5	-69-6	2-09-	-60.9	-61-9	-61.5	-63.5	-63.6	-70
-75	1.8	6-40-	-63.4	-63.7	-63.6	-63.5	2.5	-63.5	-63.6 -63.6	9:60-	-63.8	-63-6	-75
0	-67.6	-67.3	1:25-	-66.0	-66.8	£:60-	6-64-	\$-69-	7-69-	-66.6	-66.6	-66.7	0 4-
-85	-79-5	-19:4	- 29:3	-79:1	8-62-	-69.9	4-5	4.69-	-69-8 2-4	4-69-8	-69.8	63.8	5 & −
06-	-73.5	5-82-	-73.5	-73.5	-73.5	-73.2	-73-2	-73.5	-73.5	-73:3	-73.5	-73.3	06-
LAT			1	,	;		,					•	1 4 1
F. LONG	JO ₂	505	110	315	∪ 2₹	325	130	375	340	345	350	355	1 . 10N6



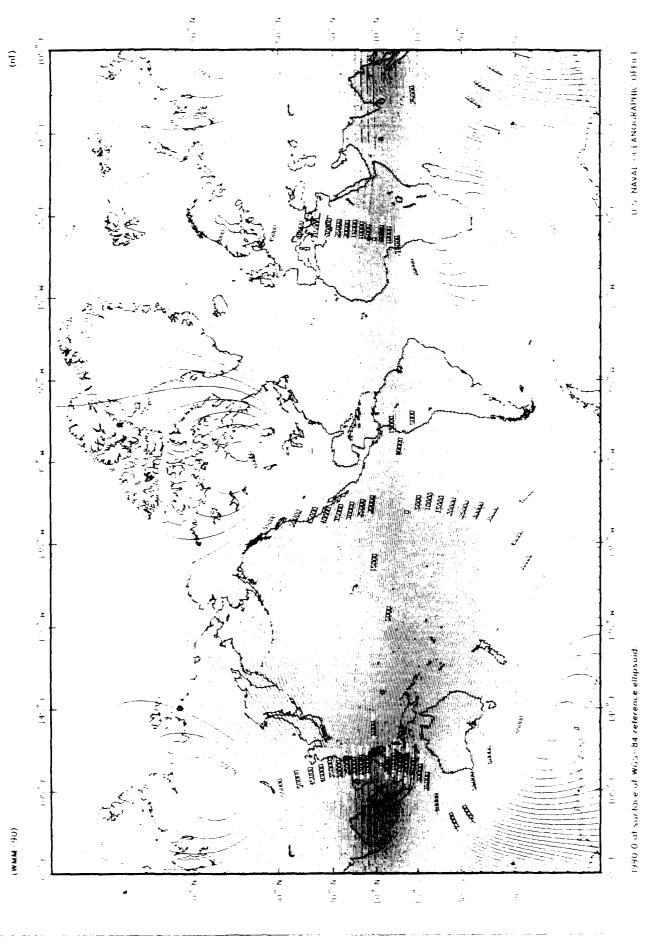




CHART 10. TOTAL INTENSITY (F)

CHART 11. DECLINATION (P)

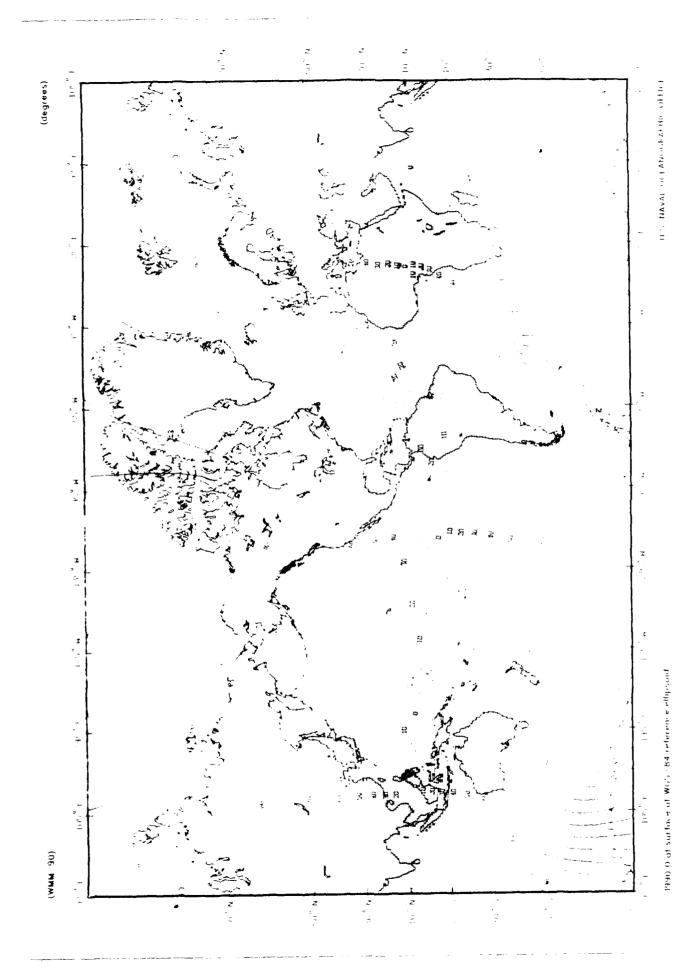


CHART 12. INCLINATION (I)

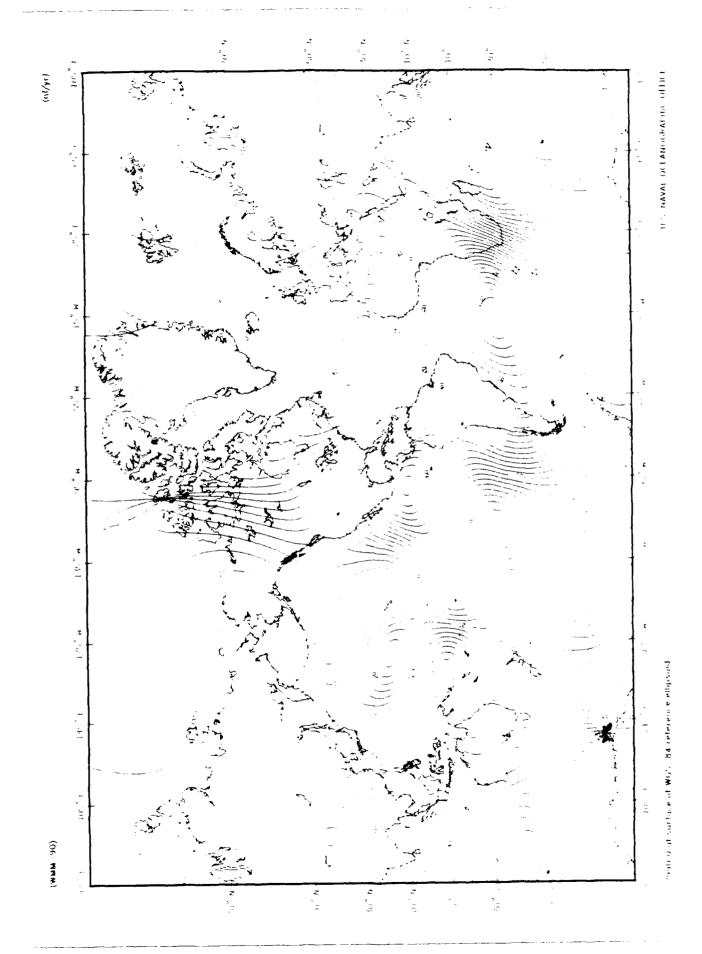


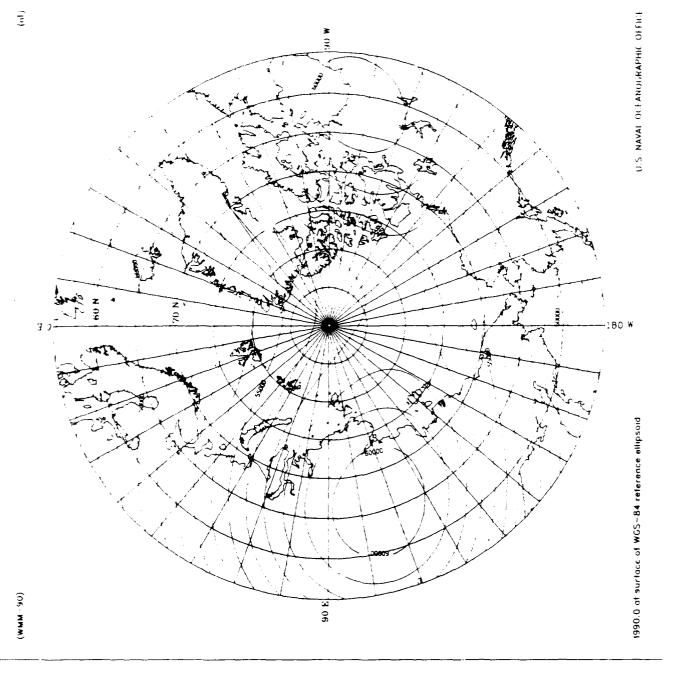
CHART 15. TOTAL INTENSITY (I)

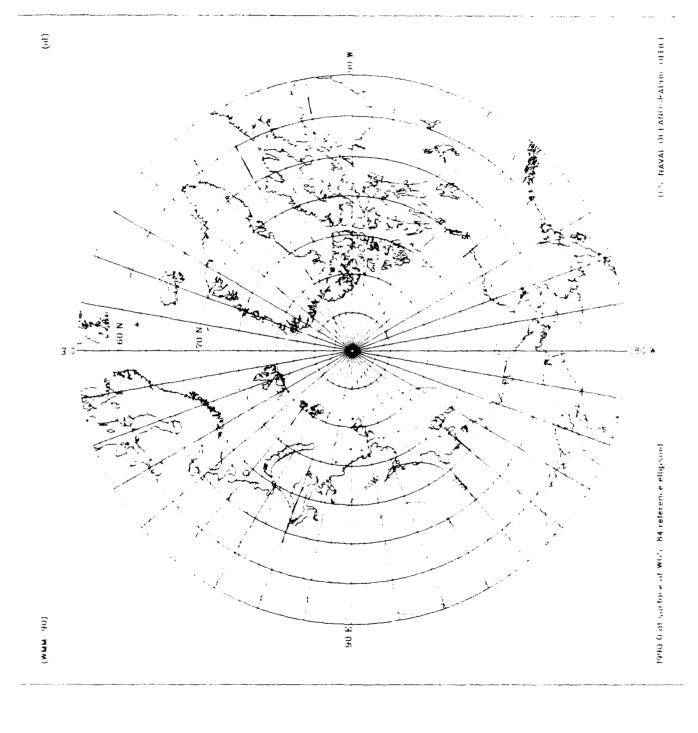


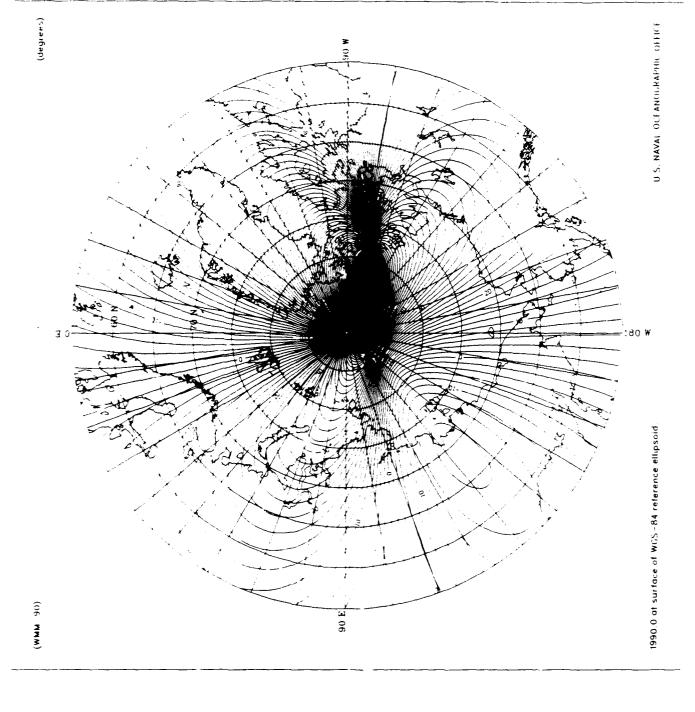
CHART 16. DECLINATION (P)

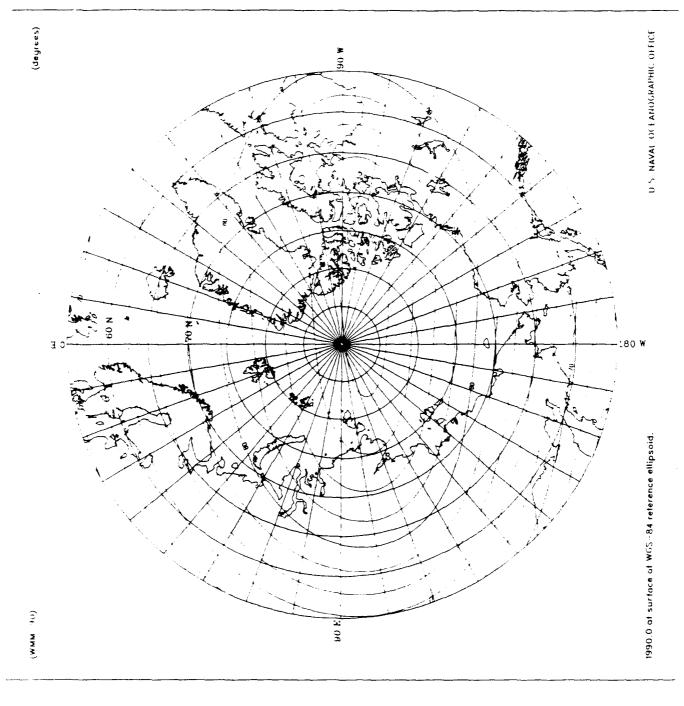
CHART 17. INCLINATION (I)

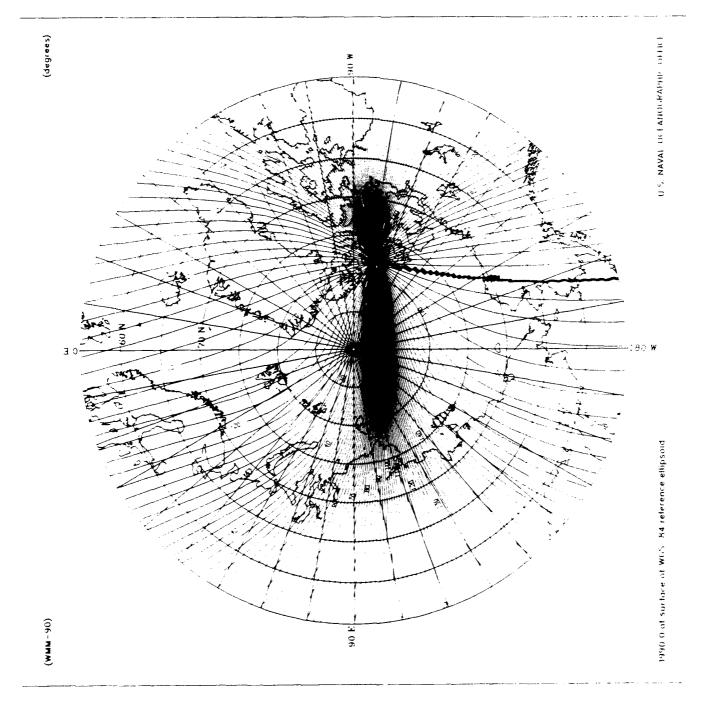
CHART 18. HORIZONTAL INTENSITY (11)

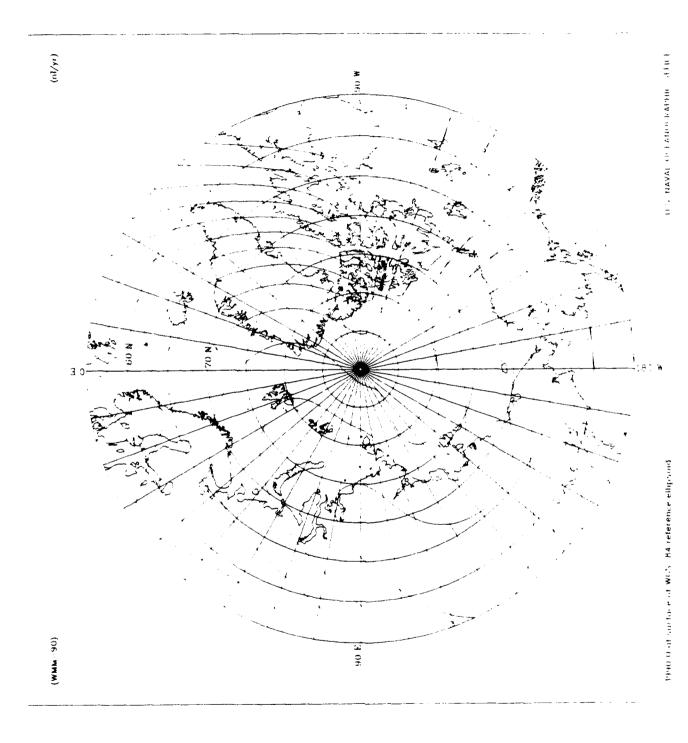


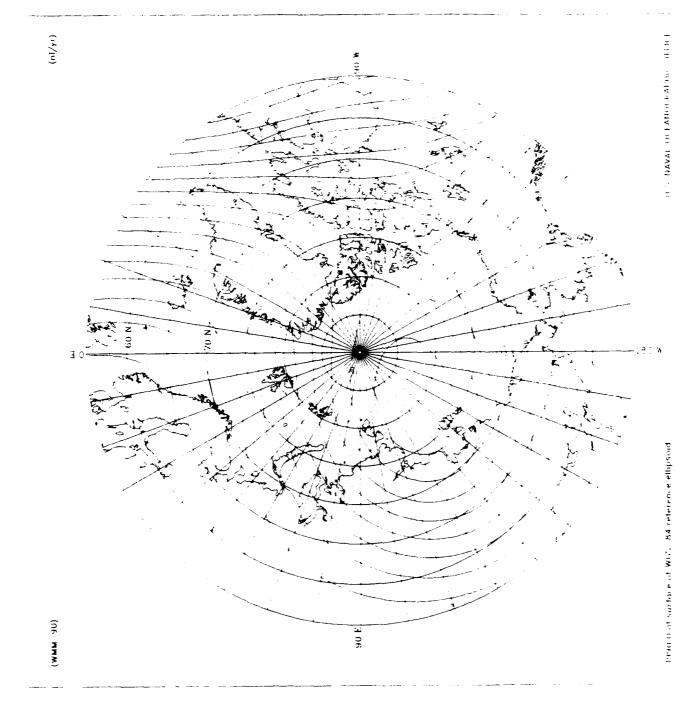












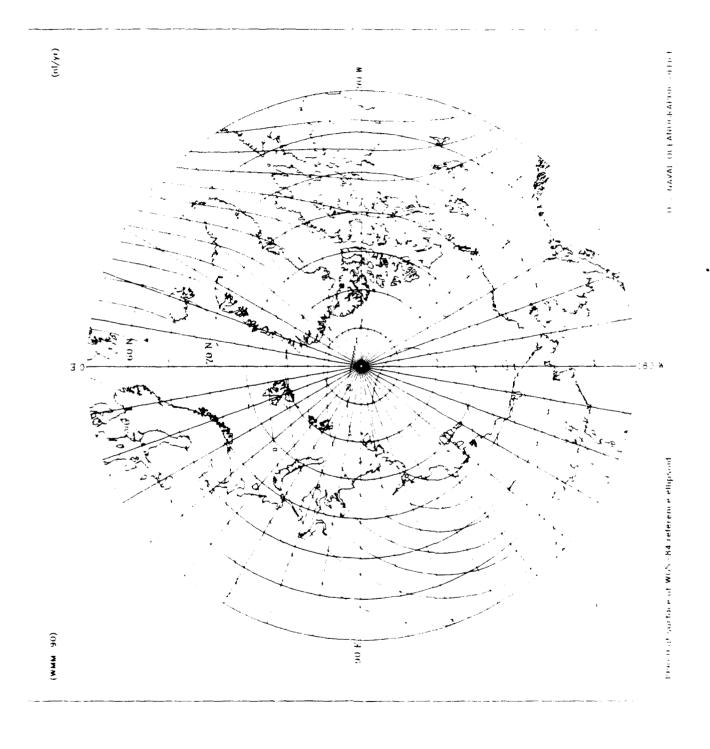


CHART 26. TOTAL INTENSITY (I

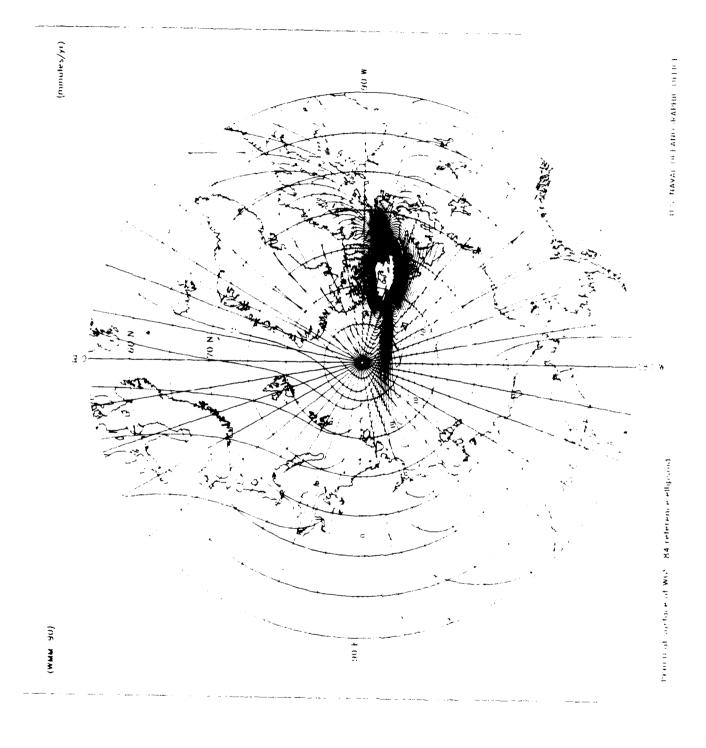
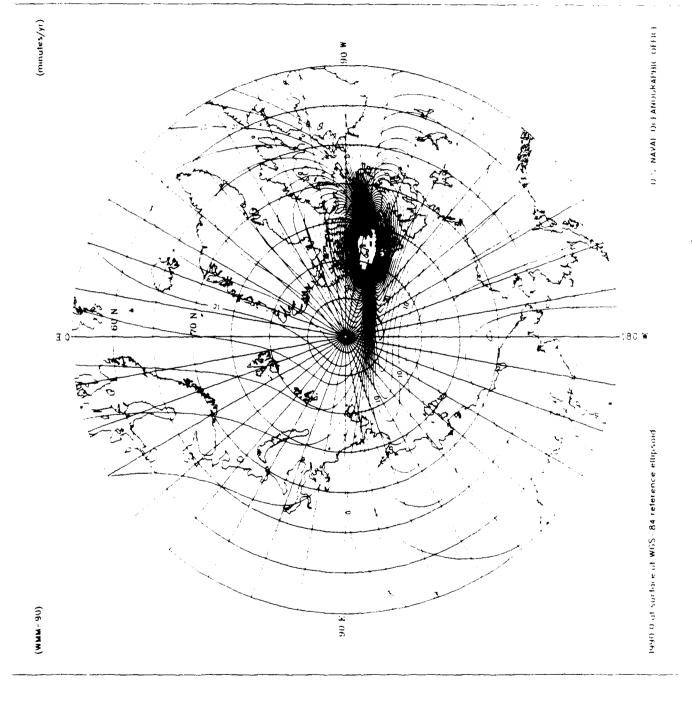


CHART 28. INCLINATION (I)

. O. F.

(MMM 30)



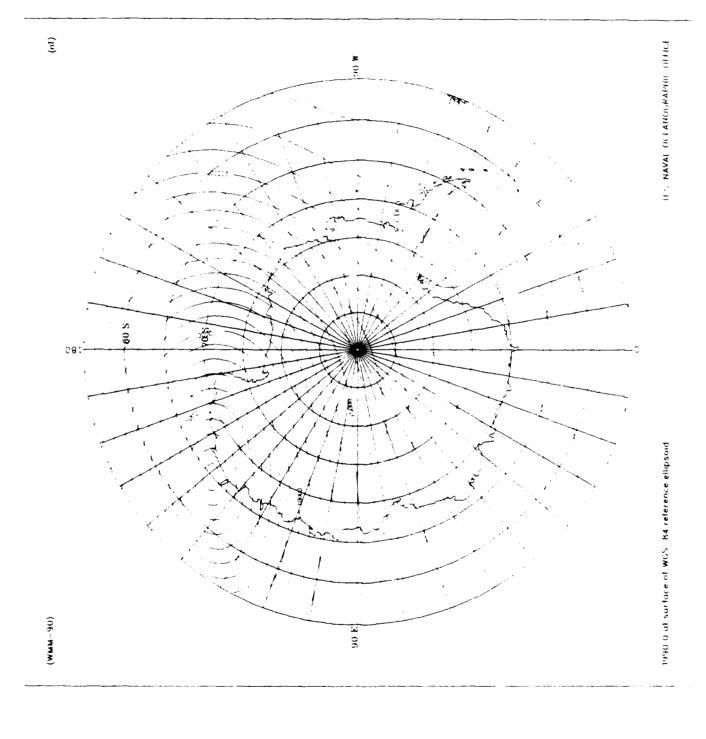
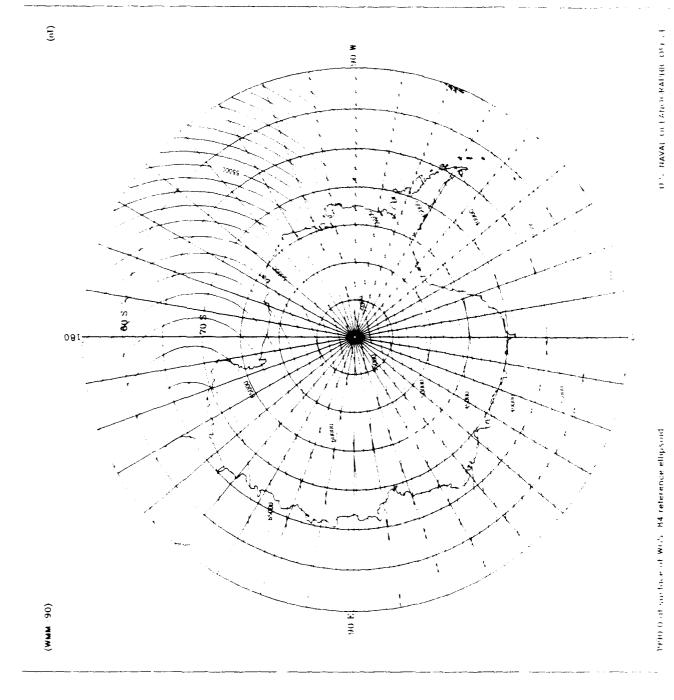
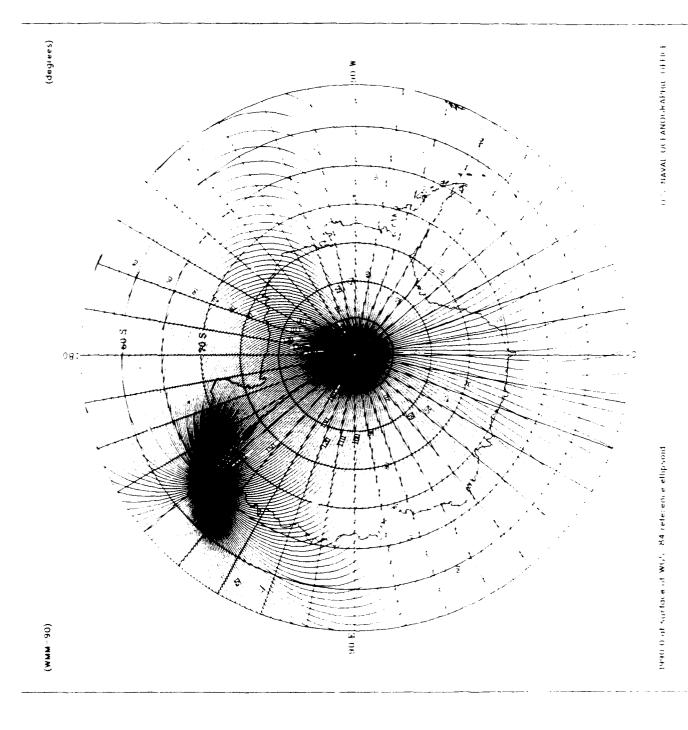


CHART 31, VERTICAL COMPONENT (Z)





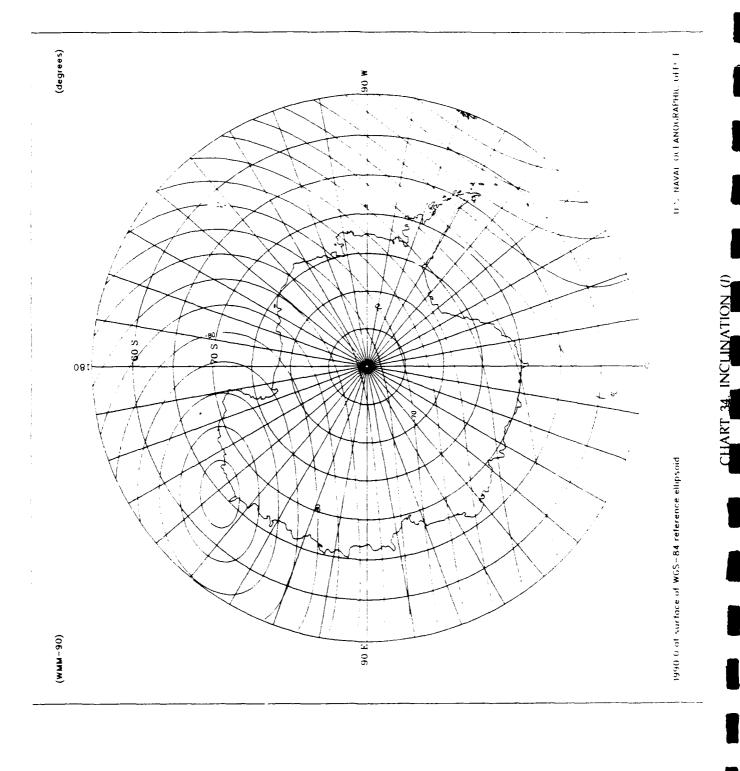
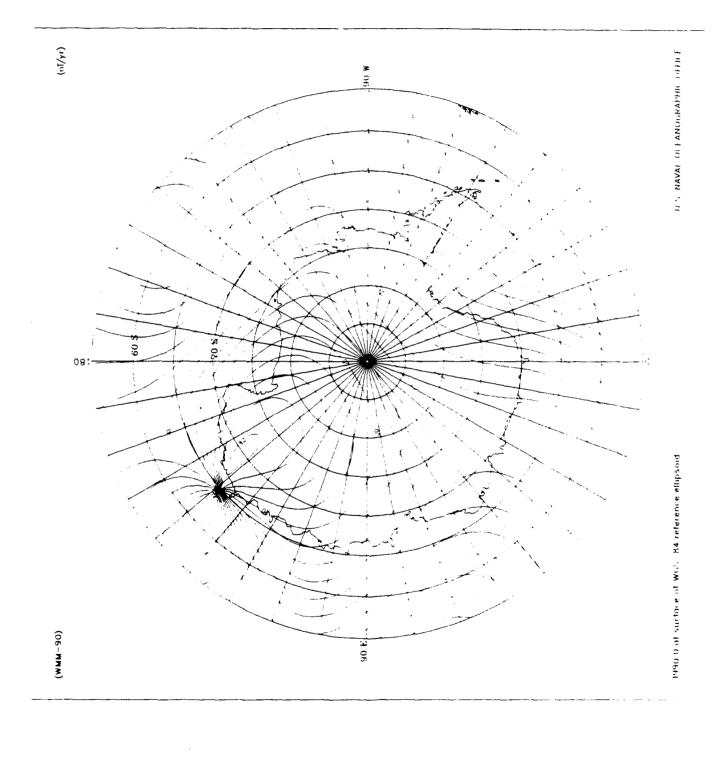
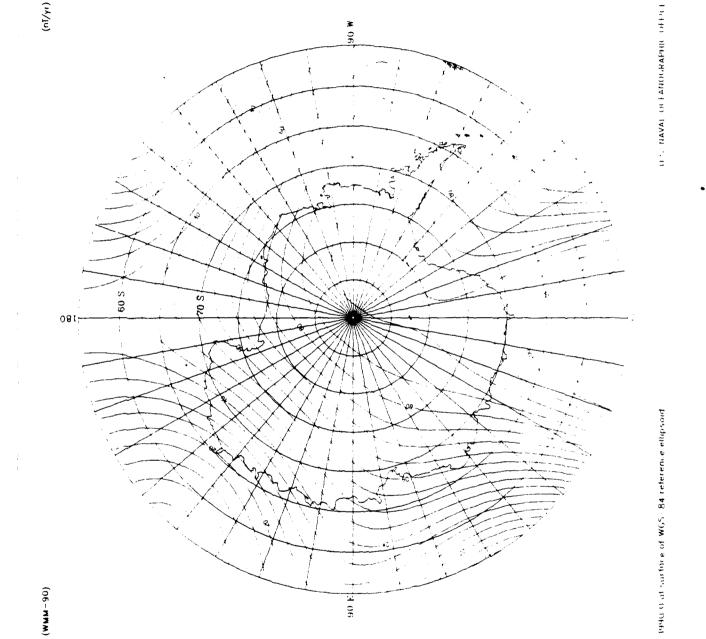


CHART 35. GRID VARIATION (GV)





(n1/yr)

CHART 37. VERTICAL COMPONENT (Z)

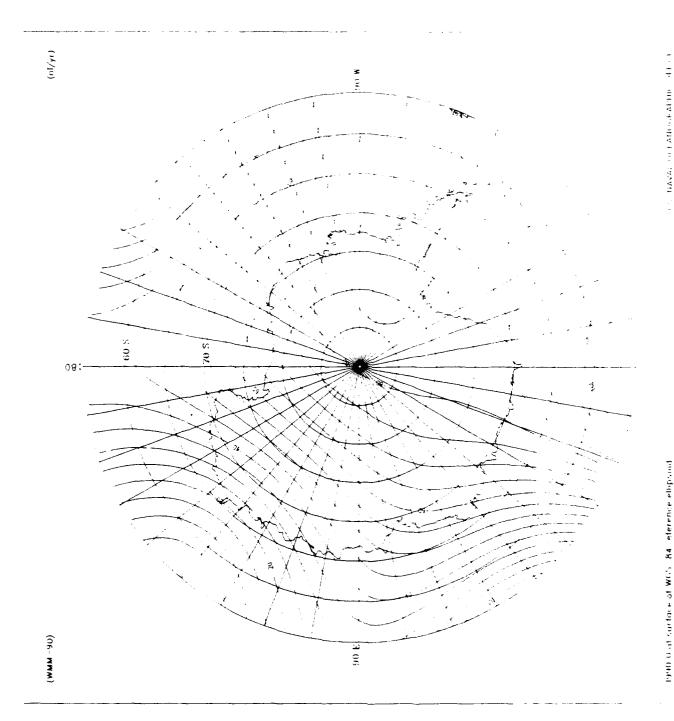
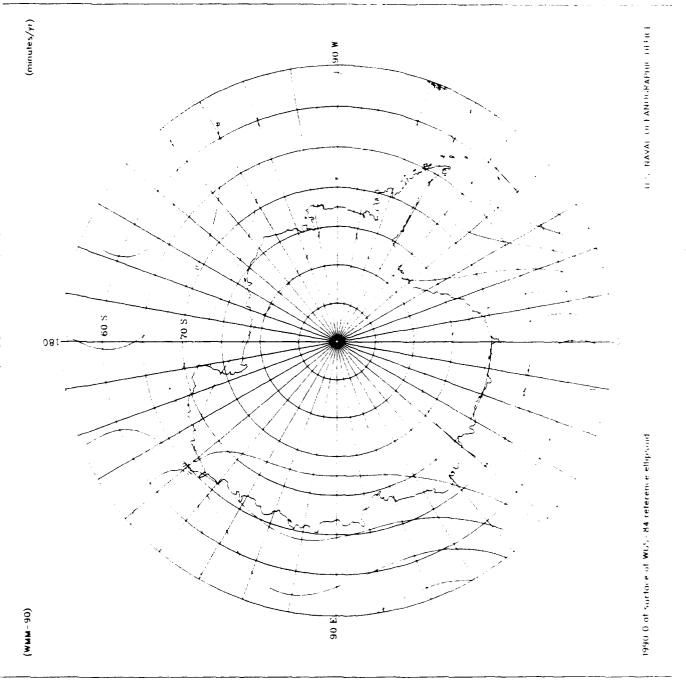


CHART 38. TOTAL INTENSITY (I)



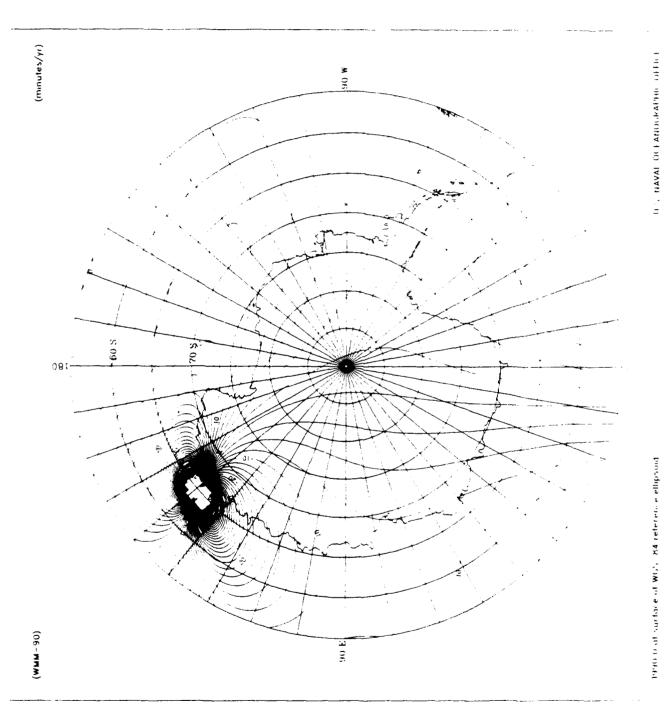
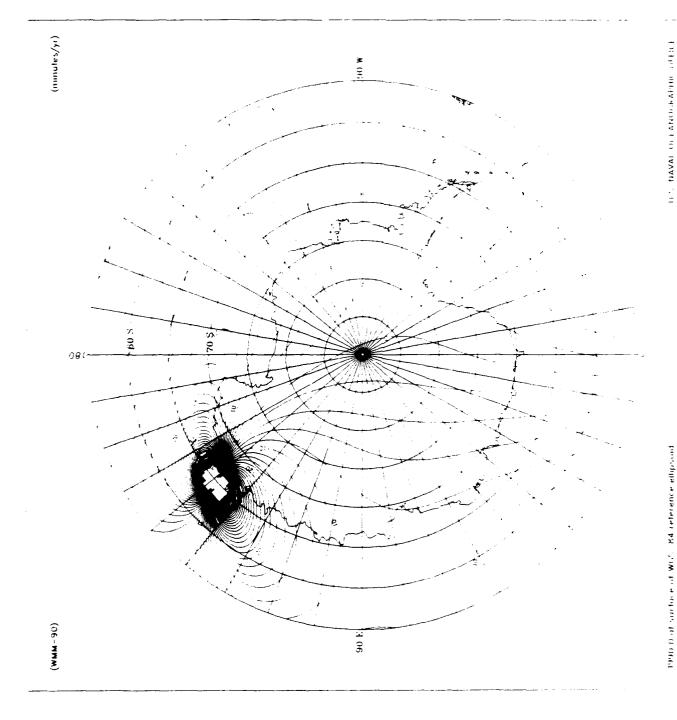


CHART 40. INCLINATION (I)



193

REFERENCES

- Cain, Joseph C., et al.; A Proposed Model for the International Geomagnetic Reference Field 1965, <u>Journal of Geomagnetism and Geoelectricity</u>, Vol. 19, No. 4, pp. 335-355, 1967. (see appendix)
- Department of Defense World Geodetic System 1984, <u>Technical Report</u> <u>TR 8350.2</u>, Defense Mapping Agency, 1987.
- Langel, Robert A.; The Main Field in <u>Geomagnetism</u>, Vol. 1, Chapter 4, edited by J.A. Jacobs, Academic Press, New York, pp. 249-512, 1987.
- Langel, Robert A. and R. H. Estes; The near-Earth magnetic field at 1980 determined from MAGSAT data, <u>J. Geophys. Res. 90</u>, pp. 2495-2509, 1985.
- Quinn, John M., David J. Kerridge, and David R. Baraclough; World Magnetic Charts for 1985 spherical harmonic models of the geomagnetic field and its secular variation, <u>Geophys. J.R. Astr. Soc.</u> Vol. 87, pp. 1143-1157, 1986.
- Zmuda, Alfred J.; World Magnetic Survey 1957-1969, International Association of Geomagnetism and Aeronomy (IAGA) Bulletin #28, pp. 186-188, 1971.

APPENDIX

FORTRAN LISTING OF SUBROUTINE GEOMAG WITH
THE WMM-90 MODEL COEFFICIENTS

0SUBROUTINE GEOMAG (GEOMAGNETIC FIELD COMPUTATION) WMM-90 is a proposed Defense Mapping Agency (DMA) standard product. For information on the use and applicability of this product contact: DIRECTOR DEFENSE MAPPING AGENCY/HEADQUARTERS ATTN: CODE PR 8613 LEE HIGHWAY FAIRFAX, VA 22031-2137 **GEOMAG PROGRAMMED BY:** JOHN M. QUINN 7/19/90 GEOPOTENTIAL DIVISION, CODE GGM U.S. NAVAL OCEANOGRAPHIC OFFICE (NAVOCEANO) STENNIS SPACE CENTER (SSC), MS 39522-5001 PHONE: COM: (601) 688-4252 AV: 485-4252 FAX: (601) 688-5701 PURPOSE: THIS ROUTINE COMPUTES THE DECLINATION (DEC), INCLINATION (DIP), TOTAL INTENSITY (TI), AND GRID VARIATION (GV - POLAR REGIONS USING A POLAR STEREOGRAPHIC PROJECTION ONLY) OF THE EARTH'S MAGNETIC FIELD IN GEODETIC COORDINATES FROM THE COEFFICIENTS OF THE CURRENT OFFICIAL DEPARTMENT OF DEFENSE (DOD) SPHERICAL HARMONIC WORLD MAGNETIC MODEL (WMM-90). THE WMM SERIES OF MODELS IS UPDATED EVERY 5 YEARS ON 1 JANUARY OF THOSE YEARS WHICH ARE DIVISIBLE BY 5 (I.E., 1980, 1985, 1990, ETC.) BY THE U.S. NAVAL OCEANOGRAPHIC OFFICE IN COOPERATION WITH THE BRITISH GEOLOGICAL SURVEY (BGS) AND IS BASED ON GEOMAGNETIC SURVEY MEASUREMENTS FROM AIRCRAFT, SATELLITE, AND GEOMAGNETIC OBSERVATORIES.

MODEL: THE WMM SERIES GEOMAGNETIC MODELS ARE COMPOSED OF TWO PARTS: THE MAIN FIELD MODEL, WHICH IS VALID AT THE BASE EPOCH OF THE CURRENT MODEL, AND A SECULAR VARIATION MODEL, WHICH ACCOUNTS FOR SLOW TEMPORAL VARIATIONS IN THE MAIN GEOMAGNETIC FIELD FROM THE BASE EPOCH TO A MAXIMUM OF 5 YEARS BEYOND THE BASE EPOCH. FOR EXAMPLE, THE BASE EPOCH OF THE WMM-90 MODEL IS 1990.0. THIS MODEL IS THEREFORE CONSIDERED VALID BETWEEN 1990.0 AND 1995.0. THE COMPUTED MAGNETIC PARAMETERS ARE REFERENCED TO THE WGS-84 ELLIPSOID.

ACCURACY: IN OCEAN AREAS AT THE EARTH'S SURFACE OVER THE ENTIRE 5-YEAR LIFE OF A DEGREE AND ORDER 12 SPHERICAL HARMONIC MODEL SUCH AS WMM-90, THE RMS DECLINATION ERROR IS ESTIMATED TO BE < .5 DEGREES, AND THE RMS INCLINATION ERROR IS ESTIMATED TO BE < .5 DEGREES. ALSO, THE RMS TOTAL INTENSITY ERROR IS ESTIMATED TO BE < 200 NANOTESLAS.

 \circ

THE ACCURACY AT ANY GIVEN TIME OF ALL FOUR GEOMAGNETIC PARAMETERS DEPENDS ON THE GEOMAGNETIC LATITUDE. THE ERRORS ARE LEAST AT THE EQUATOR AND GREATEST AT THE MAGNETIC POLES.

IT IS VERY IMPORTANT TO NOTE THAT A DEGREE AND ORDER 12 MODEL, SUCH AS WMM-90, DESCRIBES ONLY THE LONG WAVELENGTH SPATIAL MAGNETIC FLUCTUATIONS DUE TO EARTH'S CORE. NOT INCLUDED IN THE WMM SERIES MODELS ARE INTERMEDIATE AND SHORT WAVELENGTH SPATIAL FLUCTUATIONS OF THE GEOMAGNETIC FIELD WHICH ORIGINATE IN THE EARTH'S MANTLE AND CRUST. CONSEQUENTLY, ISOLATED ANGULAR RESIDUALS AT VARIOUS POSITIONS ON THE SURFACE (PRIMARILY OVER LAND, IN CONTINENTAL MARGINS, AND OVER OCEANIC SEAMOUNTS, RIDGES, AND TRENCHES) OF SEVERAL DEGREES MAY BE EXPECTED. ALSO NOT INCLUDED IN THE MODEL ARE NONSECULAR TEMPORAL FLUCTUATIONS OF THE GEOMAGNETIC FIELD OF MAGNETOSPHERIC AND IONOSPHERIC ORIGIN. DURING MAGNETIC STORMS, TEMPORAL FLUCTUATIONS CAN CAUSE SUBSTANTIAL DEVIATIONS OF THE GEOMAGNETIC FIELD FROM MODEL VALUES. IN ARCTIC AND ANTARCTIC REGIONS, AS WELL AS IN EQUATORIAL REGIONS, DEVIATIONS FROM MODEL VALUES ARE BOTH FREQUENT AND PERSISTENT.

 C IF THE REQUIRED DECLINATION ACCURACY IS MORE STRINGENT THAN THE WMM SERIES OF MODELS PROVIDE. THE USER IS ADVISED TO REQUEST SPECIAL (REGIONAL OR LOCAL) SURVEYS BE PERFORMED AND MODELS PREPARED BY NAVOCEANO, WHICH OPERATES THE PROJECT MAGNET AIRCRAFT AND THE POLAR ORBITING GEOMAGNETIC SURVEY (POGS) SATELLITE. REQUESTS OF THIS NATURE SHOULD BE MADE THROUGH DMA AT THE ADDRESS ABOVE. USAGE: THIS ROUTINE IS BROKEN UP INTO TWO PARTS: A) AN INITIALIZATION MODULE, WHICH IS CALLED ONLY ONCE AT THE BEGINNING OF THE MAIN (CALLING) **PROGRAM** B) A PROCESSING MODULE, WHICH COMPUTES THE MAGNETIC FIELD PARAMETERS FOR EACH SPECIFIED GEODETIC POSITION (ALTITUDE, LATITUDE, LONGITUDE) AND TIME INITIALIZATION IS MADE VIA A SINGLE CALL TO THE MAIN ENTRY POINT (GEOMAG), WHILE SUBSEQUENT PROCESSING CALLS ARE MADE THROUGH THE SECOND ENTRY POINT (GEOMG1). ONE CALL TO THE PROCESSING MODULE IS REQUIRED FOR EACH POSITION AND TIME. THE VARIABLE MAXDEG IN THE INITIALIZATION CALL IS THE MAXIMUM DEGREE TO WHICH THE SPHERICAL HARMONIC MODEL IS TO BE COMPUTED. IT MUST BE SPECIFIED BY THE USER IN THE CALLING ROUTINE. NORMALLY IT IS 12 BUT IT MAY BE SET LESS THAN 12 TO INCREASE COMPUTATIONAL SPEED AT THE EXPENSE OF REDUCED ACCURACY. THE PC VERSION OF THIS SUBROUTINE MUST BE COMPILED WITH A FORTRAN 77 COMPATIBLE COMPILER SUCH AS THE MICROSOFT OPTIMIZING FORTRAN COMPILER VERSION 4.1 OR LATER. REFERENCES: JOHN M. OUINN, DAVID J. KERRIDGE, AND DAVID R. BARRACLOUGH, WORLD MAGNETIC CHARTS FOR 1985 - SPHERICAL HARMONIC MODELS OF THE GEOMAGNETIC FIELD AND ITS SECULAR VARIATION, GEOPHYS. J. R. ASTR. SOC. (1986) Vol. 87,

PP. 1143-1157

```
DEFENSE MAPPING AGENCY TECHNICAL REPORT TR 8350.2
            DEPARTMENT OF DEFENSE WORLD GEODETIC SYSTEM 1984.
            SEPT. 30 (1987)
         JOSEPH C. CAIN, ET AL., A PROPOSED MODEL FOR THE
            INTERNATIONAL GEOMAGNETIC REFERENCE FIELD - 1965.
            J. GEOMAG. AND GEOELECT. VOL. 19, NO. 4, PP. 335-355
            (1967) (SEE APPENDIX)
        ALFRED J. ZMUDA, WORLD MAGNETIC SURVEY 1957-1969,
            INTERNATIONAL ASSOCIATION OF GEOMAGNETISM AND
            AERONOMY (IAGA) BULLETIN #28, PP. 186-188 (1971)
                           **********
       PARAMETER DESCRIPTIONS:
                  - SEMIMAJOR AXIS OF WGS-84 ELLIPSOID (KM)
                  - SEMIMINOR AXIS OF WGS-84 ELLIPSOID (KM)
        В
       RE
                  - MEAN RADIUS OF IAU-66 ELLIPSOID (KM)
      SNORM
                  - SCHMIDT NORMALIZATION FACTORS
                  - GAUSS COEFFICIENTS OF MAIN GEOMAGNETIC MODEL (NT)
       CD
                  - GAUSS COEFFICIENTS OF SECULAR GEOMAGNETIC MODEL (NT/YR)
                  - TIME ADJUSTED GEOMAGNETIC GAUSS COEFFICIENTS (NT)
- TIME ON PREVIOUS CALL TO GEOMAG (YRS)
- GEODETIC ALTITUDE ON PREVIOUS CALL TO GEOMAG (YRS)
       TC
      OTIME
      OALT
                  - GEODETIC LATITUDE ON PREVIOUS CALL TO GEOMAG (DEG.)
      OLAT
      OLON
                  - GEODETIC LONGITUDE ON PREVIOUS CALL TO GEOMAG (DEG.)
                                                                                            (INPUT)
      TIME
                  - COMPUTATION TIME (YRS)
                   (E.G., 1 JULY 1985 = 1985.50
       ALT
                  - GEODETIC ALTITUDE (KM
                                                                                            (INPUT)
                  - GEODETIC LATITUDE (DEG.)
- GEODETIC LONGITUDE (DEG.)
- BASE TIME OF GEOMAGNETIC MODEL (YRS)
      GLAT
                                                                                            (INPUT)
                                                                                            (INPUT)
      GLON
      EPOCH
       DTR
                  - DEGREE TO RADIAN CONVERSION
                  - SINE OF (M*SPHERICAL COORD. LONGITUDE)
- COSINE OF (M*SPHERICAL COORD. LONGITUDE)
      SP(M)
      CP(M)
                  - SINE OF (SPHERICAL COORD. LATITUDE)
       ST
       CT
                  - COSINE OF (SPHERICAL COORD. LATITUDE)
                  - SPHERICAL COORDINATE RADIAL POSITION (KM)
- COSINE OF SPHERICAL TO GEODETIC VECTOR ROTATION ANGLE
- SINE OF SPHERICAL TO GEODETIC VECTOR ROTATION ANGLE
- RADIAL COMPONENT OF GEOMAGNETIC FIELD (NT)
        R
       CA
        SA
       BR
                  - THETA COMPONENT OF GE MAGNETIC FIELD (NT)
       BT
                  - PHI COMPONENT OF GEOMAGNETIC FIELD (NT)
       BP
     P(N,M)
                  - ASSOCIATED LEGENDRE POLYNOMIALS (UNNORMALIZED)
                  - ASSOCIATED LEGENDRE POLYNOMIALS FOR M=1 (UNNORMALIZED)
      PP(N)
                  - THETA DERIVATIVE OF P(N,M) (UNNORMALIZED)
- NORTH GEOMAGNETIC COMPONENT (NT)
- EAST GEOMAGNETIC COMPONENT (NT)
     DP(N,M)
       BX
       BY
       BZ
                  - VERTICALLY DOWN GEOMAGNETIC COMPONENT (NT)
                  - HORIZONTAL GEOMAGNETIC COMPONENT (NT)
       BH
                  - GEOMAGNETIC DECLINATION (DEG.)
                                                                                            (OUTPUT)
       DEC
                    EAST=POSITIVE ANGLES
                    WEST=NEGATIVE ANGLES
```

0000000	DIP	- GEOMAGNETIC INCLINATION (DEG.) DOWN=POSITIVE ANGLES UP=NEGATIVE ANGLES	(OUTPUT)
	TI GV	- GEOMAGNETIC TOTAL INTENSITY (NT) - GEOMAGNETIC GRID VARIATION (DEG.) REFERENCED TO GRID NORTH GRID NORTH REFERENCED TO 0 MERIDIAN	(OUTPUT) (OUTPUT)
000000000	MAXDEG MOXORD	OF A POLAR STEREOGRAPHIC PROJECTION (ARCTIC/ANTARCTIC ONLY) - MAXIMUM DEGREE OF SPHERICAL HARMONIC MODEL - MAXIMUM ORDER OF SPHERICAL HARMONIC MODEL	(INPUT)
C**	******	**********************************	******
0000		THIS VERSION OF GEOMAG USES THE WMM-90 GEOMAGNE DEL REFERENCED TO THE WGS-84 GRAVITY MODEL ELLIPS	
C**	*****	********************	******
č			
0000000			
č			
C			
č			
C			
C**	*****	*********************	*****
Č			
CCCC		INITIALIZATION MODULE	
č		INTIMEZATION MODULE	
C		******************	• • • • • • • • • • • • • • • • • • •
C	र । २० वट प्रशासिक प		or ear ear ear ear ear ear ear ear ear ear ear
C			
C	SUBROU	JTINE GEOMAG(MAXDEG)	
C C			
	DIMENS DIMENS REAL K	SION C(0:12,0:12),CD(0:12,0:12),TC(0:12,0:12) SION P(0:12,0:12),DP(0:12,0:12),SNORM(0:12,0:12) SION SP(0:12),CP(0:12),FN(0:12),FM(0:12),PP(0:12) (0:12,0:12)	
С	EQUIVA	LENCE (SNORM,P)	
C		DO 071/1000 04	
C	DATA E	POCH/1990.0/	
C C			

*	DATA C/	0.0, 59.0,	-29780.5, 76.1,	-2134.3, 22.9,	1312.9, 3.6,	933.5, -3.3,	-208.3, 1.3,
*		-1.3,		-1851.7,	3062.2, 2.3,	-2244.7, 9.5,	784.9, -2.6,
*		352.2, -1.4,	63.7, 0.1,	-62.1, -2278.3,		1691.9,	1246.8,
*			246.5,	60.0,	1.3,	-1.2,	-0.9,
*		4.5,	-2.5,	0.5,	-284.9,	291.7,	-352.4,
*		808.6,			-181.3,	30.2,	-11.7,
*		-10.7,	-5.6,		0.7,	249.4, 0.4,	-232.7, 4.7,
*		91.3, -17.5,	-296.5, 10.7,			0.4,	40.8,
*		148.7,	-154.6,	•	97.4,	-37.2,	15.4,
*		7.9,	2.2,	-3.2,	3.9,	-1.1,	-0.2,
*		-14.7,	82.2,	70.0,	-56.2,	-1.4,	24.6,
*		-96.0,	10.1,		-1.4,	3.2,	0.3,
*		-1.1,	-78.6,		0.1, 3.0,	19.9, 6.3,	17.9, 1.7,
*		-21.5, -0.3,	-6.8, 0.9,		-19.3,	6.6,	-20.1,
*		13.4,	9.8,		-9.1,	-7.0,	0.8,
*		3.0,	0.9,	-0.6,	-21.9,	14.3,	9.5,
*		-6.7,	-6.4,		8.9,	-8.0,	2.1,
*		-5.5,	3.7, 5.7,	-1.1, -4.0,	0.8, -0.4,	2.6, -1.7,	
*		2.6, -0.8,	-6.5,			0.2,	
*		1.0,	-1.6,		1.1,	-0.7,	-1.7,
*		-1.5,	-1.3,	-1.1,	0.6,	3.0,	0.4,
*		0.7,	0.7,				
*		-1.1,	1.2,	-0.2,	-1.3,	0.6,	0.6.
*		0.2/					
C C							
C	DATA CD/	0.0,	16.0,	-11.7, 2.1	l, -0.8,	1.7,	0.8, 0.5,
*		0.0,			0.0,	-13.8,	
*		-7.6,	1.0,	0.0, 0.0		-1.1,	
*		0.0, 1.5,	0.0,	-12.8, -14.9 0.0, 0.0		0.0, 0.0,	
*		0.8,	-11.3,	5.8. 0.8	3, -2.7,	0.0,	1.5, 0.0,
*		0.0,	0.0,	0.0, 0.0), 3.3,		2.8, 0.0,
*		-6.4,	0.0,	0.0, 2.7	7, -2.1,	0.0,	0.0, 0.0,
*		0.0,	0.0,	-2.1, 1.2		0.6,	3.0, 0.0,
*		-1.0,	0.0,	0.0, 0.0 0.0, 0.0		0.0, 0.0,	-0.6, -0.6, 1.0, 0.0,
*		0.0, 0.0,	-2.3, 0.0,	0.0, 0.0		0.0,	0.0, 0.0,
*		0.4,	0.0,	0.0, 0.0	•	0.0,	0.0, 0.0,
*		0.4,	-0.8,	0.5, 0.3	3, 0.5,	0.0,	-0.7, 0.0,
*		57*0.0/					

```
INITIALIZE CONSTANTS
CCC
        IF (MAXDEG .GT. 12) MAXDEG=12
        MAXORD=MAXDEG
        PI=3.14159265359
        DTR=PI/180.0
        SP(0)=0.
        CP(0)=1.
        P(0,0)=1.
        PP(0)=1.
        DP(0,0)=0.
        A=6378.137
        B=6356.7523142
        RE=6371.2
        A2=A**2
        B2=B**2
        C2 = A2 - B2
        A4=A2**2
        B4=B2**2
        C4 = A4 - B4
CCCC
          CONVERT SCHMIDT NORMALIZED GAUSS COEFFICIENTS TO
         UNNORMALIZED
        SNORM(0,0)=1.
        DO 20 N=1,MAXORD
        SNORM(N,0)=SNORM(N-1,0)*FLOAT(2*N-1)/FLOAT(N)
        J=2
        DO 10 M=0,N
        K(N,M)=FLOAT((N-1)**2-M**2)/FLOAT((2*N-1)*(2*N-3))
        IF (M.GT. 0) THEN
        FLNMJ=FLOAT((N-M+1)*J)/FLOAT(N+M)
        SNORM(N,M)=SNORM(N,M-1)*SQRT(FLNMJ)
        J=1
        C(M-1,N)=SNORM(N,M)*C(M-1,N)
        CD(M-1,N)=SNORM(N,M)*CD(M-1,N)
        ENDIF
        C(N,M)=SNORM(N,M)*C(N,M)
        CD(N,M)=SNORM(N,M)*CD(N,M)
    10 CONTINUE
        FN(N)=FLOAT(N+1)
        FM(N)=FLOAT(N)
    20 CONTINUE
        K(1,1)=0.
        OTIME = -1000.
        OALT=-1000.
        OLAT = -1000.
         OLON=-1000.
```

```
C
C
        RETURN
C
00000000
                  PROCESSING MODULE
Č
        ENTRY GEOMG1(ALT,GLAT,GLON,TIME,DEC,DIP,TI,GV)
C
        DT=TIME-EPOCH
        IF (OTIME .LT. 0. .AND. (DT .LT. 0. .OR. DT .GT. 5.)) THEN
         PRINT *,
        PRINT *, 'WARNING - TIME EXTENDS BEYOND MODEL 5-YEAR LIFE SPAN' PRINT *, 'CONTACT DMA FOR PRODUCT UPDATES:'
         PRINT *
        PRINT *.'
                      DEFENSE MAPPING AGENCY'
         PRINT *
                      ATTN: Code PRS'
        PRINT *.'
                      8613 LEE HIGHWAY'
         PRINT *.'
                      FAIRFAX, VA 22031-2137'
                     (703)285-9197, AUTOVON 356-9197'
         PRINT *
         PRINT *
         PRINT *, 'EPOCH = ',EPOCH
         PRINT *, 'TIME = ',TIME
         ENDIF
C
         RLON=GLON*DTR
         RLAT=GLAT*DTR
         SRLON=SIN(RLON)
         SRLAT=SIN(RLAT)
         CRLON=COS(RLON)
         CRLAT=COS(RLAT)
         SRLON2=SRLON**2
         SRLAT2=SRLAT**2
         CRLON2=CRLON**2
         CRLAT2=CRLAT**2
         SP(1)=SRLON
         CP(1)=CRLON
 C
           CONVERT FROM GEODETIC COORDS. TO SPHERICAL COORDS.
 C
         IF (ALT .NE. OALT .OR. GLAT .NE. OLAT) THEN
         Q=SQRT(A2-C2*SRLAT2)
```

```
O1=AI.T*O
        Q2=((Q1+A2)/(Q1+B2))**2
        CT=SRLAT/SQRT(Q2*CRLAT2+SRLAT2)
        ST=SQRT(1.0-CT**2)
        R2=ALT**2+2.0*Q1+(A4-C4*SRLAT2)/Q**2
        R=SQRT(R2)
        D=SQRT(A2*CRLAT2+B2*SRLAT2)
        CA=(ALT+D)/R
        SA=C2*CRLAT*SRLAT/(R*D)
        ENDIF
C
        IF (GLON .NE. OLON) THEN
        DO 40 M=2,MAXORD
        SP(M)=SP(1)*CP(M-1)+CP(1)*SP(M-1)
        CP(M)=CP(1)*CP(M-1)-SP(1)*SP(M-1)
    40 CONTINUE
        ENDIF
C
        AOR=RE/R
        AR=AOR**2
C
        BR=0.
        BT=0.
        BP=0.
        BPP=0.
C
C
        DO 70 N=1,MAXORD
        AR=AR*AOR
        DO 60 M=0,N
C
         COMPUTE UNNORMALIZED ASSOCIATED LEGENDRE POLYNOMIALS
         AND DERIVATIVES VIA RECURSION RELATIONS
C
        IF (ALT .NE. OALT .OR. GLAT .NE. OLAT) THEN
        IF (N .EO. M) THEN
        P(N,M)=ST*P(N-1,M-1)
        DP(N,M)=ST*DP(N-1,M-1)+CT*P(N-1,M-1)
        GO TO 50
        ENDIF
        IF (N.EQ. 1.AND. M.EQ. 0) THEN
        P(N,M)=CT*P(N-1,M)
        DP(N,M)=CT*DP(N-1,M)-ST*P(N-1,M)
        GO TO 50
        ENDIF
        IF (N.GT. 1.AND. N.NE. M) THEN
        IF (M.GT. N-2) P(N-2,M)=0.0
        IF (M.GT. N-2) DP(N-2,M)=0.0
```

```
P(N,M)=CT*P(N-1,M)-K(N,M)*P(N-2,M)
        DP(N,M)=CT*DP(N-1,M)-ST*P(N-1,M)-K(N,M)*DP(N-2,M)
        ENDIF
        ENDIF
    50
        CONTINUE
\mathbf{C}
         TIME ADJUST THE GAUSS COEFFICIENTS
C
        IF (TIME .NE. OTIME) THEN
        TC(N,M)=C(N,M)+DT*CD(N,M)
        IF (M.NE. 0) THEN
        TC(M-1,N)=C(M-1,N)+DT*CD(M-1,N)
        ENDIF
        ENDIF
C
         ACCUMULATE TERMS OF THE SPHERICAL HARMONIC EXPANSIONS
C
        PAR = AR * P(N.M)
        IF (M.EQ. 0) THEN
        TEMP1=TC(N,M)*CP(M)
        TEMP2=TC(N,M)*SP(M)
        ELSE
        TEMP1=TC(N,M)*CP(M)+TC(M-1,N)*SP(M)
        TEMP2=TC(N,M)*SP(M)-TC(M-1,N)*CP(M)
        ENDIF
        BT=BT-AR*TEMP1*DP(N,M)
        BP=BP+FM(M)*TEMP2*PAR
        BR=BR+FN(N)*TEMP1*PAR
C
          SPECIAL CASE: NORTH/SOUTH GEOGRAPHIC POLES
C
        IF (ST .EQ. 0.0 .AND. M .EQ. 1) THEN
        IF (N.EQ. 1) THEN
        PP(N)=PP(N-1)
        ELSE
        PP(N)=CT*PP(N-1)-K(N,M)*PP(N-2)
        ENDIF
        PARP=AR*PP(N)
        BPP=BPP+FM(M)*TEMP2*PARP
        ENDIF
C
    60
        CONTINUE
    70
        CONTINUE
C
        IF (ST .EQ. 0.0) THEN
        BP=BPP
        ELSE
        BP=BP/ST
        ENDIF
```

-	ROTATE MAGNETIC VECTOR COMPONENTS FROM SPHERICAL TO GEODETIC COORDINATES
С	BX=-BT*CA-BR*SA BY=BP
_	BZ=BT*SA-BR*CA
C	COMPLETE DECLINATION (DECL. INCLINATION (DID) AND
_	COMPUTE DECLINATION (DEC), INCLINATION (DIP), AND TOTAL INTENSITY (TI)
C	DII CODT/DV++2.DV++2\
	BH=SQRT(BX**2+BY**2) TI=SQRT(BH**2+BZ**2)
	DEC=ATAN2(BY,BX)/DTR
	DIP=ATAN2(BT,BA)/DTR DIP=ATAN2(BZ,BH)/DTR
С	
	COMPUTE MAGNETIC GRID VARIATION IF THE CURRENT GEODETIC POSITION IS IN THE ARCTIC OR ANTARCTIC (I.E. GLAT > +55 DEGREES OR GLAT < -55 DEGREES)
С	(I.E. GLAT > +33 DEGREES OR GLAT < -33 DEGREES)
C	OTHERWISE, SET MAGNETIC GRID VARIATION TO -999.0
С	OTHERWISE, SET MERCINETIC GRAD VARIATION TO 377.0
C	GV=-999.0
	IF (ABS(GLAT) .GE. 55.) THEN
	IF (GLAT .GT. 0AND. GLON .GE. 0.) GV=DEC-GLON
	IF (GLAT .GT. 0AND. GLON .LT. 0.) GV=DEC+ABS(GLON)
	IF (GLAT .LT. 0AND. GLON .GE. 0.) GV=DEC+GLON
	IF (GLAT .LT. 0AND. GLON .LT. 0.) GV=DEC-ABS(GLON)
	IF (GV .GT. +180.) GV=GV-360.
	IF (GV .LT180.) GV=GV+360. ENDIF
C	ENDIF
C C	
C	OTIME=TIME
	OALT=ALT
	OLAT=GLAT
	OLON=GLON
C	
C	
_	RETURN
C C	
C	EMD.
	END

DISTRIBUTION LIST

CGFMFLANT (NSAP Advisor)	
CGFMFPAC (NSAP Advisor)	•
CGMCDEC (NSAP Advisor)	•
CINCLANTELT (N37C, NSAP Advisor)	3 : -1 : -1 : -1 : -1 : -1 : -1 : -1 : -
CINCPACELT (02M, J37, NSAP Advisor)	3
CINCUSNAVEUR (NSAP Advisor)	•
COMAREASWFORSIXTHFLT (CTF 66)	1
COMINEWARCOM (NSAP Advisor)	-
COMNAVAIRLANT (NSAP Advisor)	-
COMNAVAIRPAC (NSAP Advisor)	-
COMNAVSEASYSCOM (Codes 56Z22, Library Documentation Branch	*
SEA 09B31	2
COMNAVSURFLANT (NSAP Advisor)	
COMNAVSURFPAC (NSAP Advisor)	1
COMOPTEVFOR	-
COMPACMISTESTCEN (Codes 1018, 3250, 4024, 5021)	-
COMSEABASEDASWWINGSLANT (NAVOCEANO Flt. Rep.)	-
COMSECONDLET (NSAP Advisor)	-
COMSEVENTHELT (NSAP Advisor)	-
COMSEVENTHELT (NSAP Advisor) COMSIXTHFLT (NSAP Advisor)	-
COMSTRUCTION TWELVE (20B)	-
, , ,	1
COMSUBLANT (NSAP Advisor)	1
COMSUBPAC (NSAP Advisor)	1 1 1 1 8
ALL COMSURFWARDEVGRU	5
COMTHIRDFLT (NSAP Advisor)	1
ALL DPT NAVSCI	1 6 3
FASOTRAGRULANT (Det Brunswick, Cecil Field, Jacksonville)	3
FASOTRAGRUPAC (Det Agana, Barbers Point, Cubi Point,	_
Moffett Field, North Island	5 1 1
FCTCLANT (Code 213)	1
FLEASWTRACENLANT	1
FLEASWTRACENPAC	1
FLEBALMISUBTRACEN	1
FLEMINEWARTRACEN	1
FLENUMOCEANCEN	1
NAVAIRCEVCEN (Code 8131)	1
NAVAIRTESTCEN (Technical Information Dept.)	1
NAVAVIONICCEN (Technical Library)	1
NAVCOASTSYSCEN (Technical Information Center - Code 6120)	1
NAVEASTOCEANCEN	1
NAVELEXCEN (Technical Library - Code AL)	1 2 2
ALL NAVELEXDET	2
NAVOCEANCOMCEN	
ALL NAVOCEANCOMDET	47
NAVOCEANO (Maury Oceanographic Library)	100
NAVOCEANSYSCEN (Technical Library - Code 447)	1
NAVPGSCOL	1
NAVPHIBASE	1
NAVPOLAROCEANCEN	1
NAVSHIPWPNSYSSENGSTA (Code 5125)	7

NAVSWC (Technical Library - Code E23)	1
NAVTACSUPPACT (Technical Library)	1
NAVWARCOL (Technical Library)	1 1 1 1 1 7
NAVWESTOCEANCEN	1
NAVWPNSUPPCEN (Code 016)	1
NISC (Technical Library - Code 63)	ĩ
NOARL (Codes 245, 302, 352, 370, 372, 372, 550)	7
NRL (Technical Library - Code 2620)	
NUSC (Technical Library - Code 02152)	1
OPTEVFOR (Technical Library)	1
SUBASE	1 1 1 1
SWFPAC (Technical Library - Code SPB161)	1
SWOSCOLCOM (Technical Library)	1
USNA (Nimitz Library)	1
WPNSTA (Technical Library)	1
ARMY	
Avionics R&D Act.	1
Eng Topo Lab	1
ESEIA	1
USAATCA-ASO	1
36 Medical DET	1
AIR FORCE	_
AFGWC	1
Ogden AFLC	1
(SPECIAL) (AFLC)	į.
CPUSS	1 1 1 1 1 1 1
HQSD	1
USAF Academy (Technical Library	1
9th SRW/IND	1
31st Test and Evaluation Squadron	1
366th Tectical Fighter Wing	1
403 Rescue and Weather Reconnaissance Wing/DOX 815 Weather Reconnaissance Wing/DOT	1
4029th Strategic Reconnaissance Training Squadron	1
6514th Test Squadron	1
DCA (Technical Library)	1
Defense Information School	1 1 1 1
DMACSC	i
DMAHTC (Technical Library)	1
DMAIAGS	Š
DNA (Technical Library)	1
DTIC	2
National Defense University	1
Analysis Technology	1
AVCO Systems Vision	1
BGS	1
Boeing Aerospace Company	1
Boeing Commercial Airplane Company	ī
Boeing Military Airplane Company	ĩ
Canadian Pacific Airlines	1
Center for Naval Analyses (Technical Library)	1

center for Potential Field Studies, CSM	Ţ
College Observatory	1
Control Systems Technology Center	1
Danish Meteorological Institute	1
Defense Communications Agency	1
Digital Cartographic Systems	1 1 1 1
Eastern Airlines	1
EG&G/Geometrics	1
ESL	1
General Dynamics	2
General Electric Co.	1
Geophysical Services, Inc.	2
Geosource Marine	1
Goddard Space Flight Center	1 1 2 1 2 1 2 1 2 2
Hughes Aircraft	2
Institute Nazionale Di Geofisica	1
Intergraph Corporation	1
KLM-Royal Dutch Airlines	1
LDGO	1
LITEF	1
Litton	1 1 1 1 1 1
Lockheed Corporation	1
Maritime Safety Agency	
McDonnell Douglas Corporation	1
McDonnel Douglas Helicopter Corp.	1
NOAA/NDBC	1
NOAA/NGDC	3
NOAA/NOS (Codes N/CG22X2, N/CG21X4)	2
Northrop Corporation	1
Shell Offshore, Inc.	1
Singer/Link SIO	1 1 1 3 2 1 1 1
Systems & Applied Sciences Corp.	1
Systems Control Technology	1
Technical Studies & Analytical Corp.	
TWR Corporation	1
USGS Denver	1 1 3 1 1
USGS Fredericksburg	1
USGS Menlo Park	1
WHOI	1